

LAMONT GEOLOGICAL OBSERVATORY OF  
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**SONIC PROPERTIES OF DEEP-SEA CORES  
FROM THE NORTH PACIFIC BASIN AND  
THEIR BEARING ON THE ACOUSTIC  
PROVINCES OF THE NORTH PACIFIC**

by

D. R. Horn, B. M. Horn and M. N. Delach

TECHNICAL REPORT NO. 10

CU-10-68 NAVSHIPS N00024-67-C-1186

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## P R E F A C E

This report has been compiled and written by deep-sea sedimentologists, not acousticians. It is an attempt to aid acousticians in their complex task of interpreting and predicting performance levels of bottom bounce sonar. Conclusions should be considered tentative. The investigation was undertaken because of the writers' confidence in the thesis that acoustic and sedimentary provinces of the ocean floor are strongly related.

David R. Horn





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## I N T R O D U C T I O N

There are two fundamental properties of the sea floor: roughness and bottom material. Both play critical roles in the performance of bottom bounce sonar because such systems employ the sea floor as an acoustic interface. An understanding of the properties of surface and near surface ocean sediments, which may either reflect or absorb sound, remains at an almost elementary level. The purpose of this report is to describe the materials comprising the floor of the North Pacific Ocean. In so doing, it is hoped that the data will serve system analysts in their tasks of interpreting and predicting performance levels of sonar equipment within this deepest and largest of ocean basins.

During the past two years, sedimentologists at Lamont have amassed a large amount of data on the acoustical properties of deep-sea cores. This work was part of the Marine Geophysical Survey Project of the U.S. Naval Oceanographic Office. Knowledge gained from the investigations has made it possible to predict the sonic properties of sediment accumulating on the ocean floor. The U. S. Naval Ship Systems Command contracted Lamont Geological Observatory to apply this knowledge to cores from the North Pacific (Fig. 1).



FIGURE 1

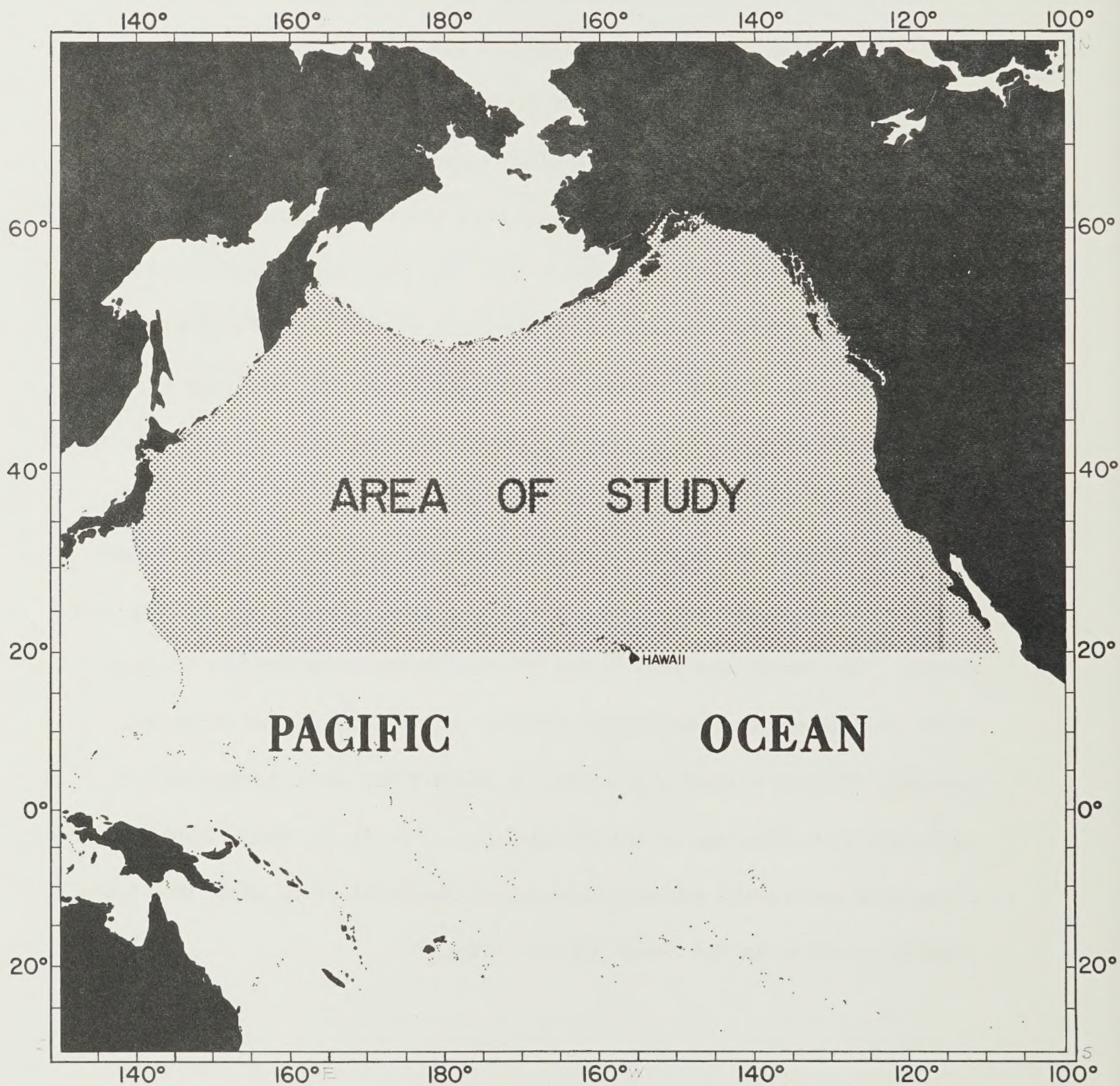


Figure 1. Location of study area. Cores taken north of 20° N. latitude were analyzed.



All sediment cores taken north of a line that passes east-west through Hawaii ( $20^{\circ}$  N. latitude) have been described and analyzed. Included in the report are maps depicting submarine physiography of the North Pacific, regional distribution of sub-bottom reflecting horizons (turbidity current deposits and volcanic ash layers), and predicted sonic properties of the sea floor at Lamont coring sites.

It is postulated that the distribution of surface and near surface reflecting horizons on the floor of the North Pacific (i. e. reflectivity of the ocean bottom) is directly related to the framework of deep-sea sedimentation within the North Pacific Basin. Research on the performance of bottom bounce sonar will be greatly hampered if similar studies are not conducted in other parts of the world's oceans.

## METHODS

### General statement

The cores were collected by scientists and crews aboard the research vessels VEMA and ROBERT D. CONRAD. A Ewing piston corer was employed to recover the cores. They are 2 1/2 inches (6.4 cm) in diameter and range in length from a few inches to 56 feet (17.1 m). The average length of the cores from the North Pacific is 25 feet (7.6 m). A complete description of the coring procedure and methods of storage at Lamont has been given by Ericson and others (1961).

The use of textural and bulk properties of cores as indices to their acoustical character is discussed at length in the next section of the report. Sound velocity data on which these predictions are based were determined using a sediment velocimeter (Underwater Systems, Inc. - Model 201 A). Bulk properties of cores were measured on samples taken from freshly extruded or split cores employing air comparison pycnometers (Beckman Instruments, Inc. - Model 930). Complete textural analyses of 1500 samples were carried out following the procedure of sieving and pipetting outlined by Folk (1961).

#### Prediction of the acoustical properties of sediment cores

Under the Marine Geophysical Survey Project of the U. S. Naval Oceanographic Office, Lamont personnel measured 50,000 sound speeds through ocean sediment cores. These velocities were then compared with bulk, textural and chemical properties of the cores (Horn, 1967; Horn and others, 1967a, 1967b, 1968a, 1968b, 1968c). The results supported the findings of other workers and confirmed that certain bulk and textural properties have a definite bearing on the speed at which sound travels through unconsolidated sediments (Hamilton and others, 1956; Sutton and others, 1957; Nafe and Drake, 1957, 1961, 1963; Shumway, 1960a, 1960b; Schreiber, 1966, 1967a, 1967b, 1967c, 1967d, 1968a, 1968b).

Although bulk properties (wet density, porosity, moisture content and void ratio) and mean grain size correlate well with sound speed, only



mean grain size shows a consistent relationship (Fig. 2). Plots of velocity versus bulk properties exhibit considerable scatter. An example is shown in Figure 3 where sound velocity is plotted against wet density. Careful inspection of the samples revealed that correlation between sonic and bulk properties broke down when sediments exhibited 1) secondary compaction effects produced by loading, 2) post-depositional alteration of volcanic constituents that resulted in changes of primary properties and 3) layers containing significant amounts of hollow particulate material (e.g. foraminiferal tests, pumice fragments). In Figure 4 such sediments have been deleted from the plot and the correlation between wet density and sound velocity is greatly enhanced.

Curves were fitted to plots of mean size versus velocity and wet density versus velocity (Figs. 2, 3, 4) using the method of least squares. The evidence indicates that these properties are interdependent and serve as indices of each other. A series of statistical tests are being applied to the data and results will be presented in a later report. To date, when all data are grouped together regardless of sediment type, the absolute deviation from the least squares curve for mean size versus velocity is 27.9 m/sec, whereas for wet density versus velocity it is 29.3 m/sec. Until further tests are completed, the data indicate that mean grain size is the best over-all index of the sonic properties of a sediment.

Mean grain size was adopted as an index of the acoustical properties of sediment cores from the North Pacific. Computer programs

FIGURE 2

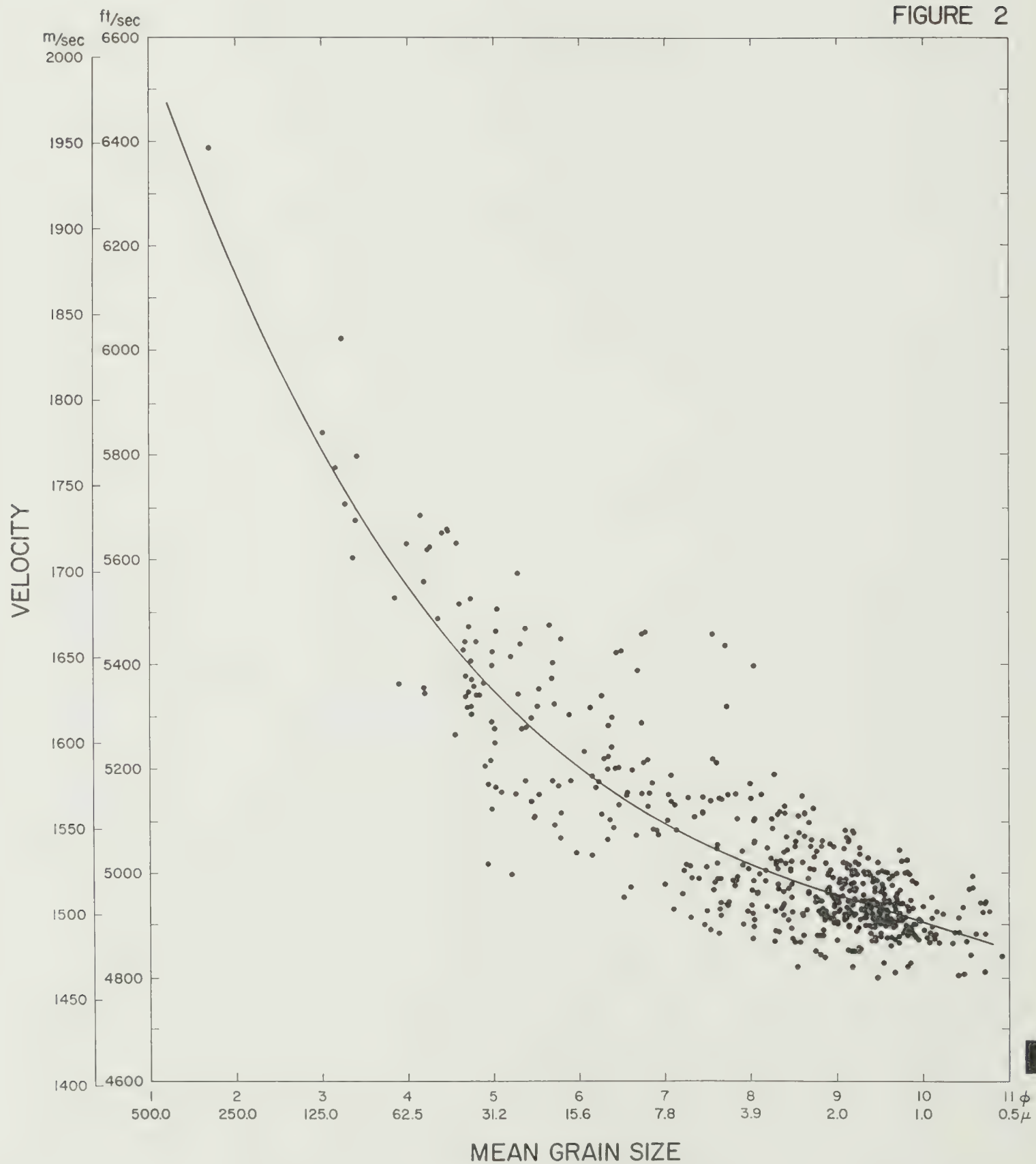


Figure 2. Mean grain size versus velocity. Trend line on this and subsequent figures is least squares curve drawn to third power.



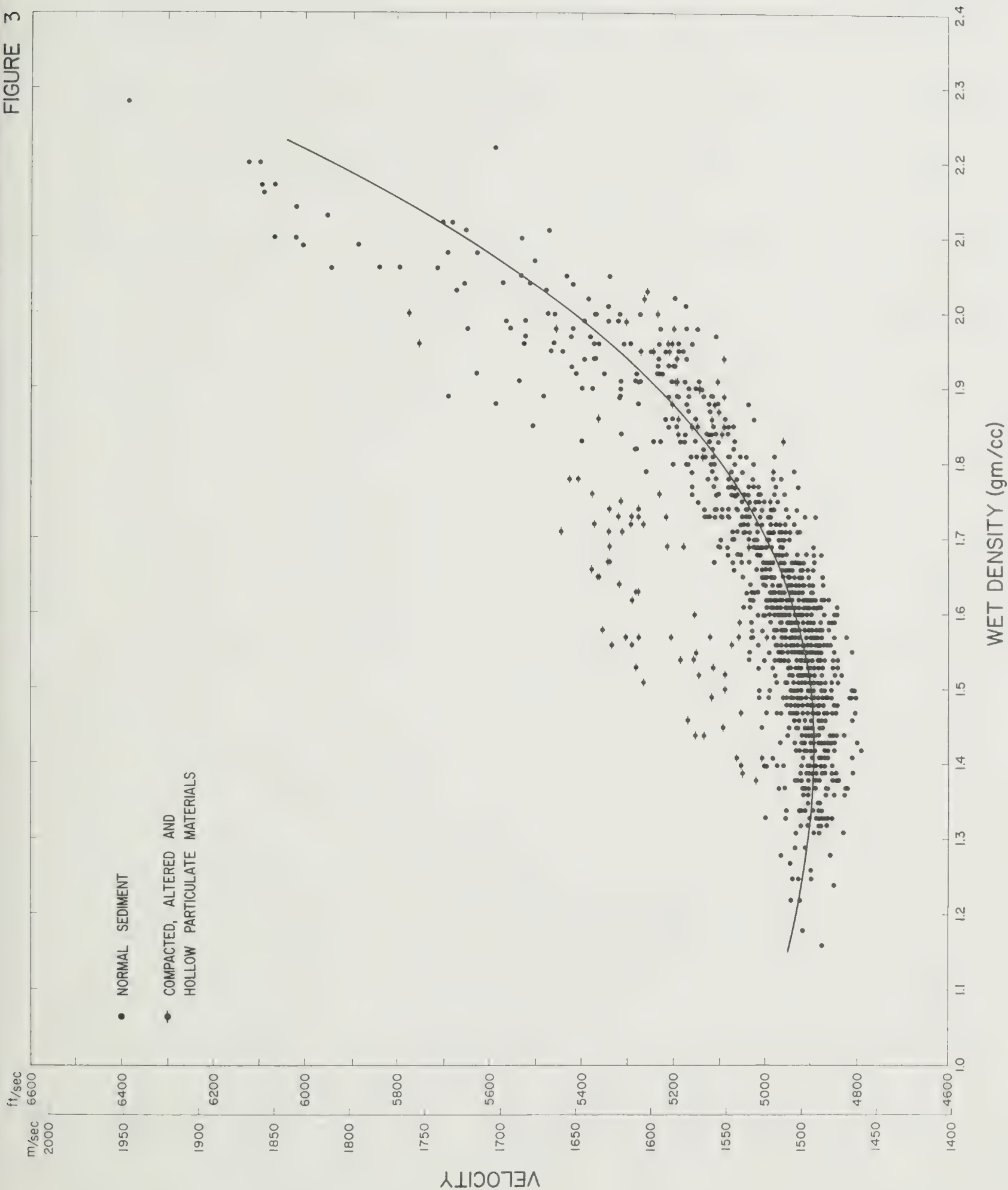


Figure 3. Wet density versus velocity, total data. Plot includes 1) normal sediment and 2) compacted, altered, and hollow particulate materials. Note that the latter have higher than normal velocities.

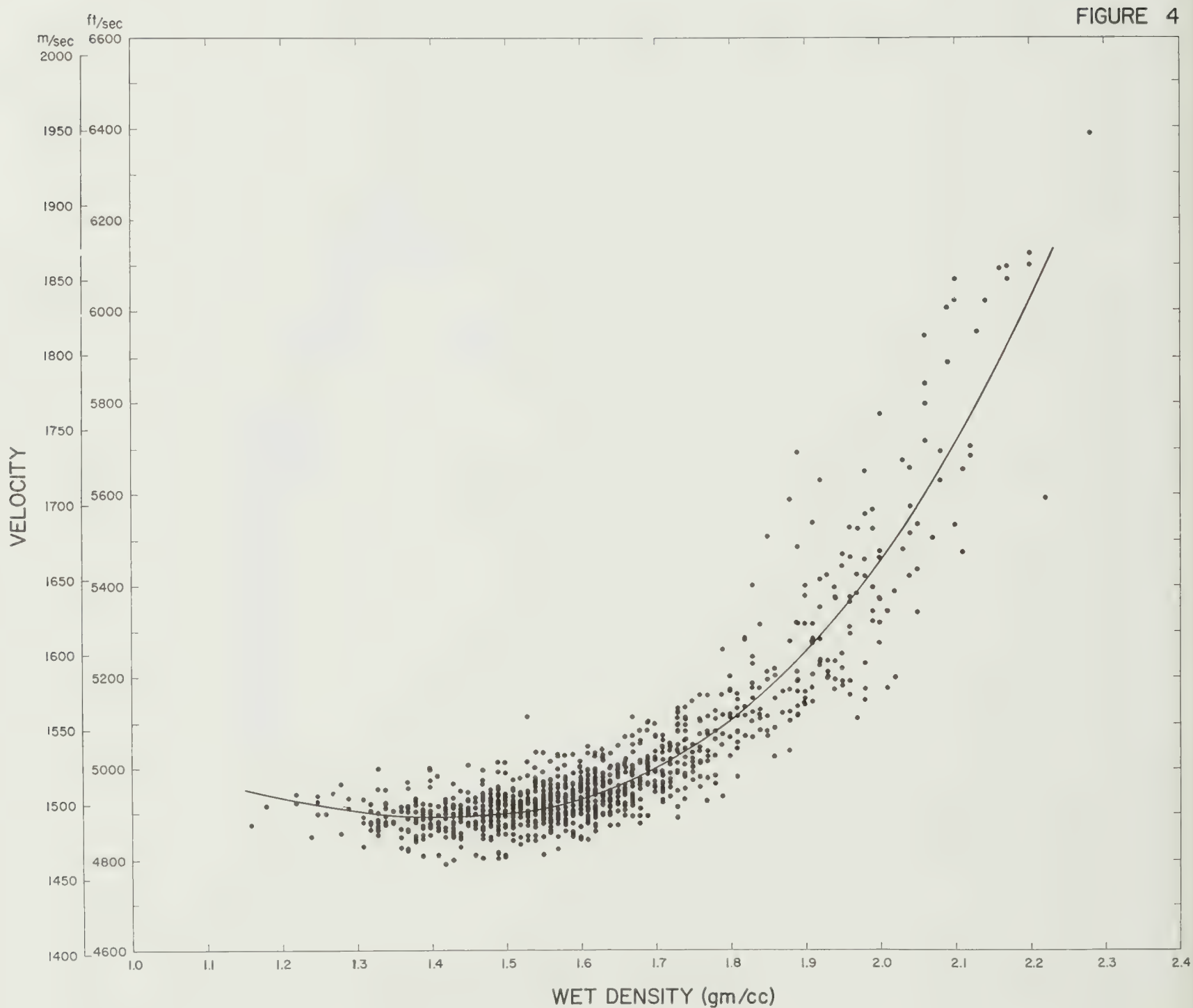


Figure 4. Wet density versus velocity, cleaned data. There is a strong correlation between these properties when compacted, altered and hollow particulate materials are removed from plot.

designed specifically to predict wet density and sound velocity of deep-sea sediments were executed. Appendix B provides a listing of the samples which were analyzed for texture and they serve as the basis for predicting sound velocity and wet density of sediments from the North Pacific. A table of sound velocities and wet densities with their equivalent mean grain sizes is presented in Appendix C. This information is plotted in Appendix D with the position and thickness of surface and near surface reflecting horizons. The method of presenting the data is such that the reader can locate a core closest to his point of interest in the North Pacific using the large maps (Figs. 6, 7, 8); then refer to Appendix D for details of the sonic and other physical properties of the sea floor at the coring site. The acoustic data should be corrected for depth and temperature as outlined by Hamilton (1963).

## DISTRIBUTION OF SUB-BOTTOM REFLECTING HORIZONS IN THE NORTH PACIFIC

### Coincidence of sedimentary and acoustic provinces

Sub-bottom reflecting horizons described in this report are layers of sediment at least 10 cm thick, coarse-grained, characterized by intermediate to high sediment sound velocities, and reflect sound. In the North Pacific only two types of sediment comply with this definition and have widespread distribution. They are volcanic ashes and turbidity current deposits.



Volcanic ash and turbidites occur within definite sedimentary provinces. Therefore, the reflectivity of the sea floor based upon bottom materials should prove to be a direct function of the distribution of these sediments in the North Pacific. Because ash and turbidites offer the only reliable reflecting horizons, the emphasis of this report has been placed on mapping their distribution and defining their acoustic properties (Figs. 5, 6, 7, 8 and Appendix D).

It is predicted that best performance of bottom bounce sonar will occur in areas of turbidity current activity (see Fig. 5). It is here that coarse-grained, closely spaced, high velocity layers occur; and reflectivity will be at a maximum. Areas of turbidite deposition are characteristically flat (i. e. abyssal plains), further enhancing sound reflection at the sea floor.

Intermediate bottom reflectivity should be a trait of areas where volcanic ash horizons are present (Fig. 5). The ash generally is in thin layers of silt and sandy silt with sound velocities of 1625-1650 m/sec or 5331 - 5413 ft/sec. In the cores they are separated from one another by thick sections of uniform brown mud. Because these deposits are the products of aerial and subsequent submarine dispersal, they occur over wide areas of the sea floor. Their distribution is not restricted by submarine physiography.

It is predicted that poorest performance of bottom bounce sonar will coincide with central areas of the North Pacific (Fig. 5). For millions

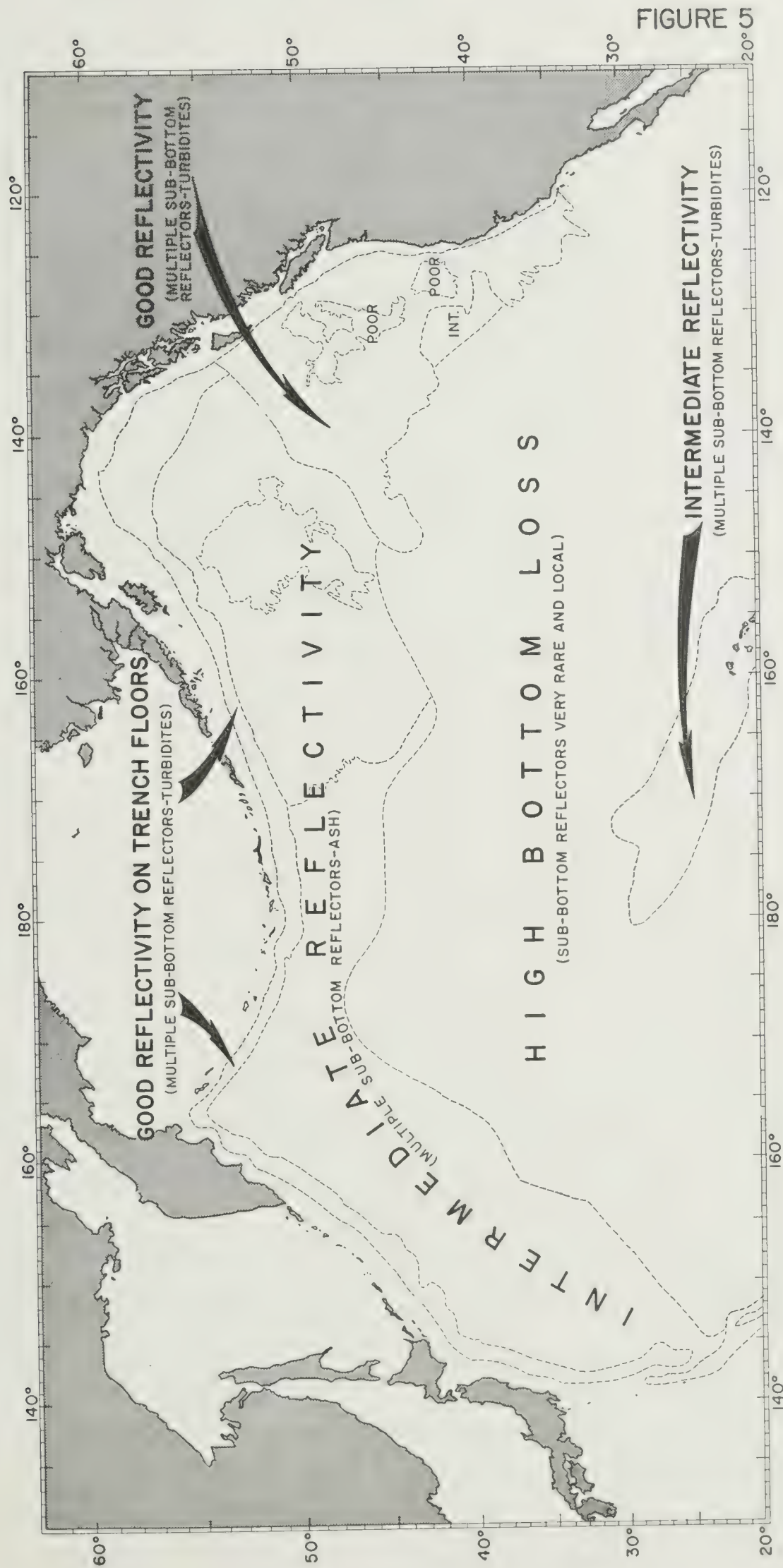


Figure 5. Reflectivity of the floor of the North Pacific based on deep-sea cores.



of years these have been and still are sites of clay deposition.

Bottom loss will be either very high or erratic and unpredictable. The former is due to thick sections of clay, whereas the latter results from patchy distribution of manganese nodules at the surface or coarse detritus produced by local submarine volcanism.

#### Northeast Pacific - Gulf of Alaska

Core data at Lamont indicate that latest turbidity current activity in the northeast Pacific is confined to the Alaskan Plain immediately adjacent to the continental terrace, the eastern and southern Tufts Plain, and are the prevalent sediment of the Cascadia Plain. No cores are available from the western half of the Tufts Plain or from much of the Alaskan Plain. Off the west coast of North America at 40° N. latitude turbidites extend at least 165 miles seaward; at 45° N. they have their maximum extension into the North Pacific Basin and occur in cores 1100 miles from shore; and at 50° N. they are present in cores taken 570 miles west of Vancouver Island (Figs. 5, 8). Areas of the northeast Pacific that have received turbidites during the Pleistocene should be marked by good reflection of sound at the sea floor.

The northeast corner of the Pacific Ocean includes numerous seamounts and abyssal hills. Both are features of positive relief, yet they have different sediment covering them. The summits of the seamounts are sites of either extremely coarse sand and gravel or have no

sediment cover and rock crops out at the surface. This is true of all coring sites at depths of less than 885 fathoms. Where coarse deposits occur, they are either products of in place weathering of volcanic rock constituting the seamount or they are lag deposits. The latter are common at the summits of seamounts. They are attributed to winnowing over long periods of time of fine sediment fractions with gradual concentration of sand and gravel.

Local bottom sediment transfer of silt-size material occurs on the flanks of seamounts. This results in a zone of silt around the base of these features. Core data suggest that the summits of the higher seamounts are characterized by highly reflective materials. In addition, their lower slopes receive relatively coarse sediment through local processes of submarine weathering of the seamounts themselves. Therefore, bottom reflectivity should be quite good at the bases of submarine mountains.

Crestal portions of the Ridge and Trough Province off Washington and Oregon are covered by pelagic clay interlayered with biogenic chalk. These hills are generally above the compensation level for  $\text{CaCO}_3$  and lie above the upper level of turbidity current activity. Sediments covering the Ridge and Trough Province are clay and chalk throughout. These abyssal hills are the sites of pure pelagic sedimentation of fine-grained materials and bottom reflectivity presumably will be low.



Abyssal hills of the Gulf of Alaska, although similar in aspect to the hills to the east, lie within the fallout zone of ash released by volcanoes on the Aleutian Islands and the Alaskan Peninsula. The presence of ash horizons in sediments covering the hills may result in better system performance in this area than experienced over the Ridge and Trough Province.

In summary, much of the northeast Pacific is a site of turbidite deposition. Floors of the Alaskan, Tufts and Cascadia Abyssal Plains should be marked by good performance of bottom bounce sonar. The combination of multiple, closely spaced, sub-bottom reflecting horizons and lack of relief provide ideal conditions for efficient system performance. Submarine topographic highs within this turbidite province may either provide poor or intermediate system operation. Summits of the highest seamounts possess highly reflective materials but ruggedness of relief may result in poor performance. The Ridge and Trough Province should be an area of poor performance, whereas the central abyssal hills of the Gulf of Alaska are likely to provide intermediate levels of operation.

#### Aleutian Trench and Abyssal Plain

Cores from the floor of the Aleutian Trench and the bases of its walls contain turbidites. In fact, all cores from these parts of the trenches penetrate turbidite sequences (Fig. 8). The steep insular walls

of the trenches are free of graded units and it appears that these are areas of sediment bypass rather than deposition.

A common feature of the rugged landward walls of dea-sea trenches is a submarine terrace. Such benches occur at various levels on the steep trench slopes. A large submarine terrace or bench is present on the north wall of the Aleutian Trench (Figs. 6, 7, 8). Cores from this terrace contain turbidite sequences similar to those encountered on the floor of the trench.

Reflectivity of the Aleutian Trench and associated submarine benches should be good. Both contain multiple sub-bottom reflectors and they have level floors. Steep portions of the north wall do not have a cover of coarse sediment. Turbidites bypass this part of the trench, slopes are relatively great, and a combination of these factors critical to sonar performance should result in poor functioning of equipment.

No turbidites occur in cores taken from the Aleutian Abyssal Plain. This feature is a good example of why abyssal plains cannot be equated with good reflectivity. The Aleutian Plain is a product of an ancient sedimentary regime and turbidites that leveled the sea bottom south of the Trench are now covered by a thick section of pelagic mud. Hamilton (1967) reports that 96 meters of pelagic sediment overlies turbidites at the center of the Plain.

The reflectivity of the Aleutian Abyssal Plain presumably is intermediate, not because turbidites occur deep below the surface,

but rather because ash horizons cover all but the southernmost part of the Plain. Ash derived from the Aleutian Islands has been transported great distances in a southerly direction into the North Pacific (Fig. 7). It occurs as distinct layers as far south as 680 miles from the Fox Islands, 440 miles south of the Andreanof Islands, and 540 miles seaward of Rat Island. More important to acousticians is the ash which is in layers thick enough to reflect sound. Sub-bottom reflectors consisting of ash extend across much of the Aleutian Abyssal Plain. They occur in cores 690 miles south of Unimak Island immediately west of the Alaskan Peninsula (Figs. 5, 6). Ash reflectors extend 400 miles south of the central islands of the Aleutian Island arc. These relatively coarse sediments result in a belt at the northern limits of the North Pacific Basin which should be characterized by intermediate performance levels. Reflectivity may increase over the floor of the Aleutian Abyssal Plain where the sea bed is flat.

#### Japan - Kamchatka

The situation seaward of Japan, the Kurils, and Kamchatka is much the same as that described for the sea floor south of the Aleutian Islands (Fig. 5). Deep trenches lie immediately oceanward of land areas, but abyssal plains are absent. Sedimentation beyond the trenches is predominantly pelagic and has occasionally been interrupted by rapid accumulation of volcanic ash.

Turbidites cover submarine terraces on the insular walls of the trenches and are the principal sediment along axes of trenches.



Sound reflection should be good in these areas, but should drop off over the steep walls of these submarine deeps.

Seaward of the trenches, sub-bottom reflecting horizons are predominantly the product of volcanism. Ash derived from vents located along the Asiatic coast constitute the reflectors. Very distinctive layers of white ash occur within a broad zone due east of Japan, the Kurils, and the Kamchatka Peninsula (Fig.7). These beds are in cores as much as 780 miles southeast of Kamchatka and extend as far as 1100 miles due east of the northern end of Honshu Island, Japan.

All ash horizons are not thick enough to serve as reflectors of sound. However, within a zone 600 miles wide that follows the northwest edge of the North Pacific Ocean (Fig. 6), these silts and sandy silts represent very reliable reflectors. They are consistently present in the cores taken within this region.

Reflectivity of the sea bed within the ash zone should be intermediate. The reflecting horizons are more widely separated in the sediment column than is true of the turbidites in the North Pacific. In addition, there are no abyssal plains here and relief is often rugged. Yet confidence that the layers are there, along with the knowledge that they reflect sound, suggest performance levels should be at least intermediate.

#### Hawaii - Midway Island Chain

Submarine slides and turbidity currents are active in the

vicinity of the Hawaiian Ridge (Hamilton, 1956; Moore, 1964; Schreiber, 1968a; and others). The few cores available from the archipelagic apron surrounding the islands contain turbidites. The latter occur within a narrow zone encircling the islands and extend seaward at least 80 to 140 miles from the nearest island (Fig. 8). Reflectivity should be intermediate over the Hawaiian Deep and other areas of turbidite fill (Figs. 5, 6). Presumably this will hold true for areas of the North Pacific adjacent to major seamounts and seamount chains (e.g. Emperor Seamount Chain). Performance of systems may deteriorate toward the islands as the slopes of the sea floor increase.

#### Central North Pacific

Except for the sea floor near the Hawaiian Islands, the great central area of the North Pacific Ocean has been the site of continuous and uniform clay deposition for millions of years. Thick sections of sound absorbing, very fine-grained sediment blanket the ocean bottom (Figs. 7, 8). Reflectivity here should be minimal (Fig. 5).

The central North Pacific does contain occasional reflecting horizons which are concentrations of manganese nodules, basaltic gravel, and thin partially indurated clays that are alteration products of volcanic detritus. The latter two occur within the Baja California Seamount Province and appear to result from local volcanism on the sea floor. The distribution of manganese nodules and volcanic debris is erratic and may hamper the prediction of system performance in the central North Pacific.

## C O N C L U S I O N S

Acoustic provinces of the world's oceans are strongly related to submarine physiography and bottom materials. An understanding of bottom roughness by itself does not provide the complete answer to problems of system performance. For example, parts of the Alaskan and Tufts Plains, and the entire Cascadia Plain are smooth and covered by highly reflective materials. However, the neighboring Aleutian Abyssal Plain offers an equally smooth surface yet may show lower levels of performance. This can be explained by both an absence of turbidites near the surface and the fineness of texture of pelagic sediments that cover the Plain. In addition, higher seamounts of the Gulf of Alaska have summits of bare rock or highly reflective lag gravels and sands. Yet seamounts of less relief are characterized by thick sections of pelagic clay and chalk. System performance over these features will be greatly dependent on the type of sediment that covers them.

Studies of over-all reflectivity of the world's oceans should follow a double-barreled approach: Bottom roughness surveys in conjunction with mapping of sediment distribution in the oceans offer the best means of evaluating sound reflection an/or absorption by the sea floor. The main conclusion of this investigation is that without maps showing surface and near surface sediment distribution on the ocean floors acousticians will have difficulty interpreting and predicting reflectivity of the sea bottom.



Within the North Pacific Basin the following conclusions have been arrived at solely on the basis of materials contained in sediment cores:

1. Highest reflectivity should occur in the northeast corner of the Pacific. Much of the Gulf of Alaska, and the abyssal sea floor off British Columbia, Washington, Oregon and northern California is covered with multiple sub-bottom reflectors (turbidites).
2. Bottom reflectivity will be good along axial portions of the circum-Pacific trench system and over benches on the insular walls of the trenches. Steep walls of these deeps are areas of sediment bypass which may result in their being sites of poor performance.
3. Seaward of Japan, the Kurils, Kamchatka Peninsula and the Aleutian Islands is a broad zone of intermediate reflectivity. Here volcanic ash horizons constitute the only sub-bottom reflectors. In addition, intervening hemipelagic sediments which are also slightly coarser may enhance sound reflection.
4. A zone of turbidites surrounds the Hawaii-Midway Island Chain. Reflectivity should be at least intermediate over these areas of turbidite fill.
5. The central North Pacific should be characterized by either high bottom loss or erratic performance of systems.

## A C K N O W L E D G M E N T S

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## APPENDIX A

CORE NUMBER, LOCATION, WATER DEPTH AND LENGTH OF CORE





## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
RC10-156	22° 20.5'N	157° 49' E	2954	5402	27.66	843
RC10-157	24° 46.5'N	159° 03' E	3107	5682	31.56	962
RC10-158	28° 07' N	160° 36' E	3222	5892	32.15	980
RC10-159	31° 13' N	162° 18.5'E	3223	5894	35.70	1088
RC10-160	32° 28.5'N	159° 50' E	2527	4621	39.67	1209
RC10-161	33° 05' N	158° 00' E	1961	3587	34.78	1060
RC10-162	31° 25' N	158° 48' E	2140	3913	30.81	939
RC10-163	32° 43' N	157° 30' E	1941	3550	35.93	1095
RC10-164	31° 43.5'N	157° 30' E	2059	3766	31.79	969
RC10-166	31° 49.5'N	157° 20' E	2039	3729	17.22	525
RC10-167	33° 24' N	150° 23' E	3331	6092	58.30	1777
RC10-168	32° 23' N	148° 25.5'E	3145	5751	32.94	1004
RC10-169	32° 30.5'N	151° 04' E	3139	5740	35.96	1096
RC10-170	32° 29' N	152° 13.5'E	3074	5621	20.50	625
RC10-171	32° 28.5'N	153° 01.5'E	3032	5544	39.07	1191
RC10-172	32° 06' N	154° 37.5'E	2399	4387	21.95	669
RC10-173	31° 41' N	156° 27' E	2218	4056	19.36	590
RC10-174	32° 04' N	157° 35' E	1745	3191	28.41	866
RC10-175	34° 35' N	159° 10' E	2195	4014	28.48	868
RC10-176	34° 47' N	160° 40' E	2311	4226	24.67	752
RC10-177	37° 12' N	170° 51' E	2899	5302	32.15	980
RC10-178	37° 48' N	172° 20' E	3176	5808	34.12	1040
RC10-179	39° 38' N	173° 43' E	2358	4312	24.84	757
RC10-181	44° 05' N	176° 50' E	3116	5698	38.09	1161
RC10-182	45° 37' N	177° 52' E	3041	5561	37.07	1130
RC10-184	49° 31' N	179° 04' W	2726	4986	37.83	1153

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
RC10-186	50° 12' N	177° 11' W	3604	6591	28.61	872
RC10-187	50° 39.5' N	175° 40' W	3399	6216	23.65	721
RC10-199	51° 19' N	174° 01' W	2569	4698	14.21	433
RC10-200	50° 44' N	173° 56' W	4001	7317	0.85	26
RC10-201	48° 32' N	173° 13' W	2820	5158	37.96	1157
RC10-202	45° 37' N	173° 00' W	3120	5523	38.06	1160
RC10-203	41° 42' N	171° 57' W	3217	5883	37.07	1130
RC10-205	44° 37' N	170° 03' W	3325	6081	37.73	1150
RC10-206	47° 13' N	170° 26' W	3006	5497	37.80	1152
RC10-207	50° 55' N	171° 33' W	3972	7264	9.91	302
RC10-208	51° 38' N	171° 46' W	2043	3737	16.08	490
RC10-210	50° 48' N	172° 38' W	3983	7284	16.08	490
RC10-211	50° 03' N	171° 45' W	2809	5137	17.75	541
RC10-212	51° 06' N	170° 08' W	3954	7231	19.13	583
RC10-213	51° 49' N	167° 45' W	3935	7196	12.96	395
RC10-214	50° 59' N	164° 08' W	2587	4731	24.08	734
RC10-215	51° 01' N	158° 06' W	2672	4887	19.03	580
RC10-216	50° 58' N	151° 10' W	2728	4989	28.64	873
RC10-217	50° 57' N	146° 05' W	2372	4338	15.75	480
RC10-218	50° 55' N	143° 15' W	497	909	2.62	80
RC10-219	51° 03' N	139° 33' W	2070	3786	16.40	500
RC10-220	51° 03' N	133° 44' W	1726	3157	37.60	1146
RC10-221	50° 33' N	131° 37' W	1550	2834	33.46	1020
RC10-222	49° 57' N	135° 14' W	1946	3559	24.67	752



## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
RC10-223	49° 18' N	134° 39' W	1993	3645	35.50	1082
RC10-224	49° 03.5' N	130° 57' W	634	1159	1.64	50
RC10-225	48° 45' N	127° 45' W	1387	2536	16.63	507
RC10-226	47° 27' N	127° 16' W	1386	2534	35.83	1092
RC10-227	46° 18' N	128° 00' W	1517	2774	30.87	941
RC10-228	45° 56' N	127° 00' W	1512	2765	12.50	381
RC10-229	45° 35' N	126° 09' W	1412	2582	10.79	329
RC10-230	40° 28' N	128° 25' W	1750	3200	35.04	1068
RC10-231	37° 58' N	128° 34' W	2584	4726	37.17	1133
RC10-232	35° 35' N	128° 39' W	2556	4674	31.79	969
RC10-234	28° 38' N	129° 06' W	2341	4281	14.60	445
RC10-235	25° 50' N	129° 25' W	2590	4737	15.09	460
RC10-236	22° 58' N	128° 17' W	2456	4491	14.30	436
RC10-237	21° 15' N	125° 07' W	2443	4468	21.49	655

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
RC11-158	20° 55' N	149° 54.5'E	1737	3177	31.92	973
RC11-159	23° 34' N	148° 35' E	3037	5554	7.71	235
RC11-160	26° 48' N	142° 54' E	2201	4025	12.96	395
RC11-163	39° 32' N	152° 42' E	3040	5559	34.61	1055
RC11-164	35° 19.5'N	162° 38' E	2820	5158	12.89	393
RC11-165	37° 03' N	166° 34' E	2722	4978	4.07	124
RC11-166	43° 46' N	171° 14' E	3194	5841	36.09	1100
RC11-167	50° 50' N	176° 15' W	2665	4874	19.36	590
RC11-168	45° 30' N	174° 35' W	3185	5824	1.18	36
RC11-169	42° 10' N	170° 14' W	3098	5665	34.68	1057
RC11-170	44° 29.4'N	163° 21.1'W	2981	5451	33.20	1012
RC11-171	46° 36.2'N	159° 39.7'W	2825	5167	38.09	1161
RC11-172	51° 15.3'N	164° 52.6'W	2629	4808	33.96	1035
RC11-173	53° 11.5'N	164° 58.5'W	1972	3607	39.53	1205
RC11-174	52° 34.6'N	151° 21' W	885	1618	11.68	356
RC11-175	54° 32.2'N	150° 22.1'W	532	972	8.53	260
RC11-176	56° 57' N	144° 44' W	2088	3819	33.96	1035
RC11-177	57° 00' N	138° 08.9'W	1617	2957	23.23	708
RC11-178	55° 11' N	140° 15' W	846	1547	2.85	87
RC11-179	53° 30' N	145° 39.4'W	2224	4067	25.98	792
RC11-180	53° 09.1'N	142° 53.7'W	2111	3860	34.32	1046
RC11-181	53° 17.5'N	135° 41' W	705	1298	.33	397

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
RC11-183	51° 29' N	136° 58.7' W	1988	3636	29.69	905
RC11-184	49° 43.2' N	140° 30.9' W	2165	3959	35.30	1076
RC11-185	47° 59.5' N	143° 24.5' W	2427	4438	29.46	898
RC11-186	47° 54' N	127° 12' W	1412	2582	40.19	1225
RC11-187	47° 08.7' N	130° 06.7' W	1460	2670	35.43	1080
RC11-188	46° 44.3' N	131° 35.1' W	1815	3319	37.17	1133
RC11-189	45° 58' N	134° 25' W	2145	3922	31.89	972
RC11-190	44° 57' N	138° 22' W	2326	4254	32.32	985
RC11-191	44° 31' N	139° 56.5' W	2399	4387	33.46	1020
RC11-192	42° 02' N	139° 57' W	2251	4116	8.04	245
RC11-193	39° 56.5' N	140° 02.5' W	2596	4748	33.46	1020
RC11-194	34° 59.5' N	139° 57' W	2900	5303	32.02	976
RC11-195	31° 51' N	139° 58.5' W	2698	4934	31.82	970
RC11-196	29° 10.5' N	139° 55.2' W	2694	4927	17.45	532
RC11-197	26° 23.6' N	139° 58.7' W	2413	4413	3.94	120
RC11-198	21° 30.5' N	139° 59.8' W	2941	5378	27.92	851



## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V20-64	23° 21' N	155° 52' W	2298	4204	15.09	460
V20-65	25° 51' N	153° 12' W	2933	5363	12.50	381
V20-66	28° 00' N	151° 10' W	2919	5338	23.69	722
V20-67	30° 33' N	148° 12' W	2757	5042	10.53	321
V20-68	30° 58' N	146° 48' W	3165	5788	16.27	496
V20-69	33° 16' N	144° 03' W	2926	5351	18.86	575
V20-70	35° 42' N	140° 51' W	2847	5207	18.44	562
V20-71	37° 41.5' N	137° 51' W	2899	5302	19.03	580
V20-72	39° 38' N	135° 06' W	2619	4790	15.09	460
V20-73	39° 38' N	133° 41' W	2610	4773	2.33	71
V20-74	41° 04' N	132° 22' W	2050	3749	25.46	776
V20-75	48° 12' N	126° 10' W	906	1657	14.01	427
V20-76	47° 54' N	127° 39' W	1437	2628	11.78	359
V20-77	47° 42' N	128° 40' W	1454	2659	9.51	290
V20-78	47° 15' N	131° 02' W	1631	2983	30.51	930
V20-79	46° 50' N	133° 18' W	2029	3711	24.48	746
V20-80	46° 30' N	135° 00' W	2079	3801	23.13	705
V20-81	46° 14' N	136° 30' W	2314	4232	9.28	283
V20-82	45° 56' N	138° 14' W	2348	4294	6.07	185
V20-83	45° 45' N	139° 24' W	2376	4345	4.82	147
V20-84	45° 27' N	141° 11' W	2437	4457	12.53	382
V20-85	44° 54' N	143° 37' W	2087	3817	22.87	697
V20-86	43° 37' N	148° 06' W	2809	5138	32.68	996
V20-87	41° 48' N	149° 55' W	2635	4819	21.88	667

## Location, Depths and Length of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V20-88	40° 11' N	151° 39' W	2778	5081	27.89	850
V20-89	38° 12' N	153° 35' W	3120	5706	27.66	843
V20-90	38° 48' N	155° 37' W	3276	5991	25.62	781
V20-91	37° 18' N	157° 42' W	3206	5863	14.63	446
V20-92	36° 18' N	159° 38' W	3152	5764	27.03	824
V20-93	35° 27' N	161° 28' W	3170	5797	20.80	634
V20-94	34° 36' N	163° 14' W	3277	5993	24.74	754
V20-95	33° 53' N	164° 47' W	3174	5804	29.79	908
V20-96	33° 01.5' N	166° 42' W	3156	5771	19.82	604
V20-97	32° 04' N	168° 44' W	3194	5841	26.61	811
V20-98	31° 10' N	170° 35' W	3102	5673	31.82	970
V20-99	30° 21' N	172° 17' W	3000	5486	8.04	245
V20-100	29° 05' N	174° 35' W	2920	5340	29.20	890
V20-101	28° 18' N	176° 57' W	2439	4460	26.51	808
V20-102	31° 11' N	177° 49' W	2852	5216	37.96	1157
V20-103	33° 59' N	177° 50' W	1882	3442	12.66	386
V20-104	37° 18' N	178° 10' W	2980	5449	38.19	1164
V20-105	39° 00' N	178° 17' W	2918	5336	40.58	1237
V20-107	43° 24' N	178° 52' W	3211	5872	42.06	1282
V20-108	45° 27' N	179° 14.5' W	3076	5625	56.10	1710
V20-109	47° 19' N	179° 39' W	3078	5629	47.64	1452
V20-110	49° 14' N	180° 00' W	2370	4334	15.92	485
V20-111	51° 01' N	179° 58' W	2106	3851	26.01	793

## Location, Depths, and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V20-118	50° 22' N	172° 43' E	2931	5360	31.43	958
V20-119	47° 57' N	168° 47' E	1498	2739	38.39	1170
V20-120	47° 24' N	167° 45' E	3399	6216	53.44	1629
V20-121	46° 58' N	164° 16' E	3204	5859	52.62	1604
V20-122	46° 34' N	161° 41' E	3042	5563	51.61	1573
V20-123	46° 15' N	157° 55' E	2681	4903	44.62	1360
V20-124	45° 50' N	154° 30' E	3026	5534	28.12	857
V20-125	43° 29' N	154° 22' E	3032	5545	31.10	948
V20-126	42° 09' N	155° 52' E	3016	5515	34.45	1050
V20-127	40° 17' N	156° 55' E	3053	5583	37.73	1150
V20-128	38° 47' N	157° 24' E	3069	5612	34.88	1063
V20-129	37° 41' N	156° 35' E	3153	5766	41.90	1277
V20-131	36° 20' N	151° 00' E	3203	5858	33.99	1036
V20-133	32° 58' N	140° 34' E	822	1503	5.77	176
V20-135	34° 43' N	139° 55' E	1421	2598	25.69	783
V20-136	32° 55' N	142° 32' E	3448	6306	13.02	397



## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V21-59	20° 55' N	158° 06' W	1636	2992	12.47	380
V21-60	20° 51' N	158° 09' W	2051	3751	11.22	342
V21-61	21° 36' N	161° 26' W	2506	4583	19.46	593
V21-62	22° 14' N	165° 14' W	2529	4625	19.36	590
V21-63	22° 51' N	169° 41' W	2556	4674	16.63	507
V21-64	23° 27' N	173° 13' W	2661	4867	21.49	655
V21-65	23° 58' N	176° 51' W	2934	5365	27.23	830
V21-66	24° 31' N	179° 21' E	3063	5601	25.13	766
V21-67	24° 58' N	176° 16' E	3215	5879	19.85	605
V21-68	25° 31' N	172° 45' E	3261	5953	19.75	602
V21-69	26° 26' N	169° 02' E	3271	5982	19.55	596
V21-70	27° 05' N	166° 04' E	3256	5954	21.33	650
V21-71	27° 54' N	162° 31' E	3256	5954	25.10	765
V21-72	28° 47' N	158° 50' E	2936	5369	5.91	180
V21-73	29° 28' N	154° 36' E	3211	5872	31.07	947
V21-74	29° 51' N	150° 50' E	3289	6015	35.47	1081
V21-75	30° 04' N	147° 41' E	3346	6119	27.89	850
V21-76	30° 25' N	144° 30' E	3235	5916	29.72	906
V21-77	30° 49' N	141° 59' E	3713	6790	13.78	420
V21-78	33° 05' N	140° 25' E	605	1106	31.17	950

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V21-85	27° 58' N	142° 30' E	921	1684	9.35	285
V21-86	27° 53' N	145° 03' E	3126	5717	23.92	729
V21-87	27° 53' N	146° 35' E	3215	5879	29.53	900
V21-88	25° 28' N	146° 30' E	3148	5757	1.18	36
V21-89	23° 35' N	145° 39' E	3183	5821	8.56	261
V21-90	23° 57' N	144° 23' E	3194	5841	7.84	239
V21-91	23° 25' N	143° 23' E	2804	5128	12.43	379
V21-92	23° 00' N	143° 10' E	2342	4283	.69	21
V21-93	24° 37' N	142° 28' E	1574	2878	9.02	275
V21-139	27° 47' N	144° 18' E	3286	6009	37.89	1155
V21-140	28° 33' N	146° 53' E	3253	5949	15.65	477
V21-141	30° 48' N	154° 04' E	3183	5821	20.47	624
V21-142	31° 35' N	156° 25' E	2319	4241	29.92	912
V21-143	31° 51' N	157° 20' E	1964	3592	2.53	77
V21-144	32° 41' N	160° 01' E	2696	4931	40.19	1225
V21-145	34° 03' N	164° 50' E	3329	6088	40.19	1225
V21-146	37° 41' N	163° 02' E	2170	3968	38.55	1175
V21-147	39° 33' N	162° 05' E	2874	5256	40.81	1244
V21-148	42° 05' N	160° 36' E	2995	5477	47.51	1448
V21-149	45° 08' N	160° 28' E	3098	5665	39.40	1201
V21-150	48° 00' N	162° 01' E	2962	5416	39.76	1212
V21-151	52° 16' N	163° 38' E	2764	5055	18.96	578

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V21-166	51° 25' N	169° 12' W	3884	7103	17.59	536
V21-167	52° 52' N	163° 45' W	3778	6909	3.94	120
V21-170	52° 21' N	165° 35' W	3834	7011	8.60	262
V21-171	49° 53' N	164° 57' W	2741	5013	28.38	865
V21-172	47° 40' N	164° 21' W	2842	5198	35.56	1084
V21-173	44° 22' N	163° 33' W	3004	5493	39.96	1218
V21-174	40° 08' N	162° 30' W	3112	5691	33.43	1019
V21-175	38° 22' N	161° 06' W	3092	5654	36.38	1109
V21-176	34° 54' N	160° 19' W	3074	5621	24.67	752
V21-177	33° 52' N	160° 08' W	3293	6022	33.79	1030
V21-178	31° 31' N	159° 42' W	3128	5720	28.25	861
V21-179	30° 43' N	159° 34' W	3156	5771	23.00	701
V21-180	28° 24' N	159° 11' W	3104	5676	31.27	953
V21-181	28° 51' N	158° 21' W	2899	5302	28.22	860
V21-182	29° 51' N	157° 02' W	3185	5824	29.17	889
V21-183	27° 15' N	157° 00' W	3123	5711	22.44	684
V21-184	25° 03' N	157° 54' W	2627	4804	10.50	320
V21-185	23° 01' N	159° 21' W	2656	4857	3.25	99
V21-187	20° 52' N	158° 09' W	2057	3762	31.73	967

## Location, Depths and Lengths of Cores

Core No.	Location		Water Depth		Core Length	
	Latitude	Longitude	Fathoms	Meters	Feet	Cm.
V24-89	20° 52' N	165° 07' E	3022	5544	15.58	475
V24-90	22° 12' N	168° 02' E	3055	5587	.59	18
V24-91	23° 39' N	170° 52' E	3246	5936	23.82	726
V24-92	24° 57' N	174° 00' E	3231	5909	26.74	815
V24-93	25° 48' N	176° 13' E	3162	5782	21.85	666
V24-94	26° 34' N	177° 46' E	3117	5700	29.07	886
V24-95	27° 36' N	177° 46' E	2891	5287	21.39	652
V24-96	27° 40' N	177° 59' W	1807	3305	23.62	720
V24-97	24° 48' N	178° 04' W	2979	5447	23.95	730
V24-98	21° 47' N	178° 47' W	2977	5444	25.85	788



## APPENDIX B

GRAIN SIZE DATA USED TO PREDICT SOUND VELOCITIES AND  
WET DENSITIES OF SEDIMENT LAYERS



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-156	5402	0	0.00	0.04	38.57	61.39	0.39	9.74	1.17	2.39	+10	.49
		55	0.00	0.01	19.79	80.20	0.20	9.99	0.98	2.26	+13	.45
		750	0.00	0.00	16.94	83.06	0.17	10.44	0.72	2.33	-.08	.44
RC10-157	5682	0	0.00	0.08	25.27	74.65	0.25	9.61	1.27	2.38	+21	.48
		923	0.00	0.95	24.74	74.31	0.25	9.80	1.12	2.78	-.09	.47
RC10-158	5892	0	0.00	0.05	20.77	79.18	0.21	9.84	1.09	2.29	+15	.45
		945	0.00	0.02	10.17	89.81	0.10	10.82	0.55	2.16	-.12	.45
RC10-159	5894	0	0.00	0.12	26.04	73.84	0.26	9.68	1.22	2.38	+19	.45
		1101	0.00	0.02	20.80	79.18	0.21	9.93	1.03	2.31	+10	.45
RC10-160	4621	0	0.00	0.43	28.98	70.59	0.29	9.51	1.37	2.57	+10	.47
		1161	0.00	0.96	34.31	64.73	0.35	9.02	1.93	2.51	+16	.50
RC10-161	3587	0	0.00	0.58	36.23	63.19	0.36	8.80	2.23	2.83	+11	.49
		52	0.00	0.13	44.37	55.50	0.44	8.57	2.63	2.74	+08	.53
		1045	0.00	1.53	31.30	67.17	0.32	9.09	1.83	2.36	+13	.57

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-162	3913	0	0.00	1.66	39.36	58.98	0.40	8.74	2.33	2.76	+0.08	.52
		54	0.00	0.65	36.32	63.03	0.36	8.36	3.04	2.16	-0.02	.61
		351	0.00	0.08	23.83	76.09	0.24	9.29	1.59	2.02	+0.07	.62
		922	0.00	0.23	28.43	71.34	0.28	9.63	1.26	2.73	-0.01	.48
RC10-163	3550	0	0.00	1.70	51.63	46.67	0.53	7.90	4.16	3.01	+0.14	.44
		455	0.00	1.42	34.07	64.51	0.34	8.89	2.09	2.43	+0.08	.59
		555	0.00	0.48	47.12	52.40	0.47	7.81	4.43	2.16	-0.03	.57
		1071	0.00	1.04	34.69	64.27	0.35	8.83	2.19	2.39	+0.15	.56
RC10-164	3766	0	0.00	1.58	44.31	54.11	0.45	8.51	2.73	2.92	+0.09	.50
		41	0.00	1.81	25.75	72.44	0.26	9.05	1.88	2.22	+0.08	.63
		150	0.00	0.57	45.95	53.48	0.46	8.25	3.28	2.87	+0.08	.48
		875	0.00	1.20	37.09	61.71	0.38	8.86	2.15	2.38	+0.08	.61
RC10-166	3729	0	0.00	1.00	46.62	52.38	0.47	8.38	2.99	3.00	+0.12	.45
		500	0.00	2.39	41.71	55.90	0.43	7.99	3.91	2.38	-0.02	.54



GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
RC10-167	6092	0	0.00	1.57	46.66	51.77	0.47	8.39	2.50	+19	.53
		69	0.00	38.01	53.79	8.20	0.87	4.71	1.77	+36	.54
		389	0.00	52.38	40.43	7.19	0.85	4.28	1.71	+53	.58
		764	0.00	0.63	43.42	55.95	0.44	8.79	2.72	+18	.47
		1154	0.00	8.88	78.58	12.54	0.86	5.71	1.68	+41	.59
		1228	0.00	9.86	84.81	5.33	0.94	5.19	1.24	+40	.54
		1616	0.00	6.95	79.87	13.18	0.86	5.86	1.68	+47	.58
		1626	0.00	31.22	61.38	7.40	0.89	4.85	1.58	+35	.54
		1676	0.00	1.44	38.74	59.82	0.39	8.98	2.75	+11	.47
RC10-168	5751	0	0.00	2.69	48.81	48.50	0.50	7.86	2.81	+06	.50
		973	0.00	19.24	40.59	40.17	0.50	7.13	3.26	+01	.48
RC10-169	5740	0	0.00	1.43	45.24	53.33	0.46	8.76	2.74	+19	.47
		165	0.00	32.47	55.95	11.58	0.83	5.15	2.05	+19	.54
		321	0.00	14.53	75.36	10.11	0.88	5.66	1.76	+20	.56

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC10-169	5740	931	0.00	36.12	56.85	7.03	0.89	4.74	37.20	1.55	+ .38	.53
		985	0.00	11.25	83.07	5.68	0.93	5.26	25.97	1.31	+ .33	.52
		1074	0.00	0.55	33.53	65.92	0.34	9.22	1.67	2.73	+ .09	.48
RC10-170	5621	0	0.00	0.76	33.54	65.70	0.34	9.19	1.71	2.79	+ .03	.47
		581	0.01	1.94	32.91	65.14	0.34	9.18	1.72	2.86	+ .07	.46
RC10-171	5544	0	0.00	1.11	33.64	65.25	0.34	9.16	1.74	2.67	+ .09	.47
		1170	0.00	5.99	45.81	48.20	0.49	7.93	4.09	3.11	+ .07	.44
RC10-172	4387	0	0.00	2.91	32.41	64.68	0.33	9.07	1.86	2.82	+ .13	.47
		480	0.00	33.43	65.51	1.06	0.98	4.19	54.70	0.61	+ .04	.55
		495	0.00	51.99	44.31	3.70	0.92	4.00	62.30	0.88	+ .38	.68
		523	0.00	18.51	76.90	4.59	0.94	4.71	38.10	1.07	+ .34	.64
		538	0.00	47.95	49.74	2.31	0.96	4.19	54.60	1.03	+ .38	.59
		548	0.07	44.09	53.50	2.34	0.96	4.21	54.00	0.98	+ .18	.52
		595	0.07	6.25	60.29	33.39	0.64	6.90	8.37	2.60	+ .26	.48
		643	0.00	21.75	75.92	2.33	0.97	4.77	36.60	1.03	+ .15	.56

# GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-173	4056	0	0.00	2.47	35.86	61.67	0.37	9.05	1.89	2.81	+ .16	.46
		115	0.00	1.49	20.21	78.30	0.20	9.44	1.44	2.15	+ .15	.61
		420	0.00	0.37	48.60	51.03	0.49	8.27	3.23	2.62	+ .16	.51
		540	0.00	0.07	25.35	74.58	0.25	9.59	1.29	2.37	+ .17	.48
RC10-174	3191	0	0.00	1.98	34.90	63.12	0.36	9.03	1.91	2.85	+ .06	.49
		262	0.00	0.77	40.64	58.59	0.41	8.73	2.34	3.05	+ .04	.44
		842	0.00	0.69	27.01	72.30	0.27	10.08	0.92	2.74	- .21	.44
RC10-175	4014	0	0.00	1.47	35.03	63.50	0.36	9.23	1.65	2.76	+ .04	.46
		75	0.00	0.87	36.76	62.37	0.37	9.04	1.90	2.72	+ .08	.49
		661	0.00	0.87	18.65	80.48	0.19	9.68	1.22	2.30	+ .07	.61
		830	0.00	0.62	37.23	62.15	0.37	8.98	1.98	2.68	+ .08	.49
RC10-176	4226	0	0.00	1.36	36.70	61.94	0.37	8.96	2.00	2.82	+ .01	.52
		210	0.00	0.84	36.39	62.77	0.37	8.86	2.14	2.40	+ .19	.54
		700	0.00	0.52	45.52	53.96	0.46	8.35	3.05	1.59	+ .32	.63



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-177	5302	0	0.00	0.00	27.16	72.84	0.27	9.68	1.22	2.42	+ .17	.46
		400	0.00	0.07	32.15	67.78	0.32	9.38	1.50	2.43	+ .17	.47
		852	0.00	0.02	30.29	69.69	0.30	9.45	1.43	2.41	+ .18	.46
		970	0.00	0.18	20.03	79.79	0.20	9.61	1.28	2.12	+ .18	.46
RC10-178	5808	0	0.00	0.00	25.87	74.13	0.26	10.54	0.67	2.15	+ .12	.44
		915	0.00	0.00	23.30	76.70	0.23	9.82	1.11	2.33	+ .16	.46
RC10-179	4312	0	0.00	0.11	31.08	68.81	0.31	9.41	1.47	2.57	+ .14	.48
		450	0.00	1.46	24.33	74.21	0.25	9.50	1.38	2.24	+ .24	.54
		670	0.00	2.10	25.54	72.36	0.26	9.61	1.27	3.06	- .21	.46
RC10-181	5698	0	3.19	0.24	29.58	66.99	0.31	9.35	1.53	2.73	+ .05	.49
		146	0.00	13.46	68.51	18.03	0.79	6.03	15.26	2.12	+ .27	.53
		1132	0.34	0.37	29.75	69.54	0.30	9.51	1.37	2.43	+ .18	.47
RC10-182	5561	0	0.00	1.97	31.11	66.92	0.32	9.38	1.50	2.69	+ .08	.47
		185	9.23	8.57	69.06	13.14	0.84	5.64	20.05	3.05	- .08	.71
		1102	0.00	1.09	35.68	63.23	0.36	9.27	1.62	2.67	+ .11	.47





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC10-188	3673	0	0.00	1.59	40.41	58.00	0.41	8.62	2.52	3.04	+0.02	.46
		385	0.00	1.53	53.55	44.92	0.54	8.11	3.61	2.81	+0.27	.47
		554	0.00	0.40	63.10	36.50	0.63	7.11	7.22	2.84	+0.21	.43
		690	0.00	1.44	49.35	49.21	0.50	8.33	3.09	2.88	+0.18	.49
RC10-189	3422	0	0.00	22.62	54.08	23.30	0.70	5.91	16.63	3.22	+0.05	.54
		74	0.00	97.59	2.41	0.00	1.00	2.76	146.90	0.51	+0.12	.51
		324	0.00	93.15	6.44	0.41	0.94	2.72	151.40	0.93	-0.20	.56
		440	0.00	2.09	67.19	30.72	0.69	7.34	6.14	2.58	+0.35	.54
RC10-190	3733	0	0.00	1.68	50.55	47.77	0.51	8.31	3.15	2.76	+0.24	.52
		53	0.00	47.68	51.11	1.21	0.98	3.96	63.90	0.64	+0.04	.58
		110	0.00	1.46	56.18	42.36	0.57	7.79	4.48	2.99	+0.25	.45
		142	0.00	57.46	40.68	1.86	0.96	3.79	72.20	0.62	+0.01	.55
		213	0.00	24.53	74.80	0.67	0.99	4.29	51.11	0.62	+0.16	.65
		260	0.00	0.07	42.85	57.08	0.43	8.86	2.14	2.46	+0.24	.48

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC10-191	3025	0	0.00	1.49	51.52	46.99	0.52	8.29	3.18	2.59	+ .31	.50
		96	0.00	1.67	86.55	11.78	0.88	5.74	18.62	1.79	+ .46	.57
		200	0.00	0.47	54.53	45.00	0.55	8.30	3.16	2.44	+ .35	.52
RC10-192	3684	0	0.00	1.09	46.57	52.34	0.47	8.62	2.53	2.45	+ .29	.51
		21	0.00	0.50	43.60	55.90	0.44	8.82	2.21	2.44	+ .25	.49
		220	0.00	1.30	34.25	62.45	0.35	9.24	1.65	2.80	+ .08	.46
RC10-193	137	0	0.24	95.89	2.72	1.15	0.70	2.21	215.60	0.79	- .12	.56
RC10-194	3801	0	0.00	0.00	31.65	68.35	0.32	9.59	1.30	2.42	+ .27	.43
		110	0.00	0.29	38.83	60.88	0.39	9.12	1.80	2.41	+ .26	.47
		424	0.00	0.02	29.96	70.02	0.30	9.04	1.90	2.43	+ .76	.42
RC10-195	3835	0	0.00	0.16	31.61	68.23	0.32	9.58	1.30	2.48	+ .20	.45
		457	0.00	0.03	36.02	63.95	0.36	9.69	1.21	2.60	+ .03	.43
		547	0.00	0.06	93.00	6.94	0.93	6.05	15.05	1.14	+ .46	.63
		772	0.00	0.29	95.10	4.61	0.95	5.79	18.03	0.92	+ .18	.55
		781	0.00	80.08	16.25	3.67	0.82	3.42	93.20	1.08	+ .44	.73



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-196	1007	0	0.00	17.88	53.09	29.03	0.65	6.36	12.09	2.98	+26	.50
		341	0.00	12.86	56.69	30.45	0.65	7.25	6.55	3.14	+27	.45
RC10-197	397	0	0.40	95.33	2.42	1.85	0.57	2.50	175.90	0.57	-.01	.57
		200	0.00	36.31	40.07	23.62	0.63	5.76	18.41	3.21	+55	.49
		462	26.55	62.11	5.54	5.80	0.49	0.99	501.00	3.14	-.17	.56
RC10-198	3728	0	0.00	3.33	54.34	42.33	0.56	7.96	4.01	2.72	+23	.55
		200	0.00	87.93	10.66	1.41	0.88	3.01	123.50	0.68	+29	.51
		233	0.20	94.06	4.36	1.38	0.76	2.11	230.00	0.90	+42	.53
RC10-199	4698	0	0.00	2.37	50.11	47.52	0.51	7.99	3.92	2.79	+14	.51
		104	0.00	27.93	45.89	26.18	0.64	5.90	16.66	2.90	+74	.47
		280	0.00	19.03	67.69	13.28	0.84	5.78	18.11	2.01	-.03	.49
		380	0.00	1.74	44.81	53.45	0.46	8.74	2.32	2.87	+22	.45
		430	0.00	60.37	35.24	4.39	0.88	3.76	73.60	0.97	+31	.64
RC10-200	7317	0	0.00	0.09	33.93	65.98	0.34	9.51	1.37	2.62	+12	.44



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-201	5158	0	4.89	3.84	31.92	59.35	0.35	8.78	2.27	3.66	-.12	.62
		310	0.00	1.43	58.01	40.56	0.59	7.48	5.58	2.96	+.19	.42
		522	0.00	1.35	82.13	16.52	0.83	6.41	11.75	1.63	+.28	.54
		960	0.00	1.65	55.81	42.54	0.57	8.13	3.56	2.54	+.30	.53
		1079	0.00	2.15	85.71	12.14	0.88	6.03	15.26	1.51	+.21	.49
RC10-202	5523	0	0.00	1.02	29.76	69.22	0.30	9.39	1.49	2.50	+.12	.48
		161	0.00	1.39	87.73	10.88	0.89	6.16	13.92	1.25	+.25	.51
		672	0.00	1.30	85.38	13.32	0.87	6.32	12.48	1.42	+.27	.53
		905	0.00	0.08	59.17	40.75	0.59	8.04	3.79	1.94	+.37	.58
		1145	0.00	1.06	51.78	47.16	0.52	8.33	3.09	2.21	+.35	.54
RC10-203	5883	0	0.00	0.07	22.92	77.01	0.23	9.89	1.05	2.21	+.12	.45
		700	0.00	0.77	22.41	76.82	0.23	9.94	1.01	2.46	+.04	.45
		960	0.00	0.07	28.40	71.53	0.28	9.65	1.24	2.41	+.17	.45
		1100	0.00	0.85	40.43	58.72	0.41	9.13	1.78	2.47	+.28	.47

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
RC10-205	6081	0	6.18	0.63	24.97	68.22	0.27	9.37	3.91	- .19	.64
		543	0.00	0.49	26.49	73.02	0.27	9.76	2.42	+ .16	.44
		571	0.00	0.00	29.77	70.23	0.30	9.60	2.84	+ .30	.46
		1110	0.00	0.00	41.15	58.85	0.41	9.11	2.47	+ .32	.44
RC10-206	5497	0	0.00	1.97	34.07	63.96	0.35	9.09	2.82	+ .02	.47
		245	0.00	10.38	83.09	6.53	0.93	5.54	1.42	+ .28	.49
		703	0.00	9.97	81.87	8.16	0.91	5.73	1.47	+ .13	.49
		1132	0.00	6.80	39.19	54.01	0.42	8.45	3.15	+ .05	.48
RC10-207	7264	0	0.00	1.14	40.45	58.41	0.41	8.70	2.81	+ .04	.50
		86	0.00	0.87	93.30	5.83	0.94	5.48	0.99	+ .29	.62
		130	0.00	0.91	24.89	74.20	0.25	10.17	2.42	- .05	.42
		181	0.00	0.00	88.98	11.02	0.89	6.69	1.33	+ .34	.65
		265	0.00	1.22	84.64	14.14	0.86	5.90	1.88	+ .63	.64
		299	0.00	6.56	89.96	3.48	0.96	4.37	0.56	+ .61	.73

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-208	3737	0	0.00	1.45	52.47	46.08	0.53	7.64	5.00	3.03	+1.13	.42
		190	1.03	52.28	27.57	19.12	0.59	4.54	42.70	3.54	+4.44	.48
		300	0.00	1.54	46.69	51.77	0.47	8.43	2.88	2.78	+1.16	.47
		410	4.96	69.75	17.79	7.50	0.70	2.51	174.70	3.07	+1.16	.55
RC10-210	7284	0	0.00	1.68	38.57	59.75	0.39	8.84	2.17	2.85	+1.10	.48
		250	0.00	0.00	23.65	76.35	0.24	10.26	0.82	2.36	-.04	.41
		446	0.00	0.04	55.34	44.62	0.55	8.34	3.08	2.86	+3.35	.43
		479	0.00	1.46	84.91	13.63	0.86	5.80	17.90	1.90	+6.61	.67
RC10-211	5137	0	0.00	2.00	46.38	51.62	0.47	7.96	3.98	2.81	+3.03	.49
		508	0.00	1.49	37.25	61.26	0.38	8.93	2.05	2.78	+3.09	.47
RC10-212	7231	0	0.00	0.21	35.43	64.36	0.36	9.13	1.78	2.56	+1.15	.47
		192	0.00	8.86	90.62	0.52	0.99	4.65	39.80	0.70	+4.49	.60
		296	0.00	86.86	11.91	1.23	0.91	3.26	104.10	0.61	+3.07	.53
		380	0.00	72.49	20.59	6.91	0.75	3.58	83.40	1.44	+4.45	.74
		516	0.00	1.14	96.73	2.13	0.98	4.79	36.10	0.58	+4.46	.58



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core (cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\tau_I$	$Sk_I$	$K'_G$
RC10-213	7196	0	0.00	0.81	54.23	44.96	0.55	8.07	3.72	2.97	+ .24	.45
		342	0.00	1.99	90.91	7.10	0.93	5.42	23.35	1.42	+ .43	.60
		351	0.00	0.27	67.52	32.21	0.68	7.50	5.49	2.59	+ .53	.49
		367	0.00	1.60	92.43	5.97	0.94	4.88	33.80	1.05	+ .60	.70
		390	0.00	2.04	62.38	35.58	0.64	7.44	5.74	3.00	+ .42	.45
RC10-214	4731	0	0.19	19.18	30.62	50.01	0.38	7.86	4.30	3.97	- .06	.43
		211	0.00	20.63	71.50	7.87	0.90	5.24	26.33	1.58	+ .18	.53
		273	0.00	20.87	70.33	8.80	0.89	5.53	21.54	1.89	- .11	.52
		319	0.00	26.27	69.05	4.68	0.94	4.91	33.10	1.47	+ .34	.49
		430	0.00	1.55	38.18	60.27	0.39	8.98	1.98	2.72	+ .16	.46
		725	0.00	29.56	67.04	3.40	0.95	4.75	37.10	1.48	+ .24	.49
RC10-215	4887	0	17.00	0.30	47.14	35.56	0.57	5.85	17.33	4.88	- .15	.54
		56	0.00	0.84	44.44	54.72	0.45	8.65	2.48	2.47	+ .29	.49
		217	0.00	27.66	66.44	5.90	0.92	5.09	29.36	1.67	+ .08	.48



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
								$\phi$	$\mu$			
RC10-215	4887	498	0.00	0.84	87.01	12.15	0.88	6.17	13.85	1.29	+ .30	.51
		550	0.00	1.88	42.05	56.07	0.43	8.66	2.46	2.81	+ .09	.50
RC10-216	4989	0	0.00	2.25	71.01	26.74	0.73	6.38	11.97	2.38	+ .44	.50
		13	0.00	2.42	93.86	3.72	0.96	5.92	16.43	1.16	+ .00	.48
		401	0.00	1.11	51.35	47.54	0.52	8.11	3.61	3.00	+ .18	.47
		822	0.00	1.70	49.15	49.15	0.50	8.26	3.26	3.03	+ .16	.44
RC10-217	4338	0	2.75	5.33	36.59	55.33	0.40	8.39	2.96	3.60	- .09	.55
		28	0.00	2.04	88.62	9.34	0.90	5.93	16.40	1.39	+ .37	.57
		120	0.00	1.87	45.08	53.05	0.46	8.49	2.76	2.97	+ .12	.46
		173	0.00	1.65	64.78	33.57	0.66	7.31	6.28	2.35	+ .42	.60
		187	0.00	30.46	60.61	8.93	0.87	5.06	29.83	1.98	+ .36	.57
RC10-218	909	0	4.67	86.63	5.89	2.81	0.51	1.92	264.00	1.62	- .03	.60
		40	39.88	50.28	5.39	4.45	0.55	- .43	1347.00	3.25	+ .13	.54
		65	88.72	9.07	1.52	0.69	0.69	-3.24	9490.00	1.61	+ .56	.61

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC10-219	3786	0	0.00	2.34	44.99	52.67	0.46	8.66	2.46	2.76	+1.19	.50
		16	0.00	90.27	9.73	0.00	1.00	3.03	122.40	0.67	+0.04	.53
		151	0.00	0.27	37.96	61.77	0.38	9.12	1.79	2.73	+1.14	.46
		164	0.00	61.38	25.43	13.19	0.66	4.21	53.70	2.70	+1.67	.56
		333	0.00	0.01	26.23	73.76	0.26	9.85	1.08	2.40	+1.10	.43
		353	0.00	0.01	93.57	6.42	0.94	5.67	19.59	0.95	+1.36	.64
		498	0.00	76.03	22.44	1.53	0.94	3.42	93.20	0.83	+1.20	.53
RC10-220	3157	0	0.00	1.03	29.70	69.27	0.30	9.55	1.33	2.61	+1.07	.46
		192	0.00	0.47	96.93	2.60	0.97	5.40	23.62	0.62	+1.08	.54
		315	0.00	0.21	49.29	50.50	0.49	8.65	2.48	2.76	+1.31	.42
		924	0.00	1.14	31.61	67.25	0.32	9.49	1.38	2.70	+1.08	.44
		1125	0.00	0.41	37.25	62.34	0.37	9.41	1.46	2.62	+1.11	.43
RC10-221	2834	0	0.00	0.10	33.20	66.70	0.33	9.31	1.57	2.74	+1.03	.45
		206	0.00	1.71	94.55	3.74	0.96	4.93	32.80	0.95	+1.27	.51

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC10-221	2834	554	0.00	0.00	39.80	60.20	0.40	9.32	1.56	2.74	+0.01	.45
		900	0.00	1.54	94.16	4.30	0.96	4.95	32.20	0.90	+0.38	.58
RC10-222	3559	0	0.00	0.07	38.37	61.56	0.38	9.05	1.88	2.78	+0.18	.42
		180	0.00	0.00	38.39	61.61	0.38	9.18	1.72	2.67	+0.14	.42
		350	0.00	1.90	95.21	2.89	0.97	4.63	40.10	0.62	+0.55	.64
		371	0.00	0.34	90.97	8.69	0.91	5.16	27.96	1.38	+0.65	.72
		703	0.00	0.21	92.78	7.01	0.93	5.25	26.27	1.19	+0.55	.69
		720	0.00	0.28	89.58	10.14	0.90	5.17	27.77	1.38	+0.49	.74
		738	0.00	0.81	92.67	6.52	0.93	4.91	33.20	1.13	+0.53	.74
RC10-223	3645	0	0.00	0.00	32.53	67.47	0.33	9.57	1.31	2.62	+0.03	.44
		400	0.00	0.06	28.00	71.94	0.28	9.79	1.13	2.59	+0.00	.44
		535	0.00	0.36	47.80	51.84	0.48	8.34	3.07	2.63	+0.16	.47
		861	0.00	0.04	21.93	78.03	0.22	10.08	0.92	2.36	+0.02	.44
		967	0.00	0.06	97.99	1.95	0.98	5.17	27.71	0.61	+0.32	.53
		1078	0.00	0.12	96.20	3.68	0.96	5.39	23.79	0.61	+0.18	.70



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	$\sigma'_0$ Gravel	$\sigma'_0$ Sand	$\sigma'_0$ Silt	$\sigma'_0$ Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\epsilon_I$	$Sk_I$	$K'_G$
								$\phi$	$\mu$			
RC10-224	1159	Jar	63.09	32.82	2.36	1.73	0.58	-1.70	3249.00	2.92	+ .40	.37
RC10-225	2536	0	0.00	0.20	24.13	75.67	0.24	9.75	1.16	2.48	+ .10	.45
		193	0.00	0.09	29.76	70.15	0.30	9.65	1.24	2.46	+ .14	.45
		341	0.00	12.18	81.82	6.00	0.93	4.51	43.60	1.00	+ .55	.83
		413	0.00	3.26	89.12	7.62	0.92	4.75	37.10	1.33	+ .81	.83
		438	0.00	22.58	71.12	6.30	0.92	4.51	43.70	1.32	+ .51	.73
		493	0.00	0.53	92.27	7.20	0.93	5.21	26.95	1.25	+ .61	.62
		506	0.00	74.46	24.88	0.66	0.97	3.66	78.70	0.43	+ .23	.47
RC10-226	2534	0	0.00	0.11	29.18	70.71	0.48	9.68	1.22	2.61	+ .01	.46
		513	0.00	0.12	76.48	23.40	0.77	6.67	9.79	2.49	+ .72	.55
		766	0.00	1.34	79.18	19.48	0.80	6.04	15.16	2.26	+ .73	.55
		951	0.00	0.04	48.29	51.71	0.48	8.62	2.52	2.77	+ .25	.45
		960	0.00	0.80	93.06	6.04	0.94	5.27	25.79	1.13	+ .39	.66
		1005	0.00	0.08	81.18	18.74	0.81	6.47	11.25	2.05	+ .58	.63



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
								$\phi$	$\mu$			
RC10-227	2774	0	0.00	0.08	15.57	84.35	0.16	10.13	0.89	2.14	+1.19	.46
		336	0.00	90.17	9.68	0.15	0.98	2.35	195.60	0.91	+3.36	.72
		716	0.00	0.02	92.64	7.34	0.93	6.33	12.40	0.87	+3.35	.59
		931	0.00	0.05	33.09	66.86	0.33	9.59	1.29	2.52	+1.11	.43
RC10-228	2765	0	0.00	0.12	22.51	77.37	0.23	9.70	1.20	2.47	+1.13	.48
		42	0.00	0.34	94.59	5.07	0.95	5.69	19.32	0.88	+2.24	.59
		65	0.00	0.50	44.92	54.58	0.45	8.72	2.36	2.79	+2.20	.44
		103	0.00	1.08	96.30	2.62	0.97	5.41	23.41	0.90	+1.15	.50
		165	0.00	2.06	87.16	10.78	0.89	5.19	27.33	1.70	+7.71	.72
		180	0.00	90.79	7.72	1.49	0.84	3.07	119.00	0.54	+3.32	.57
		237	0.00	0.66	90.74	8.60	0.91	5.40	23.57	1.18	+4.40	.67
		266	0.00	58.94	36.27	4.79	0.88	3.86	68.70	0.98	+4.45	.70
		320	0.00	91.62	6.27	2.11	0.75	2.68	156.00	0.73	+3.31	.59
		349	0.00	95.06	4.17	0.77	0.84	2.31	200.70	0.71	+2.21	.55
		380	0.00	83.67	13.62	2.71	0.83	2.95	129.10	1.11	+3.31	.58

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$S_{K_I}$	$K'_G$
RC10-229	2582	0	0.00	0.53	20.67	78.80	0.21	10.03	2.29	+ .12	.45
		172	0.00	1.49	82.46	16.05	0.84	5.70	1.82	+ .72	.58
		203	0.00	79.81	19.71	0.48	0.98	3.55	0.63	+ .33	.57
		247	0.00	94.70	3.40	1.90	0.64	2.56	0.71	+ .22	.52
		292	0.00	0.60	32.55	66.85	0.33	9.48	2.78	+ .01	.44
RC10-230	3200	0	0.00	1.90	37.29	62.52	0.37	9.22	2.69	+ .10	.46
		41	0.00	0.13	81.09	18.78	0.81	6.50	2.05	+ .57	.61
		63	0.00	0.09	30.41	69.50	0.30	9.68	2.42	+ .17	.44
		101	0.00	1.52	86.52	15.96	0.84	6.17	1.91	+ .57	.62
		151	0.00	0.84	82.09	17.07	0.83	6.45	1.93	+ .59	.65
		183	0.00	0.02	93.76	6.22	0.94	5.68	0.97	+ .33	.67
		191	0.00	0.52	34.58	64.90	0.35	9.39	2.65	+ .13	.46
		251	0.00	0.54	79.84	19.62	0.80	6.78	1.94	+ .56	.63
		301	0.00	2.40	93.74	3.86	0.96	5.06	0.83	+ .33	.64





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	Sk <sub>I</sub>	$K'_G$
RC10-231	4726	0	0.00	0.00	33.19	66.81	0.33	9.56	1.32	2.53	+ .14	.43
		65	0.00	0.00	52.09	47.91	0.52	8.42	2.90	2.96	+ .29	.40
		92	0.00	1.39	82.26	16.35	0.83	5.72	18.97	2.20	+ .78	.67
		152	0.00	0.00	54.46	45.54	0.55	7.84	4.35	3.33	+ .22	.37
		240	0.00	0.70	80.87	18.43	0.81	5.97	15.95	2.33	+ .79	.63
		261	0.00	0.01	17.68	82.31	0.18	10.14	0.88	2.22	+ .12	.45
		324	0.00	0.00	35.83	64.17	0.36	9.53	1.35	2.70	+ .07	.42
		382	0.00	0.44	58.54	41.02	0.59	7.41	5.85	2.61	+ .29	.48
		398	0.00	1.22	84.71	14.07	0.86	5.41	23.51	1.82	+ .72	.70
		420	0.00	0.00	34.85	65.15	0.35	9.50	1.38	2.69	+ .03	.42
		471	0.00	0.00	40.47	59.53	0.41	9.18	1.72	2.81	+ .07	.43
		502	0.00	0.00	25.90	74.10	0.26	9.86	1.07	2.66	- .00	.48
		595	0.00	0.00	35.59	64.41	0.36	9.51	1.37	2.61	+ .11	.44
		647	0.00	0.00	59.85	40.15	0.60	8.02	3.85	2.82	+ .45	.44



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\frac{Mz}{\mu}$	$\sigma_I$	$Sk_I$	$K'_G$
RC10-231	4726	662	0.00	0.83	86.84	12.33	0.88	5.55	21.34	1.69	+ .63	.71
		692	0.00	0.01	21.46	78.53	0.22	10.03	0.96	2.30	+ .11	.44
		817	0.00	0.00	50.29	49.71	0.50	8.00	3.89	3.31	+ .09	.38
		855	0.00	0.00	53.76	46.24	0.54	8.35	3.06	2.82	+ .34	.42
		898	0.00	0.00	13.98	86.02	0.14	10.47	0.70	2.16	- .01	.43
		921	0.00	0.00	27.82	72.18	0.28	9.84	1.09	2.56	+ .00	.42
		1013	0.00	0.57	67.78	31.65	0.68	7.09	7.34	2.82	+ .68	.45
		1030	0.00	0.90	80.94	18.16	0.82	5.99	15.69	2.31	+ .80	.65
		1061	0.00	0.01	22.55	77.44	0.23	10.33	0.78	2.53	- .19	.44
		1121	0.00	0.00	40.72	59.28	0.41	9.17	1.73	2.76	+ .13	.41
RC10-232	4674	0	0.00	0.25	13.33	86.42	0.13	10.41	0.73	2.17	+ .06	.46
		181	0.00	0.11	14.45	85.44	0.15	10.35	0.76	2.15	+ .06	.44
		301	0.00	0.20	13.23	86.57	0.13	10.07	0.93	2.04	+ .26	.50
		401	0.00	0.24	16.51	83.25	0.17	10.27	0.81	2.22	+ .09	.45

## GRAIN SIZE DATA

[illegible]



# GRAIN SIZE DATA

[illegible]





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC11-163	5559	0	0.00	1.44	31.09	67.47	0.32	9.33	1.55	2.60	+1.10	.47
		191	0.00	1.92	41.52	56.56	0.42	8.75	2.31	2.77	+1.15	.48
		214	0.00	37.26	58.54	4.20	0.93	4.42	46.60	1.13	+3.31	.51
		350	0.00	45.32	50.48	4.20	0.92	4.51	43.60	1.50	+3.38	.50
		420	0.00	1.48	46.07	52.45	0.47	8.62	2.54	2.80	+1.19	.46
RC11-164		784	0.00	3.65	83.46	12.89	0.87	6.14	14.11	1.82	+4.40	.63
		950	0.00	0.24	28.24	71.52	0.28	9.64	1.25	2.39	+1.18	.45
		1035	0.00	1.15	93.69	5.16	0.95	5.78	18.11	1.16	+3.32	.49
	5158	0	44.15	0.49	16.30	39.06	0.29	4.33	49.70	6.53	-3.33	.35
		15	0.00	0.04	29.79	70.17	0.30	9.66	1.24	2.42	+1.16	.45
RC11-165		297	0.77	0.81	30.87	67.55	0.31	9.43	1.44	2.55	+1.13	.47
		364	0.00	0.08	12.72	87.20	0.13	10.69	0.60	2.24	-1.14	.47
	4978	0	31.18	0.79	19.95	48.08	0.29	4.73	37.60	6.69	-4.49	.33
		92	0.00	0.32	17.35	82.33	0.17	10.31	0.79	2.37	-0.06	.45

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
RC11-166	5841	0	0.00	0.74	45.51	53.75	0.46	8.52	2.82	+ .16	.46
		503	0.50	1.45	36.13	61.92	0.37	9.06	2.79	+ .11	.46
		1080	0.00	1.92	32.89	65.19	0.34	9.22	2.82	+ .04	.46
RC11-167	4874	0	0.00	2.17	60.41	37.42	0.62	7.54	2.81	+ .36	.52
		59	0.00	3.01	47.44	49.55	0.49	8.42	2.89	+ .20	.48
		296	0.00	2.38	87.35	10.27	0.89	5.68	1.55	+ .42	.53
		570	0.00	1.99	39.42	58.59	0.40	8.74	3.00	+ .05	.42
RC11-168	5824	0	0.00	1.58	27.74	70.68	0.28	9.58	2.49	+ .14	.47
		30	0.00	2.25	88.91	8.84	0.91	5.66	1.42	+ .42	.51
RC11-169	5665	0	0.00	0.04	22.59	77.37	0.23	9.66	2.66	+ .05	.50
		373	0.00	0.05	47.31	52.64	0.47	7.93	3.05	- .01	.39
		460	0.00	0.99	21.17	77.84	0.21	9.43	2.04	+ .04	.64
		697	0.00	0.09	66.79	33.12	0.67	7.20	2.87	+ .33	.50
		1030	0.00	0.00	27.43	72.57	0.27	9.62	2.25	+ .27	.46



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\epsilon_I$	$Sk_I$	$K'_G$
RC11-170	5451	0	0.00	0.56	24.61	74.83	0.25	9.68	1.21	2.39	+ .15	.46
		617	0.00	30.24	66.09	3.67	0.95	4.65	39.60	1.38	+ .26	.52
		680	0.00	20.44	76.34	3.22	0.96	4.88	33.80	1.24	+ .31	.53
		710	0.00	0.83	91.03	8.14	0.92	5.68	19.41	1.36	+ .45	.49
		965	0.00	0.53	49.48	49.99	0.50	8.73	2.35	2.69	+ .31	.48
RC11-171	5167	0	8.87	1.58	39.57	49.98	0.40	8.05	3.76	4.05	- .17	.64
		265	0.00	0.85	96.20	2.95	0.97	5.66	19.68	1.05	+ .27	.47
		672	0.00	0.87	83.17	15.96	0.84	6.41	11.70	1.59	+ .37	.56
		789	0.00	18.05	77.18	4.77	0.94	5.02	30.74	1.32	+ .45	.55
		822	0.00	2.43	82.88	14.69	0.85	6.16	13.95	1.60	+ .38	.55
RC11-172	4808	0	0.00	2.16	38.81	59.03	0.40	8.91	2.06	2.68	+ .15	.48
		110	0.00	2.55	29.71	67.74	0.30	9.45	1.43	2.81	- .02	.45
		442	0.00	0.88	88.23	10.89	0.89	6.14	14.11	1.27	+ .34	.55
		695	0.00	19.59	72.58	7.83	0.90	5.37	24.06	1.62	+ .18	.51
		970	0.00	2.24	41.27	56.49	0.42	8.63	2.52	3.07	+ .08	.44



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC11-173	3607	0	0.00	2.25	34.22	63.53	0.35	9.08	1.85	2.81	+0.07	.45
		1150	2.96	1.74	36.48	58.82	0.38	8.97	1.99	3.06	+0.03	.45
RC11-174	1618	0	50.75	31.89	12.42	4.94	0.72	-1.14	2214.00	3.97	+0.81	.40
RC11-175	972	0	42.84	47.93	5.04	4.19	0.55	-0.27	1208.00	3.37	+0.08	.46
		200	7.68	46.96	25.81	19.55	0.57	4.78	36.20	3.93	+0.35	.56
RC11-176	3819	0	0.00	0.62	38.12	61.26	0.38	9.08	1.84	2.67	+0.13	.48
		90	0.00	0.60	29.23	70.17	0.29	9.62	1.26	2.50	+0.10	.44
		217	0.00	0.10	23.57	66.33	0.34	9.53	1.35	2.55	+0.13	.43
		340	0.00	0.06	37.67	62.27	0.38	9.35	1.53	2.55	+0.14	.43
		810	0.00	0.12	21.46	78.42	0.21	10.13	0.89	2.32	+0.03	.43
		1000	0.35	2.79	25.08	71.78	0.26	9.68	1.21	2.60	+0.05	.46
RC11-177	2957	0	0.00	0.31	30.88	68.81	0.31	9.48	1.39	2.49	+0.15	.45
		393	0.00	97.40	1.56	1.04	0.60	2.16	223.70	0.53	+0.27	.53
		457	0.00	94.50	3.27	2.23	0.59	2.09	233.70	0.81	+0.12	.62
		665	0.00	2.31	41.48	56.21	0.42	8.74	2.33	3.01	+0.11	.44
		690	0.00	2.22	95.27	2.51	0.97	4.56	42.20	0.57	+0.55	.60

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
RC11-178	1547	0	0.72	71.15	20.16	7.97	0.72	3.35	97.60	2.06	+ .35	.68
		55	13.61	80.31	2.82	3.28	0.46	0.95	514.00	1.85	- .06	.56
		75	67.24	30.06	1.58	1.12	0.59	-1.77	3418.00	2.34	+ .62	.40
RC11-179	4067	2	0.00	2.51	36.07	61.42	0.37	8.74	2.32	2.93	+ .05	.48
		100	0.00	11.52	33.66	54.82	0.38	8.23	3.33	3.44	- .05	.48
		236	0.00	2.95	47.22	49.83	0.49	8.49	2.78	2.45	+ .30	.53
		310	0.00	2.39	30.56	67.05	0.31	9.29	1.59	2.76	+ .04	.46
		334	0.00	1.53	92.57	5.90	0.94	5.93	16.32	1.05	+ .21	.53
RC11-180	3860	0	14.52	1.45	29.48	54.55	0.35	7.14	7.07	4.55	- .28	.53
		60	0.00	11.73	38.82	49.45	0.44	8.11	3.61	3.43	+ .04	.48
		134	0.00	1.05	70.67	28.28	0.71	6.57	10.50	1.77	+ .10	.40
		691	0.00	2.18	89.22	8.60	0.91	5.92	16.47	1.29	+ .24	.52
		965	0.00	1.92	25.14	72.94	0.26	9.56	1.32	2.66	+ .05	.48
		1011	0.00	16.98	37.25	45.77	0.45	7.68	4.85	3.74	+ .14	.42

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$		$\tau_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC11-181	1289	0	1.38	90.83	6.17	3.00	0.67	1.50	351.00	1.54	+ .32	.63
		44	25.38	71.26	1.95	1.41	0.58	-0.21	1162.00	1.26	+ .13	.54
		128	66.40	32.58	0.75	0.27	0.74	-1.55	2941.00	1.43	+ .17	.50
RC11-183	3636	0	0.00	0.22	30.28	69.50	0.30	9.61	1.28	2.51	+ .09	.43
		48	0.00	0.06	92.15	7.79	0.92	6.33	12.37	1.13	+ .43	.68
		148	0.00	0.06	91.78	8.16	0.92	6.16	13.98	1.00	+ .53	.69
		156	0.00	50.57	46.66	2.77	0.94	3.94	65.10	0.79	+ .07	.54
		194	0.00	69.18	28.94	1.88	0.94	3.31	100.30	1.08	+ .11	.47
		877	0.00	1.51	31.06	67.43	0.32	9.50	1.38	2.64	+ .08	.44
RC11-184	3959	0	0.00	1.50	32.98	65.52	0.33	9.42	1.46	2.65	+ .10	.43
		170	0.00	1.28	87.90	10.82	0.89	5.85	17.29	1.44	+ .39	.62
		210	0.00	1.97	53.13	44.90	0.54	7.66	4.93	2.49	+ .11	.49
		274	0.00	0.45	95.33	4.22	0.96	5.31	25.09	0.77	+ .37	.56
		1049	0.00	0.00	29.01	70.99	0.29	9.76	1.15	2.41	+ .13	.41



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\frac{Mz}{\mu}$	$\sigma_I$	Sk <sub>I</sub>	K <sub>G</sub> '
RC11-185	4438	0	0.00	1.11	34.68	64.21	0.35	9.30	1.58	2.49	+ .21	.43
		55	0.00	1.51	58.17	40.32	0.59	7.86	4.28	2.66	+ .39	.47
		64	0.00	2.30	88.18	9.52	0.90	5.94	16.25	1.30	+ .44	.53
		85	0.00	1.78	50.85	47.37	0.52	8.03	3.82	2.59	+ .18	.50
		322	0.00	1.09	35.89	63.02	0.36	9.14	1.77	2.64	+ .13	.48
		552	0.00	0.04	26.79	73.17	0.27	9.85	1.08	2.39	+ .16	.43
		670	0.00	0.23	12.48	87.29	0.13	10.52	0.68	2.12	+ .02	.43
		736	0.00	1.38	88.73	9.89	0.90	5.93	16.40	1.39	+ .39	.56
RC11-186	2582	0	0.00	0.13	22.18	77.69	0.22	9.88	1.06	2.33	+ .14	.45
		173	0.00	46.45	48.30	5.25	0.90	4.04	60.70	1.21	+ .14	.77
		371	0.00	0.07	42.43	57.50	0.42	8.87	2.13	2.50	+ .18	.50
		464	0.00	2.68	92.04	5.28	0.95	4.89	33.60	0.99	+ .64	.64
		562	0.00	2.15	90.15	7.70	0.92	4.93	32.80	1.38	+ .72	.74
		712	0.00	0.33	91.48	8.19	0.92	5.78	18.11	1.39	+ .09	.66



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
RC11-186	2582	727	0.00	94.58	4.48	0.94	0.83	2.76	147.20	0.57	+ .30	.55
		805	0.00	0.05	38.82	61.13	0.39	9.11	1.81	2.76	+ .17	.44
		1161	0.00	3.12	87.55	9.33	0.90	4.50	44.10	1.10	+ .67	.82
RC11-187	2670	0	0.00	0.30	22.72	66.98	0.34	9.35	1.53	2.53	+ .14	.46
		100	0.00	0.75	44.26	54.99	0.45	8.60	2.56	2.54	+ .18	.54
		258	0.00	0.51	50.14	49.35	0.50	8.16	3.48	2.97	+ .15	.45
		340	0.00	1.02	23.29	75.69	0.24	9.67	1.23	2.36	+ .14	.47
		514	0.00	0.98	58.82	40.20	0.59	7.89	4.20	2.50	+ .36	.50
		631	0.00	1.95	35.79	62.26	0.37	8.94	2.03	2.71	+ .07	.53
		903	0.00	0.84	27.06	72.10	0.27	9.89	1.05	3.27	- .45	.44
		930	0.00	3.26	24.96	71.78	0.26	9.90	1.04	3.28	- .45	.44
RC11-188	3319	0	0.00	0.36	26.27	73.37	0.26	9.39	1.48	2.24	+ .14	.55
		83	0.00	1.13	45.76	53.11	0.46	8.43	2.89	2.51	+ .17	.55
		316	0.00	2.57	50.37	47.06	0.52	8.05	3.75	2.80	+ .16	.50

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	Sk <sub>I</sub>	$K'_G$
								$\phi$	$\mu$			
RC11-188	3319	558	0.00	0.24	24.79	74.97	0.25	9.42	1.46	2.32	+ .21	.50
		1115	0.00	1.80	53.47	44.73	0.54	7.92	4.11	2.75	+ .17	.51
RC11-189	3922	0	0.00	0.00	50.95	49.05	0.51	8.72	2.36	2.58	+ .37	.46
		359	0.00	0.96	43.18	55.86	0.44	8.69	2.41	2.78	+ .09	.50
		472	0.00	0.00	91.24	8.76	0.91	6.42	11.62	1.09	+ .37	.60
		666	0.00	0.01	37.81	62.18	0.38	9.01	1.94	2.15	+ .29	.54
		789	0.00	0.00	86.20	13.80	0.86	6.63	10.09	1.29	+ .42	.64
		897	0.00	1.20	49.32	49.48	0.50	8.30	3.15	2.91	+ .19	.48
RC11-190	4254	0	0.00	0.00	21.58	78.42	0.22	9.96	1.00	2.27	+ .20	.44
		53	0.00	0.00	27.19	72.19	0.27	9.86	1.08	2.33	+ .14	.41
		71	0.00	0.00	87.10	12.90	0.87	6.81	8.91	1.25	+ .39	.67
		94	0.00	0.04	17.11	82.85	0.17	10.29	0.80	2.21	+ .04	.42
		110	0.00	0.06	90.32	9.62	0.90	6.47	11.28	1.20	+ .41	.69
		130	0.00	1.92	95.27	2.81	0.97	5.09	29.22	0.71	+ .19	.50

# GRAIN SIZE DATA

[illegible]



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
RC11-191	4387	0	0.00	0.00	16.75	83.27	0.17	10.24	2.16	+1.12	.44
		377	0.00	0.07	97.58	2.35	0.98	5.60	0.44	+1.67	.63
		453	0.00	76.40	21.65	1.95	0.92	3.28	1.04	+1.15	.54
		540	0.00	0.02	22.18	77.80	0.22	10.01	2.20	+1.17	.43
		682	0.00	1.63	84.44	13.93	0.86	5.54	1.94	+1.80	.69
		800	0.53	57.05	32.91	9.51	0.76	4.01	2.44	+1.46	.55
		866	0.00	62.30	29.16	8.54	0.77	3.78	1.92	+1.50	.65
RC11-192	4116	4	0.00	1.38	34.83	63.79	0.35	9.17	2.55	+1.12	.52
		210	0.00	0.77	31.38	67.85	0.32	9.50	2.49	+1.11	.46
RC11-193	4748	7	0.00	0.01	16.86	83.13	0.17	10.09	2.17	+1.19	.46
		1000	0.00	0.01	15.81	84.18	0.16	10.33	2.20	+1.07	.42
RC11-194	5303	0	0.00	0.00	15.14	84.86	0.15	10.17	2.12	+1.17	.45
		474	0.00	0.01	18.50	81.49	0.19	10.04	2.20	+1.14	.46
		846	0.00	0.05	19.83	80.02	0.20	9.82	2.30	+1.11	.51







GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
V20-68	5788	0	0.00	0.00	19.49	80.51	0.19	10.09	0.92	2.20	.45
		330	0.00	0.00	14.99	85.01	0.15	10.19	0.86	2.10	.44
V20-69	5351	36	0.27	0.95	43.85	55.93	0.44	8.39	2.98	2.41	.55
		560	0.00	0.26	26.45	73.29	0.27	9.06	1.86	1.76	.60
V20-70	5207	0	0.00	1.00	17.75	81.25	0.18	10.13	0.89	2.31	.47
		335	0.00	0.38	11.42	88.20	0.11	10.59	0.65	2.29	.48
V20-71	5302	0	0.00	0.01	17.16	82.83	0.17	10.20	0.85	2.45	.49
		20	0.00	0.10	12.69	87.21	0.13	10.50	0.69	2.14	.43
		460	0.00	0.28	12.20	87.52	0.12	10.63	0.63	2.15	.47
V20-72	4790	5	0.00	0.14	16.38	83.48	0.16	10.11	0.90	2.18	.46
		130	0.00	0.02	15.49	84.49	0.15	10.27	0.81	2.16	.44
		390	0.00	1.07	31.88	67.05	0.32	8.93	2.04	2.61	.53
V20-73	4773	0	0.00	1.45	14.64	83.91	0.15	10.22	0.83	2.14	.44
		55	0.00	1.30	31.40	67.30	0.32	9.20	1.70	2.60	.52



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
								$\phi$	$\mu$			
V20-74	3749	0	0.00	0.12	27.85	72.03	0.28	9.69	1.21	2.40	+1.14	.45
		620	0.00	18.73	75.40	5.87	0.93	5.22	26.83	1.50	+1.13	.56
		700	0.00	0.02	19.90	80.08	0.20	10.07	0.93	2.41	+1.07	.48
V20-75	1657	0	0.00	0.37	38.87	60.76	0.39	9.11	1.81	2.66	+1.16	.44
		420	0.00	0.13	39.90	59.97	0.40	9.02	1.92	2.78	+1.15	.43
V20-76	2628	0	0.00	0.01	24.82	75.17	0.25	9.79	1.13	2.43	+1.10	.47
		61	0.00	0.01	24.37	75.62	0.24	9.96	1.00	2.49	+1.04	.45
		83	0.00	0.03	77.48	22.49	0.78	6.69	9.68	1.81	+1.50	.54
		122	0.00	0.05	72.91	27.04	0.73	7.33	6.20	2.32	+1.63	.55
		145	0.00	2.66	91.89	5.45	0.94	4.83	34.90	0.97	+1.67	.70
		210	0.00	23.49	72.03	4.48	0.94	4.48	44.80	1.26	+1.43	.78
		296	0.00	0.79	91.01	8.20	0.92	5.33	24.80	1.29	+1.55	.65
		322	0.00	32.04	52.46	15.50	0.77	5.17	27.21	2.49	+1.64	.65
		356	0.00	91.12	6.01	2.87	0.68	2.89	134.90	0.92	+1.00	.63





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
V20-79	3711	0	0.00	0.10	29.33	70.57	0.29	9.46	1.41	2.46	.49
		219	0.00	0.06	35.24	64.70	0.35	9.22	1.67	2.46	.43
		228	0.00	0.00	46.02	53.98	0.46	8.92	2.06	2.50	.45
		260	0.00	1.70	45.27	53.03	0.46	8.60	2.57	2.59	.54
		666	0.00	0.00	58.56	41.44	0.59	8.19	3.40	2.62	.49
V20-80	3801	0	0.00	0.83	48.64	50.53	0.49	8.29	3.18	2.73	.52
		390	0.00	0.97	43.51	55.52	0.44	8.58	2.60	2.73	.51
		620	0.00	0.38	33.77	65.85	0.34	9.14	1.77	2.73	.46
V20-81	4232	0	0.00	1.15	36.70	62.15	0.37	9.33	1.55	2.61	.43
		33	0.00	0.01	84.80	15.19	0.85	6.99	7.83	1.32	.68
		42	0.00	0.23	92.82	6.95	0.93	5.83	17.53	1.22	.60
		78	0.00	0.08	91.03	8.89	0.91	5.85	17.29	1.35	.73
		85	0.00	0.25	91.41	8.34	0.92	6.29	12.72	1.40	.66
		119	0.00	0.33	90.40	9.27	0.91	5.39	23.73	1.37	.76





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\mu$	$\sigma_I$	$Sk_I$	$K'_G$
V20-83	4345	0	0.00	0.32	23.28	76.40	0.23	9.95	1.01	2.46	+0.05	.46
		43	0.00	0.60	65.03	34.37	0.65	7.72	4.71	2.62	+0.59	.50
		94	0.00	0.06	12.83	87.11	0.13	10.65	0.62	2.16	-0.07	.44
		114	0.00	0.08	42.31	57.61	0.42	9.18	1.72	2.54	+0.27	.44
		143	0.00	77.96	19.78	2.26	0.87	3.02	123.20	1.07	+0.16	.49
V20-84	4457	0	0.00	0.17	27.30	72.53	0.27	9.76	1.15	2.34	+0.15	.43
		115	0.00	0.04	86.43	13.53	0.86	6.97	7.95	1.00	+0.32	.60
		272	0.00	0.04	23.42	76.54	0.23	9.85	1.08	2.37	+0.11	.44
		292	0.00	0.01	68.48	31.51	0.68	7.94	4.06	2.03	+0.45	.61
		297	0.00	1.11	81.05	17.84	0.82	6.35	12.23	1.67	+0.44	.56
V20-85	3817	0	0.00	0.71	22.01	77.28	0.22	9.89	1.05	2.40	+0.08	.47
		350	0.00	0.48	20.06	79.46	0.20	10.04	0.95	2.35	+0.09	.45
		586	0.00	0.09	25.39	74.52	0.25	9.59	1.29	2.62	+0.10	.52
		650	0.00	0.45	15.49	84.06	0.16	9.55	1.33	1.92	+0.14	.67



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\frac{Mz}{\mu}$	$\sigma_I$	$Sk_I$	$K'_G$
V20-86	5138	0	0.00	0.07	15.91	84.02	0.16	10.26	0.81	2.23	+0.08	.45
		45	0.00	0.00	58.48	41.52	0.58	8.35	3.05	2.56	+0.52	.45
		57	0.00	0.32	96.38	3.30	0.97	5.50	22.04	0.62	+0.15	.51
		70	0.00	0.05	16.73	83.22	0.17	10.31	0.79	2.21	+0.06	.43
		82	0.00	2.26	60.54	37.20	0.62	7.07	7.40	3.13	+0.72	.41
		100	0.00	0.09	95.21	4.70	0.95	4.80	35.80	0.80	+0.52	.68
		107	0.00	0.00	15.71	84.29	0.16	10.25	0.82	2.15	+0.16	.43
		271	0.00	0.00	20.23	79.77	0.20	10.06	0.93	2.19	+0.15	.43
		761	0.00	0.01	50.64	49.36	0.51	8.84	2.17	2.15	+0.54	.50
		920	0.00	0.00	16.94	83.06	0.17	10.20	0.85	2.14	+0.14	.42
V20-87	4819	0	0.00	0.08	20.83	79.09	0.21	10.00	0.98	2.21	+0.14	.45
		340	0.00	0.01	17.80	82.19	0.22	9.22	1.67	2.34	+0.09	.46
		380	0.00	0.02	16.81	83.17	0.17	10.20	0.85	2.24	+0.12	.45
		639	2.73	2.79	36.48	58.00	0.39	9.08	1.84	3.19	+0.00	.46

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\frac{Mz}{\mu}$	$\tau_I$	$Sk_I$	$K'_G$
V20-88	5081	0	0.00	0.44	23.63	75.93	0.24	9.70	1.20	2.54	+0.06	.50
		835	0.00	0.00	36.30	63.70	0.36	8.54	2.68	3.34	-.11	.36
V20-89	5706	0	0.00	0.12	17.32	82.56	0.17	10.17	0.87	2.16	+0.16	.43
		780	0.00	0.00	15.42	84.58	0.15	10.52	0.68	2.52	-.17	.48
V20-90	5991	0	0.00	0.05	19.57	80.38	0.20	10.01	0.97	2.32	+0.10	.48
		390	0.00	0.02	17.62	82.36	0.18	10.29	0.80	2.35	+0.00	.45
		760	0.00	0.00	15.74	84.26	0.16	10.45	0.71	2.30	-.04	.40
V20-91	5863	0	0.00	0.01	20.44	79.55	0.20	9.97	0.99	2.24	+0.14	.46
		410	0.32	0.72	15.03	83.93	0.15	10.10	0.91	2.30	+0.13	.48
V20-92	5764	0	0.00	0.27	19.63	88.10	0.20	9.99	0.98	2.27	+0.14	.46
		417	0.00	0.01	20.05	79.94	0.20	10.12	0.90	2.37	+0.05	.45
		660	0.00	0.56	15.96	83.48	0.16	10.46	0.71	2.45	-.14	.47
V20-93	5797	0	0.00	0.03	21.95	78.02	0.22	9.92	1.03	2.33	+0.10	.46
		605	0.00	0.10	15.54	84.36	0.16	10.36	0.76	2.41	-.07	.50

## GRAIN SIZE DATA

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## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
V20-102	5216	10	0.00	0.02	26.65	73.33	0.27	7.77	4.57	2.30	+ .14	.55
		942	0.00	0.13	23.19	76.68	0.23	10.17	0.86	2.68	- .14	.47
V20-103	3442	0	0.00	1.37	41.13	57.50	0.42	8.71	2.37	2.86	+ .11	.48
		180	0.00	0.11	41.53	58.36	0.42	8.80	2.23	3.12	+ .03	.41
V20-104	5449	0	0.00	0.02	77.44	22.54	0.77	7.00	7.77	1.72	+ .37	.57
		100	0.00	0.08	28.87	77.05	0.23	10.26	0.82	2.37	- .05	.42
		1122	0.00	0.12	22.20	77.68	0.22	9.82	1.10	2.30	+ .16	.46
V20-105	5336	0	0.00	0.86	37.89	61.25	0.38	9.55	1.33	2.16	+ .27	.44
		40	0.00	0.01	28.26	71.73	0.28	9.47	1.40	2.39	+ .18	.47
		1181	0.00	0.06	26.22	73.72	0.26	9.52	1.36	2.41	+ .20	.48
V20-107	5872	0	0.00	1.15	27.20	71.65	0.28	9.65	1.24	2.49	+ .09	.47
		70	0.00	0.55	27.28	72.17	0.27	9.62	1.27	2.47	+ .10	.49
		895	0.00	0.35	94.54	5.11	0.95	5.45	22.82	1.11	+ .46	.53
		1270	0.00	0.16	35.62	64.22	0.36	9.37	1.51	2.47	+ .23	.45



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$S_{k_I}$	$K'_G$
V20-118	5360	0	0.00	1.27	38.25	60.48	0.39	8.89	2.70	+1.10	.53
		82	0.00	2.36	35.59	62.05	0.36	9.11	2.88	+0.06	.48
		150	0.00	1.37	30.01	68.62	0.30	9.45	2.71	+0.08	.47
		920	0.00	0.23	17.79	81.98	0.18	10.35	2.25	+0.00	.43
V20-119	2739	0	0.00	2.54	67.37	30.09	0.69	6.73	2.30	+0.42	.50
		230	0.00	1.80	33.03	65.17	0.34	9.20	2.81	+0.04	.46
		657	0.00	1.89	65.19	32.92	0.66	6.95	2.96	+0.48	.45
		746	0.00	2.02	84.30	13.68	0.86	6.19	1.54	+0.25	.55
		947	0.00	1.98	58.93	39.09	0.60	7.14	2.02	+0.04	.48
		986	2.08	29.82	49.93	18.17	0.73	5.37	2.98	+0.34	.54
		1120	0.00	6.94	42.69	50.37	0.46	8.10	2.58	+0.06	.54
V20-120	6216	0	0.00	0.93	38.37	60.70	0.39	8.86	2.63	+0.16	.49
		300	0.00	1.21	48.84	49.95	0.49	7.95	3.08	+0.10	.47
		450	0.17	12.72	83.25	3.86	0.96	4.75	0.92	+0.22	.69



# GRAIN SIZE DATA

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GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
V20-122	5563	0	0.00	0.24	40.58	59.18	0.41	8.83	2.19	2.58	+1.12	.54
		1053	0.00	30.36	59.97	9.67	0.86	4.99	31.30	1.69	+5.54	.53
		1297	0.00	42.23	51.47	6.30	0.89	4.69	38.70	1.64	+4.42	.52
		1420	0.00	1.12	46.30	52.58	0.47	8.47	2.82	2.85	+1.13	.48
		1525	0.00	1.60	85.88	12.52	0.87	6.04	15.19	1.42	+4.41	.56
V20-123	4903	0	0.00	0.74	44.57	54.69	0.45	8.61	2.55	2.52	+1.15	.52
		686	0.00	6.23	84.75	9.02	0.90	5.92	16.43	1.41	+2.22	.53
		779	0.00	15.99	76.15	7.86	0.91	5.54	21.49	1.58	+1.13	.50
		1121	0.00	1.84	90.41	7.75	0.92	6.20	13.53	1.33	+1.15	.55
		1320	0.00	1.36	39.92	58.72	0.40	8.27	3.22	2.21	+0.05	.57
		1340	0.00	37.04	59.14	3.82	0.94	4.56	42.30	1.34	+2.26	.51
V20-124	5534	0	0.00	2.38	45.43	52.19	0.47	8.49	2.77	2.79	+1.17	.49
		646	0.00	15.01	80.24	4.75	0.94	4.98	31.50	1.17	+2.28	.60
		830	0.00	1.21	48.42	50.37	0.49	8.30	3.17	2.82	+1.14	.49

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
V20-125	5545	0	0.00	0.14	43.75	56.11	0.44	8.64	2.36	+1.18	.54
		433	0.00	22.03	71.55	6.42	0.92	5.38	1.85	-.23	.54
		726	0.00	2.85	86.39	10.76	0.89	6.11	1.35	+2.27	.55
		750	0.00	21.12	72.46	6.42	0.92	5.11	1.67	+2.26	.60
		928	0.00	1.68	42.37	55.95	0.43	8.74	2.87	+1.14	.45
V20-126	5515	0	0.00	0.57	37.30	62.13	0.38	8.94	2.46	+1.17	.51
		80	0.00	15.23	73.31	11.46	0.86	5.83	1.76	+0.06	.51
		573	0.00	0.82	84.19	14.99	0.85	6.31	1.60	+2.30	.56
		596	0.00	30.22	64.86	4.92	0.93	4.83	1.39	+2.24	.52
		763	0.00	53.54	39.92	6.54	0.86	4.31	1.69	+2.52	.54
		1020	0.00	1.22	45.21	53.57	0.46	8.48	2.84	+2.14	.50
V20-127	5583	0	0.00	0.36	38.28	61.36	0.38	9.08	2.61	+2.13	.53
		537	0.00	47.22	48.27	4.51	0.91	4.40	1.47	+2.38	.51
		661	0.00	23.52	68.46	8.02	0.90	5.31	1.71	+2.03	.53
		1130	0.00	0.17	30.63	69.20	0.31	9.49	2.43	+2.18	.48





# GRAIN SIZE DATA

[illegible]



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\mu$	$\sigma_I$	$Sk_I$	$K'_G$
V21-59	2992	0	0.00	1.96	43.82	54.22	0.45	8.87	2.13	2.89	+1.10	.42
		160	0.00	.49	63.92	35.59	0.64	6.90	8.35	2.59	+4.46	.45
		180	0.00	29.34	51.98	18.68	0.74	5.32	24.97	2.97	+3.31	.56
		367	0.00	1.63	68.02	30.35	0.69	7.00	7.81	2.47	+3.36	.52
V21-60	3751	0	0.00	1.52	51.14	47.34	0.52	8.35	3.05	2.84	+2.25	.46
		62	0.00	1.14	48.88	49.98	0.49	8.28	3.20	2.86	+1.19	.47
		84	0.00	36.14	47.31	16.55	0.74	5.25	26.15	2.82	+2.50	.57
		134	0.00	2.76	58.21	39.03	0.60	7.59	5.19	2.73	+3.35	.47
		188	0.00	0.75	59.78	39.47	0.60	7.55	5.32	2.81	+4.42	.47
		211	0.00	73.04	18.58	8.38	0.69	3.48	89.20	1.94	+4.47	.74
		295	0.00	0.44	57.78	41.78	0.58	7.89	4.20	2.64	+3.31	.48
V21-61	4583	0	0.00	0.39	37.24	62.37	0.37	9.02	1.92	2.70	+1.13	.45
		100	0.00	0.22	38.12	61.66	0.38	9.02	1.92	2.74	+2.09	.47
		220	0.00	0.05	64.49	35.46	0.65	7.30	6.33	2.18	+2.20	.55

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-61	4583	274	2.18	83.25	12.83	1.74	0.88	2.35	196.10	1.60	+26	.64
		312	0.00	0.21	45.29	54.50	0.45	8.56	2.63	2.46	+19	.52
		400	0.00	0.09	49.35	50.38	0.50	8.10	3.64	2.29	+14	.53
		478	0.00	0.09	65.11	34.80	0.65	7.52	5.42	1.81	+32	.56
		519	0.00	2.14	96.24	1.62	0.98	4.81	35.40	0.43	+35	.68
		545	0.00	0.08	69.96	29.96	0.70	7.30	6.31	2.03	+37	.58
		553	0.00	1.03	92.64	6.33	0.94	5.37	24.06	1.14	+46	.57
		581	0.00	0.08	64.19	35.73	0.64	7.48	5.58	1.97	+27	.53
V21-62	4625	0	0.00	0.02	48.56	51.42	0.49	8.90	2.08	2.74	+46	.45
		54	0.00	41.57	43.86	14.57	0.75	5.07	29.76	2.49	+39	.49
		248	0.00	22.71	52.18	25.11	0.68	6.08	14.78	2.92	+56	.50
		500	0.00	0.13	47.92	51.95	0.48	8.61	2.55	2.64	+26	.47
V21-63	4674	0	0.00	0.02	16.91	83.07	0.17	9.98	0.99	2.20	+22	.47
		495	0.00	0.14	17.65	82.21	0.18	9.86	1.08	2.10	+23	.48





## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K <sub>G</sub> '
								$\phi$	$\mu$			
V21-70	5954	0	0.00	0.00	20.36	79.64	0.20	9.89	1.05	2.35	+1.11	.45
		640	0.00	0.08	8.56	91.36	0.09	10.96	0.50	2.11	-.16	.48
V21-71	5954	0	0.43	0.03	25.10	74.44	0.25	9.67	1.22	2.49	+1.10	.48
V21-72	5369	12	0.38	0.31	30.24	69.07	0.30	9.49	1.39	2.77	-.02	.47
		174	0.00	0.29	17.35	82.36	0.17	10.12	0.89	2.50	.00	.51
V21-73	5872	0	0.00	0.21	25.51	74.28	0.26	9.70	1.20	2.39	+1.16	.46
		933	0.00	0.12	19.60	80.28	0.20	10.13	0.89	2.33	+1.08	.44
V21-74	6015	0	0.00	0.44	27.26	72.30	0.27	9.54	1.34	2.42	+1.13	.47
		446	0.00	11.40	80.36	8.24	0.91	5.43	23.08	1.45	+1.30	.51
		893	0.00	0.53	27.57	71.90	0.28	9.61	1.28	2.55	+1.12	.47
V21-75	6119	0	0.00	0.62	30.21	69.17	0.30	9.33	1.55	2.53	+1.18	.48
		137	0.00	0.66	64.09	35.25	0.65	7.33	6.21	2.55	+1.36	.50
		357	0.00	1.47	87.45	11.08	0.89	6.02	15.40	1.39	+1.45	.54
		805	0.00	0.10	24.90	75.00	0.25	9.79	1.13	2.42	+1.10	.44



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K' <sub>G</sub>
								$\phi$	$\mu$			
V21-76	5916	0	0.00	1.26	45.66	53.08	0.46	8.55	2.66	2.84	+16	.48
		130	0.00	8.98	77.50	13.52	0.85	6.03	15.30	1.77	+21	.55
		458	0.00	0.88	85.36	13.76	0.86	6.43	11.57	1.35	+17	.55
		628	0.00	9.76	68.38	21.86	0.76	6.30	12.63	1.90	+15	.47
		860	0.00	0.11	32.60	67.29	0.33	9.35	1.53	2.46	+22	.47
V21-78	1106	0	0.66	88.07	7.47	3.80	0.66	0.80	571.00	1.62	+49	.76
		450	7.69	92.31	0.00	0.00	0.00	0.53	689.00	0.86	-.29	.60
		900	6.73	91.62	0.57	1.08	0.35	0.35	782.00	0.86	-.06	.55
V21-85	1684	17	0.00	73.16	15.41	11.43	0.57	3.51	87.70	2.37	+61	.63
		270	0.00	70.26	16.27	13.47	0.55	3.74	74.40	2.68	+59	.66
V21-86	5717	0	0.00	2.28	26.36	71.36	0.27	8.88	2.11	2.83	+14	.49
		370	0.00	30.45	62.49	7.06	0.90	4.87	34.00	1.63	+36	.52
		380	0.00	12.77	77.25	9.98	0.88	5.66	19.77	1.64	+21	.52
		560	0.00	19.98	71.35	8.67	0.89	5.25	26.15	1.70	+36	.55
		661	0.00	3.61	36.55	59.84	0.38	8.94	2.03	2.92	+04	.47



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\epsilon_I$	Sk <sub>I</sub>	K <sub>G</sub> <sup>1</sup>
								$\phi$	$\mu$			
V21-91	5128	0	0.00	0.88	73.51	25.61	0.74	6.90	8.33	2.13	+ .40	.56
		13	0.00	0.48	86.19	13.33	0.87	5.82	17.70	1.60	+ .52	.57
		165	0.00	1.26	56.29	42.45	0.57	7.69	4.82	2.40	+ .24	.51
		215	0.00	0.87	78.88	20.25	0.80	6.91	8.31	1.55	+ .36	.59
		222	0.00	0.50	83.61	15.89	0.84	6.29	12.77	1.54	+ .32	.51
		360	0.00	0.70	50.18	49.12	0.50	8.02	3.84	2.34	+ .14	.51
V21-92	4283	0	0.00	1.93	61.49	36.58	0.63	7.52	5.44	2.51	+ .31	.53
V21-93	2878	0	0.00	42.11	52.13	5.76	0.90	4.15	56.30	1.37	+ .29	.71
		70	0.00	71.00	25.73	3.27	0.89	3.51	87.50	0.97	+ .17	.56
		100	0.00	51.33	30.74	17.93	0.63	4.45	45.60	3.48	+ .34	.47
		126	0.00	0.63	61.03	38.34	0.61	7.51	5.47	2.74	+ .39	.48
V21-139	6009	0	0.00	0.60	50.76	48.64	0.51	8.30	3.17	2.57	+ .29	.44
		60	0.00	0.15	27.86	71.99	0.28	9.44	1.43	2.50	+ .14	.48
		309	0.59	78.53	12.94	7.94	0.60	3.06	119.60	2.02	+ .51	.68



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-139	6009	637	0.00	0.01	67.39	32.60	0.67	7.46	5.67	1.92	+46	.56
		647	0.02	1.23	69.75	29.00	0.71	7.14	7.05	2.11	+48	.54
		1135	0.00	0.19	31.32	68.49	0.31	9.39	1.49	2.38	+20	.48
V21-140	5949	0	0.00	0.70	34.62	64.68	0.35	9.13	1.78	2.71	+12	.47
		160	0.00	0.39	82.35	17.26	0.83	6.38	11.97	1.72	+44	.56
		397	0.00	20.71	64.08	15.21	0.81	5.65	19.82	2.35	+28	.63
		421	0.00	0.67	27.01	72.32	0.27	9.44	1.43	2.68	+03	.48
V21-141	5821	0	0.00	1.97	44.18	53.85	0.45	8.10	3.62	3.28	+01	.44
		555	0.00	0.42	40.91	58.67	0.41	8.85	2.15	2.47	+26	.48
V21-142	4241	0	0.00	0.63	34.44	64.93	0.35	9.31	1.58	2.69	+11	.46
		471	0.00	0.93	89.37	9.70	0.90	5.51	21.84	1.37	+64	.61
		870	0.00	0.94	50.20	48.86	0.51	8.16	3.48	2.69	+19	.49
V21-143	3592	0	0.39	29.01	36.39	34.21	0.51	6.34	12.28	3.34	-.04	.46
		32	3.29	6.47	42.16	48.08	0.47	7.45	5.70	2.60	-.26	.67



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
V21-144	4931	0	0.00	0.05	23.37	76.58	0.23	9.62	2.51	+1.18	.48
V21-145	6088	0	0.18	0.06	30.27	69.49	0.30	9.21	2.39	+1.17	.53
		812	0.00	2.38	89.00	8.62	0.91	5.58	1.43	+1.47	.49
		1200	0.00	0.46	27.66	71.88	0.28	9.65	2.65	+1.05	.46
V21-146	3968	0	0.00	0.95	33.93	65.12	0.34	8.97	2.68	+1.04	.50
		92	0.00	7.21	33.98	58.81	0.37	8.84	2.91	+1.04	.49
		308	0.00	1.48	44.63	53.89	0.45	8.58	2.68	+1.14	.55
		825	0.00	1.27	43.40	55.33	0.44	8.64	2.86	+1.09	.47
		1175	0.00	1.69	26.41	71.90	0.43	9.23	2.31	+1.15	.55
V21-147	5256	0	0.00	0.08	32.10	69.82	0.32	9.45	2.43	+1.17	.49
		180	0.00	30.18	62.93	6.89	0.68	4.91	1.63	+1.41	.50
		251	0.00	0.50	26.21	73.29	0.26	9.67	2.47	+1.15	.47
		500	0.00	0.45	26.27	73.28	0.26	9.66	2.50	+1.07	.45
		751	0.00	0.17	24.03	75.80	0.24	9.89	2.43	+1.11	.45



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\sigma_I$	$Sk_I$	$K'_G$
V21-150	5416	0	0.00	1.88	34.77	63.35	0.35	8.85	2.55	+0.07	.55
		481	0.00	1.85	56.44	41.71	0.58	7.51	2.23	+0.05	.54
		504	0.00	2.23	76.44	21.33	0.78	6.56	1.92	+0.29	.53
		1140	0.00	1.82	51.03	47.15	0.52	8.10	2.66	+0.21	.50
V21-151	5055	0	0.00	2.06	47.58	50.36	0.49	8.26	3.05	+0.13	.45
		142	12.37	31.15	41.34	15.14	0.73	4.78	3.76	+0.09	.64
		254	0.00	0.36	83.19	16.45	0.83	6.44	1.63	+0.32	.56
		545	0.00	1.71	82.45	15.84	0.84	6.62	1.40	+0.21	.55
V21-166	7103	0	0.00	0.24	37.87	61.89	0.38	9.20	2.68	+0.12	.45
		152	0.00	0.01	30.72	69.27	0.31	9.60	2.52	+0.09	.43
		216	0.00	0.21	82.42	17.37	0.83	6.35	1.85	+0.73	.59
		349	0.00	83.43	8.74	7.83	0.53	3.17	1.76	+0.45	.76
		460	0.05	75.77	19.07	5.11	0.79	3.01	1.59	+0.45	.59
		505	0.10	48.31	31.33	20.26	0.61	5.16	3.35	+0.34	.46



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\frac{Mz}{\mu}$	$\sigma_I$	$Sk_I$	$K'_G$
V21-167	6909	0	0.00	27.08	63.79	9.13	0.87	4.81	35.60	1.73	+ .70	.73
		37	0.00	4.93	88.58	6.49	0.93	5.33	24.80	1.23	+ .43	.49
		63	0.00	45.22	29.56	25.22	0.54	5.84	17.41	3.13	+ .06	.44
		78	0.00	27.91	67.57	4.52	0.94	4.32	49.90	1.05	+ .21	.68
V21-170	7011	0	0.00	1.54	42.45	56.01	0.43	8.93	2.05	2.79	+ .13	.48
		28	0.00	42.41	55.92	1.67	0.97	4.00	62.50	0.69	- .13	.55
		158	0.00	16.37	79.18	4.45	0.95	4.74	37.40	1.30	+ .37	.75
		179	0.00	0.04	19.52	80.44	0.20	10.16	0.87	2.25	+ .10	.43
		238	0.00	47.37	51.61	1.02	0.98	3.95	64.40	0.58	- .08	.53
V21-171	5013	0	0.00	0.71	72.78	26.51	0.73	6.99	7.84	2.21	+ .47	.57
		10	0.00	34.59	51.25	14.16	0.78	5.34	24.68	2.38	+ .33	.51
		190	0.00	1.74	45.16	53.10	0.46	8.32	3.12	2.95	+ .09	.47
		253	0.00	26.01	66.38	7.61	0.90	5.01	31.00	1.91	+ .50	.61
		412	0.00	21.77	70.79	7.44	0.90	4.86	34.40	1.47	+ .43	.61



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\sigma_I$	Sk <sub>I</sub>	K <sub>G</sub> <sup>'</sup>
								$\phi$	$\mu$			
V21-171	5013	596	21.97	72.74	4.28	1.01	0.81	0.07	950.00	2.72	-.51	.58
		711	0.00	2.11	54.35	43.54	0.56	6.13	14.27	1.55	+.42	.62
		822	0.00	0.59	87.11	12.30	0.88	8.02	3.85	2.77	+.25	.45
		838	0.00	38.04	55.35	6.61	0.89	4.41	47.00	1.50	+.33	.70
		846	0.00	36.79	47.74	15.47	0.76	5.25	26.27	2.61	+.40	.55
V21-172	5198	0	0.00	12.24	66.40	21.36	0.76	6.24	13.16	2.17	+.26	.50
		50	0.00	1.89	44.31	53.80	0.45	8.74	2.32	2.91	+.06	.47
		268	0.00	1.90	85.80	12.30	0.87	6.11	14.47	1.36	+.46	.52
		278	0.00	35.37	58.86	5.77	0.91	4.78	36.20	1.61	+.35	.48
		579	0.00	29.38	65.29	5.33	0.92	4.77	36.60	1.43	+.40	.53
		602	0.00	1.63	32.27	66.10	0.33	9.03	1.90	2.84	+.01	.51
		1032	0.00	1.21	63.54	35.25	0.64	7.32	6.25	2.57	+.32	.49
		1069	0.00	53.63	42.39	3.98	0.91	4.08	58.90	1.43	+.33	.55
		1080	0.00	53.25	41.38	5.37	0.89	4.25	52.30	1.65	+.48	.51

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	Mz		$\epsilon_I$	Sk <sub>I</sub>	K <sub>G</sub> '
								$\phi$	$\mu$			
V21-173	5493	0	0.00	1.40	25.51	73.09	0.26	8.64	2.50	2.51	+ .14	.46
		210	0.00	1.73	88.70	9.57	0.90	5.89	16.78	1.45	+ .32	.54
		724	0.00	19.46	73.69	6.85	0.91	5.36	24.29	1.69	+ .16	.55
		812	0.00	22.76	73.48	3.76	0.95	4.76	36.90	1.25	+ .34	.54
		1182	0.00	1.19	48.18	50.63	0.49	8.58	2.61	2.46	+ .31	.50
V21-174	5691	0	0.00	0.09	20.23	79.68	0.20	10.03	0.95	2.35	+ .09	.45
		1001	0.00	0.19	17.27	82.54	0.17	9.06	1.87	1.51	+ .12	.65
V21-175	5654	10	0.00	0.01	21.96	78.03	0.22	9.78	1.14	2.28	+ .15	.48
		102	0.00	0.02	19.09	80.89	0.19	9.92	1.03	2.19	+ .22	.45
		201	0.00	0.13	22.85	77.02	0.23	9.77	1.14	2.26	+ .17	.48
		301	0.00	0.00	19.71	80.92	0.20	9.88	1.06	2.19	+ .23	.47
		400	0.00	0.00	16.88	83.12	0.17	10.10	0.91	2.20	+ .17	.45
		497	0.00	0.00	17.64	82.36	0.18	9.98	0.99	2.31	+ .13	.43
		579	0.00	0.08	17.86	82.06	0.18	10.07	0.93	2.22	+ .16	.46

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-175	5654	648	0.00	0.00	17.23	82.77	0.17	10.02	0.96	2.27	+ .17	.48
		699	0.00	0.00	17.05	82.95	0.17	10.15	0.88	2.29	+ .09	.46
		801	0.00	0.02	16.38	83.60	0.16	10.15	0.88	2.27	+ .10	.46
		901	0.00	0.07	22.62	77.31	0.23	9.69	1.21	2.72	+ .01	.53
		998	0.00	0.00	21.85	78.15	0.22	9.69	1.21	2.21	+ .22	.49
		1098	0.00	0.03	16.81	83.16	0.17	10.06	0.94	2.22	+ .16	.49
V21-176	5621	0	0.00	0.03	18.03	81.94	0.18	10.03	0.96	2.34	+ .11	.48
		670	0.00	2.59	12.75	84.66	0.13	10.56	0.66	2.53	- .20	.50
		727	0.00	1.36	34.77	63.87	0.35	9.63	1.26	3.07	- .24	.40
V21-177	6022	5	0.00	0.00	16.44	83.56	0.16	10.00	0.97	2.11	+ .27	.45
		101	0.00	0.00	17.52	82.48	0.18	10.01	0.97	2.23	+ .17	.47
		201	0.00	0.01	16.81	83.18	0.17	10.18	0.86	2.21	+ .14	.44
		301	0.00	0.05	15.54	84.41	0.16	10.22	0.83	2.18	+ .13	.45
		401	0.00	0.34	18.69	80.97	0.19	10.10	0.91	2.65	- .06	.52



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core (cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi}$	$\mu$	$\sigma_I$	$Sk_I$	$K'_G$
V21-177	6022	501	0.00	0.72	10.25	89.03	0.10	10.50	0.69	2.16	+0.01	.44
		601	0.00	0.13	16.29	83.71	0.16	10.25	0.82	2.31	+0.01	.49
		701	0.00	0.15	19.94	79.91	0.20	9.74	1.17	2.28	+0.26	.48
		801	0.00	0.13	21.28	78.59	0.21	10.11	0.90	2.49	-.05	.46
		901	0.00	0.17	27.60	72.23	0.28	9.34	1.54	2.33	+0.19	.50
		1001	0.00	0.05	12.35	87.60	0.12	10.74	0.58	2.18	-.11	.47
V21-178	5720	0	0.00	0.27	24.85	74.88	0.25	9.64	1.25	2.41	+0.17	.46
		11	0.00	0.00	20.63	79.37	0.21	9.89	1.05	2.31	+0.16	.48
		101	0.00	0.00	18.37	81.63	0.18	10.00	0.97	2.26	+0.18	.47
		201	0.00	0.01	17.77	82.22	0.18	10.03	0.96	2.23	+0.18	.46
		304	0.00	0.03	26.51	73.46	0.27	9.54	1.34	2.86	-.03	.50
		401	0.00	0.19	15.76	84.05	0.16	10.21	0.84	2.21	+0.13	.45
		504	0.00	0.18	12.95	86.87	0.13	10.44	0.72	2.29	+0.04	.47
		601	0.00	0.10	17.93	81.97	0.18	9.96	1.00	2.45	+0.04	.53



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-178	5720	701	0.00	0.24	29.52	70.24	0.30	9.14	1.76	2.66	+1.12	.46
		780	0.00	0.00	17.11	82.89	0.17	10.38	0.75	2.42	-.08	.49
V21-179	5771	0	0.00	0.03	16.59	83.38	0.17	10.16	0.87	2.35	+0.08	.48
		650	0.00	0.00	16.92	83.08	0.17	10.02	0.96	2.20	+1.12	.53
V21-180	5676	0	0.00	0.01	15.46	84.47	0.15	10.30	0.79	2.22	+1.10	.44
		940	0.00	0.02	11.22	88.76	0.11	10.58	0.65	2.12	+0.03	.46
V21-181	5302	0	3.97	0.06	15.00	80.97	0.16	10.07	0.93	2.37	+0.06	.47
		800	0.00	2.26	15.93	81.81	0.16	10.35	0.76	2.42	-.12	.47
V21-182	5824	4	0.00	0.03	15.59	84.38	0.16	10.06	0.93	2.14	+1.19	.45
		81	0.00	0.01	15.27	84.72	0.15	10.14	0.88	2.13	+1.18	.46
		161	0.00	0.01	13.88	86.11	0.14	10.19	0.86	2.06	+1.23	.44
		261	0.00	0.02	15.60	84.38	0.16	10.13	0.89	2.09	+1.20	.45
		361	0.00	0.08	13.73	86.19	0.14	10.17	0.87	2.08	+1.21	.46
		461	0.00	0.01	13.41	86.58	0.13	10.25	0.82	2.07	+1.18	.44

# GRAIN SIZE DATA

[illegible]

## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{M_z}{\phi}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-184	4804	0	0.00	0.05	22.17	77.78	0.22	9.88	1.06	2.34	+ .13	.46
		92	0.00	0.05	22.69	77.26	0.23	9.88	1.06	2.35	+ .11	.45
		121	1.45	3.39	18.38	76.78	0.19	9.73	1.17	2.56	+ .05	.51
		191	6.93	7.40	15.43	70.24	0.18	9.12	1.79	3.93	- .24	.62
		302	0.00	0.21	18.22	81.57	0.18	10.09	0.92	2.16	+ .18	.45
V21-185	4857	0	0.00	1.46	74.10	24.44	0.75	6.75	9.24	2.14	+ .50	.55
		20	0.00	0.87	85.59	13.54	0.86	6.00	15.62	1.67	+ .45	.61
		35	0.00	0.11	53.22	46.67	0.53	8.01	3.86	1.75	+ .17	.53
		50	0.00	0.30	64.28	35.42	0.64	7.42	5.82	2.08	+ .32	.52
		66	0.00	0.53	81.99	17.48	0.82	6.38	12.00	1.76	+ .48	.54
		80	0.00	0.29	84.75	14.96	0.85	6.16	13.92	1.86	+ .45	.65
V21-187	3762	0	0.00	1.58	50.84	47.58	0.52	8.45	2.84	2.88	+ .28	.44
		94	0.00	0.53	57.00	42.47	0.57	8.12	3.57	2.77	+ .33	.47
		108	0.00	16.24	62.90	20.86	0.75	6.08	14.74	2.74	+ .67	.58



## GRAIN SIZE DATA

Core No.	Depth (m)	Depth in Core(cm)	% Gravel	% Sand	% Silt	% Clay	$\frac{z}{z+c}$	$\frac{Mz}{\phi \quad \mu}$		$\sigma_I$	$Sk_I$	$K'_G$
V21-187	3762	122	0.00	38.16	46.43	15.41	0.75	5.08	29.42	2.76	+ .51	.55
		128	0.00	0.55	57.23	42.22	0.58	8.01	3.87	2.78	+ .30	.48
		201	0.00	2.61	37.74	59.65	0.39	7.95	4.04	2.86	+ .25	.46
		247	0.00	0.35	55.78	43.87	0.56	8.09	3.66	2.55	+ .31	.50
		265	0.00	4.11	64.71	31.18	0.67	6.93	8.18	2.93	+ .60	.45
		290	0.00	57.20	30.97	11.83	0.72	4.20	54.20	2.48	+ .51	.66
		294	0.00	0.84	60.78	38.38	0.61	7.93	4.08	2.75	+ .35	.46
		400	0.00	0.77	50.32	48.91	0.51	8.54	2.68	3.02	+ .16	.42
		500	0.00	2.76	46.32	50.92	0.48	8.49	2.77	3.12	+ .29	.42
		600	0.00	3.25	47.77	48.98	0.49	8.08	3.68	2.73	+ .18	.48
		700	0.00	8.43	49.08	42.49	0.54	7.60	5.15	3.17	+ .16	.50
V21-187	3762	800	0.00	2.19	63.20	34.61	0.65	7.09	7.30	2.75	+ .31	.47
		902	0.08	4.60	69.96	25.36	0.73	6.71	9.48	2.56	+ .52	.53
		930	0.98	3.73	68.91	26.38	0.72	6.76	9.22	2.60	+ .45	.51







## APPENDIX C

TABLE USED TO PREDICT SOUND VELOCITY AND WET DENSITY  
OF LAYERS FROM MEAN GRAIN SIZE OF SEDIMENT





MEAN GRAIN SIZE WET DENSITY AND EQUIVALENT SOUND VELOCITIES

m/sec	Velocity		Mean Size $\mu$	Wet Density g/cc	Velocity		Mean Size $\mu$	Wet Density g/cc
	ft/sec	m/sec			ft/sec	m/sec		
1487.6	4881	1601.2	>.75	1.16-1.42	5253	1601.2	21.0	1.90
1487.6	4881	1604.1	.75	1.42-1.45	5263	1604.1	22.0	1.91
1494.1	4902	1607.1	1.0	1.52	5273	1607.1	23.0	1.91
1499.0	4918	1609.9	1.25	1.57	5282	1609.9	24.0	1.91
1503.0	4931	1612.7	1.50	1.60	5291	1612.7	25.0	1.92
1506.5	4943	1615.4	1.75	1.62	5300	1615.4	26.0	1.93
1509.6	4953	1618.1	2.0	1.64	5309	1618.1	27.0	1.93
1515.0	4970	1620.7	2.50	1.67	5317	1620.7	28.0	1.93
1519.7	4986	1623.2	3.0	1.68	5325	1623.2	29.0	1.94
1523.9	5000	1625.8	3.50	1.70	5334	1625.8	30.0	1.94
1527.7	5012	1628.2	4.0	1.72	5342	1628.2	31.0	1.95
1534.6	5035	1630.6	5.0	1.74	5350	1630.6	32.0	1.95
1540.8	5055	1633.0	6.0	1.76	5358	1633.0	33.0	1.96
1546.4	5073	1635.3	7.0	1.77	5365	1635.3	34.0	1.96
1551.7	5091	1637.6	8.0	1.79	5373	1637.6	35.0	1.96
1556.6	5107	1639.9	9.0	1.80	5380	1639.9	36.0	1.97
1561.2	5122	1642.1	10.0	1.81	5387	1642.1	37.0	1.97
1565.6	5136	1644.3	11.0	1.82	5395	1644.3	38.0	1.97
1569.8	5150	1646.5	12.0	1.83	5402	1646.5	39.0	1.98
1573.8	5163	1648.6	13.0	1.84	5409	1648.6	40.0	1.98
1577.6	5176	1650.7	14.0	1.85	5416	1650.7	41.0	1.98
1581.3	5188	1652.7	15.0	1.86	5422	1652.7	42.0	1.98
1584.9	5200	1654.8	16.0	1.87	5429	1654.8	43.0	1.99
1588.3	5211	1656.8	17.0	1.88	5436	1656.8	44.0	1.99
1591.7	5222	1658.8	18.0	1.88	5442	1658.8	45.0	1.99
1594.2	5230	1660.7	19.0	1.89	5448	1660.7	46.0	2.00
1598.1	5243	1662.7	20.0	1.90	5455	1662.7	47.0	2.00

Velocity		Mean Size $\mu$	Wet Density g/cc	Velocity		Mean Size $\mu$	Wet Density g/cc
m/sec	ft/sec			m/sec	ft/sec		
1664.6	5461	48.0	2.00	1711.8	5616	77.0	2.07
1666.4	5467	49.0	2.01	1713.3	5621	78.0	2.07
1668.3	5473	50.0	2.01	1714.7	5626	79.0	2.07
1670.1	5479	51.0	2.01	1716.1	5630	80.0	2.07
1672.0	5486	52.0	2.01	1717.4	5635	81.0	2.07
1673.7	5491	53.0	2.01	1718.8	5639	82.0	2.07
1675.5	5497	54.0	2.02	1720.2	5644	83.0	2.08
1677.3	5503	55.0	2.02	1721.5	5648	84.0	2.08
1679.0	5509	56.0	2.02	1722.9	5653	85.0	2.08
1680.7	5514	57.0	2.03	1724.2	5657	86.0	2.08
1682.4	5520	58.0	2.03	1725.5	5661	87.0	2.08
1684.1	5525	59.0	2.03	1726.8	5665	88.0	2.09
1685.8	5531	60.0	2.03	1728.2	5670	89.0	2.09
1687.4	5536	61.0	2.03	1729.5	5674	90.0	2.09
1689.1	5542	62.0	2.04	1730.7	5678	91.0	2.09
1690.7	5547	63.0	2.04	1732.0	5682	92.0	2.09
1692.3	5552	64.0	2.04	1733.3	5687	93.0	2.09
1693.9	5557	65.0	2.04	1734.5	5691	94.0	2.09
1695.4	5562	66.0	2.04	1735.8	5695	95.0	2.10
1697.0	5568	67.0	2.05	1737.0	5699	96.0	2.10
1698.5	5573	68.0	2.05	1738.3	5703	97.0	2.10
1700.1	5578	69.0	2.05	1739.5	5707	98.0	2.10
1701.6	5583	70.0	2.05	1740.7	5711	99.0	2.10
1703.1	5588	71.0	2.06	1741.9	5715	100.0	2.10
1704.6	5593	72.0	2.06	1743.1	5719	101.0	2.10
1706.1	5597	73.0	2.06	1744.3	5723	102.0	2.10
1707.5	5602	74.0	2.06	1745.5	5727	103.0	2.10
1709.0	5607	75.0	2.06	1746.7	5731	104.0	2.11
1710.4	5612	76.0	2.06	1747.9	5735	105.0	2.11

Velocity		Mean Size μ	Wet Density g/cc	Velocity		Mean Size μ	Wet Density g/cc
m/sec	ft/sec			m/sec	ft/sec		
1749.1	5739	106.0	2.11	1780.3	5841	135.0	2.14
1750.2	5742	107.0	2.11	1781.3	5844	136.0	2.14
1751.4	5746	108.0	2.11	1782.2	5847	137.0	2.15
1752.5	5750	109.0	2.11	1783.2	5850	138.0	2.15
1753.7	5754	110.0	2.11	1784.2	5854	139.0	2.15
1754.8	5757	111.0	2.12	1785.2	5857	140.0	2.15
1755.9	5761	112.0	2.12	1786.2	5860	141.0	2.15
1757.0	5764	113.0	2.12	1787.1	5863	142.0	2.15
1758.2	5768	114.0	2.12	1788.1	5866	143.0	2.15
1759.3	5772	115.0	2.12	1789.0	5869	144.0	2.15
1760.4	5776	116.0	2.12	1790.0	5873	145.0	2.15
1761.5	5779	117.0	2.12	1791.0	5876	146.0	2.16
1762.6	5783	118.0	2.12	1791.9	5879	147.0	2.16
1763.6	5786	119.0	2.13	1792.8	5882	148.0	2.16
1764.7	5790	120.0	2.13	1793.8	5885	149.0	2.16
1765.8	5793	121.0	2.13	1794.7	5888	150.0	2.16
1766.9	5797	122.0	2.13	1795.6	5891	151.0	2.16
1767.9	5800	123.0	2.13	1796.6	5894	152.0	2.16
1769.0	5804	124.0	2.13	1797.5	5897	153.0	2.16
1770.0	5807	125.0	2.13	1798.4	5900	154.0	2.16
1771.1	5811	126.0	2.13	1799.3	5903	155.0	2.16
1772.1	5814	127.0	2.13	1800.2	5906	156.0	2.16
1773.2	5818	128.0	2.14	1801.1	5909	157.0	2.16
1774.2	5821	129.0	2.14	1802.0	5912	158.0	2.17
1775.2	5824	130.0	2.14	1802.9	5915	159.0	2.17
1776.2	5827	131.0	2.14	1803.8	5918	160.0	2.17
1777.2	5831	132.0	2.14	1804.7	5921	161.0	2.17
1778.3	5834	133.0	2.14	1805.6	5924	162.0	2.17
1779.3	5838	134.0	2.14	1806.5	1527	163.0	2.17

Velocity		Mean Size $\mu$	Wet Density g/cc	Velocity		Mean Size $\mu$	Wet Density g/cc
m/sec	ft/sec			m/sec	ft/sec		
1807.4	5930	164.0	2.17	1831.5	6009	193.0	2.19
1808.2	5933	165.0	2.17	1832.3	6011	194.0	2.19
1809.1	5935	166.0	2.17	1833.1	6014	195.0	2.20
1810.0	5938	167.0	2.17	1833.8	6017	196.0	2.20
1810.9	5941	168.0	2.17	1834.6	6019	197.0	2.20
1811.7	5944	169.0	2.18	1835.4	6022	198.0	2.20
1812.6	5947	170.0	2.18	1836.2	6024	199.0	2.20
1813.4	5950	171.0	2.18	1837.0	6027	200.0	2.20
1814.3	5952	172.0	2.18	1837.7	6029	201.0	2.20
1815.1	5955	173.0	2.18	1838.5	6032	202.0	2.20
1816.0	5958	174.0	2.18	1839.3	6034	203.0	2.20
1816.8	5961	175.0	2.18	1840.0	6037	204.0	2.20
1817.7	5963	176.0	2.18	1840.8	6039	205.0	2.20
1818.5	5966	177.0	2.18	1841.5	6042	206.0	2.20
1819.3	5969	178.0	2.18	1842.3	6044	207.0	2.20
1820.2	5972	179.0	2.18	1843.0	6047	208.0	2.20
1821.0	5974	180.0	2.18	1843.8	6049	209.0	2.21
1821.8	5977	181.0	2.19	1844.5	6052	210.0	2.21
1822.6	5980	182.0	2.19	1845.3	6054	211.0	2.21
1823.5	5982	183.0	2.19	1846.0	6056	212.0	2.21
1824.3	5985	184.0	2.19	1846.8	6059	213.0	2.21
1825.1	5988	185.0	2.19	1847.5	6061	214.0	2.21
1825.9	5990	186.0	2.19	1848.2	6064	215.0	2.21
1827.5	5996	187.0	2.19	1849.0	6066	216.0	2.21
1827.5	5996	188.0	2.19	1849.7	6069	217.0	2.21
1828.3	5998	189.0	2.19	1850.4	6071	218.0	2.21
1829.1	6001	190.0	2.19	1851.1	6073	219.0	2.21
1829.9	6004	191.0	2.19	1851.9	6076	220.0	2.21
1830.7	6006	192.0	2.19	1852.6	6078	221.0	2.21



	Velocity		Mean Size	Wet Density	Velocity		Mean Size	Wet Density
	m/sec	ft/sec	μ	g/cc	m/sec	ft/sec	μ	g/cc
1853.3	6080	1875.9	222.0	2.21	6155	1875.9	255.0	2.23
1854.0	6083	1879.2	223.0	2.21	6165	1879.2	260.0	2.24
1854.7	6085	1882.4	224.0	2.22	6176	1882.4	265.0	2.24
1855.5	6087	1885.6	225.0	2.22	6186	1885.6	270.0	2.24
1856.2	6090	1888.7	226.0	2.22	6196	1888.7	275.0	2.25
1856.9	6092	1891.8	227.0	2.22	6207	1891.8	280.0	2.25
1857.6	6094	1894.8	228.0	2.22	6217	1894.8	285.0	2.25
1858.3	6097	1897.8	229.0	2.22	6227	1897.8	290.0	2.25
1859.0	6099	1900.8	230.0	2.22	6236	1900.8	295.0	2.26
1859.7	6101	1903.8	231.0	2.22	6246	1903.8	300.0	2.26
1860.4	6104	1906.7	232.0	2.22	6256	1906.7	305.0	2.26
1861.1	6106	1909.6	233.0	2.22	6265	1909.6	310.0	2.26
1861.8	6108	1912.4	234.0	2.22	6274	1912.4	315.0	2.27
1862.5	6110	1915.2	235.0	2.22	6284	1915.2	320.0	2.27
1863.2	6113	1918.0	236.0	2.22	6293	1918.0	325.0	2.27
1863.9	6115	1920.8	237.0	2.22	6302	1920.8	330.0	2.27
1864.5	6117	1923.5	238.0	2.22	6311	1923.5	335.0	2.27
1865.2	6119	1926.2	239.0	2.22	6320	1926.2	340.0	2.28
1865.9	6122	1928.9	240.0	2.23	6328	1928.9	345.0	2.28
1866.6	6124	1931.5	241.0	2.23	6337	1931.5	350.0	2.28
1867.3	6126	1934.1	242.0	2.23	6346	1934.1	355.0	2.28
1867.9	6128	1936.7	243.0	2.23	6354	1936.7	360.0	2.28
1868.6	6130	1939.3	244.0	2.23	6363	1939.3	365.0	2.29
1869.3	6133	1941.9	245.0	2.23	6371	1941.9	370.0	2.29
1870.0	6135	1944.4	246.0	2.23	6379	1944.4	375.0	2.29
1870.6	6137	1946.9	247.0	2.23	6387	1946.9	380.0	2.29
1871.3	6139	1949.4	248.0	2.23	6396	1949.4	385.0	2.29
1872.0	6142	1951.8	249.0	2.23	6404	1951.8	390.0	2.30
1872.6	6144	1954.3	250.0	2.23	6412	1954.3	395.0	2.30

Velocity		Mean Size μ	Wet Density g/cc
m/sec	ft/sec		
1956.7	6419	400.0	2.30
1959.1	6427	405.0	2.30
1961.4	6435	410.0	2.30
1963.8	6443	415.0	2.30
1966.1	6450	420.0	2.31
1968.4	6458	425.0	2.31
1970.7	6466	430.0	2.31
1973.0	6473	435.0	2.31
1975.2	6480	440.0	2.31
1977.5	6488	445.0	2.32
1979.7	6495	450.0	2.32
1981.9	6502	455.0	2.32
1984.1	6509	460.0	2.32
1986.3	6517	465.0	2.32
1988.4	6524	470.0	2.32
1990.6	6531	475.0	2.33
1992.7	6538	480.0	2.33
1994.8	6545	485.0	2.33
1996.9	6551	490.0	2.33
1999.0	6558	495.0	2.33
2001.0	6565	500.0	2.33

## APPENDIX D

### CORES TAKEN BY R/V ROBERT D. CONRAD AND R/V VEMA

Core lithology. reflectors. predicted sound velocity  
predicted wet density and mean grain size of  
sediment layers.

## Legend

The uniformity of texture shown by various types of deep-sea deposits makes it possible to predict sonic properties of layers without actual measurement. For this reason the predicted wet density and velocity profiles of the cores are far more complete and detailed than those of actual laboratory measurements given under the mean size column. For example, all ash horizons off Japan have similar textures. Therefore, three or four samples of say ten ash layers in a given core will provide sufficient data to draw velocity and wet density profiles of all ashes in the core.

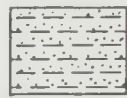
Lithology column  
symbols:



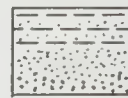
Clay



Gravel



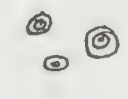
Mud



Graded Unit



Silt



Manganese nodules



Sand



Ice-rafted pebbles



Unconformity

Reflectors column:

Solid bars in columns represent position and thickness of sub-bottom reflecting horizons. A qualitative breakdown of the horizons as good, intermediate, poor and questionable is given based on thickness and texture of the horizons.

Predicted velocity  
column:

Solid line on velocity profile of core represents predictions from table in Appendix C and are based on analytical measurement of mean grain size of sediment layer.

Dashed line on velocity profile of core represents sound velocity predicted from mean grain sizes estimated from similar sediment layers within core.

Wet density column:

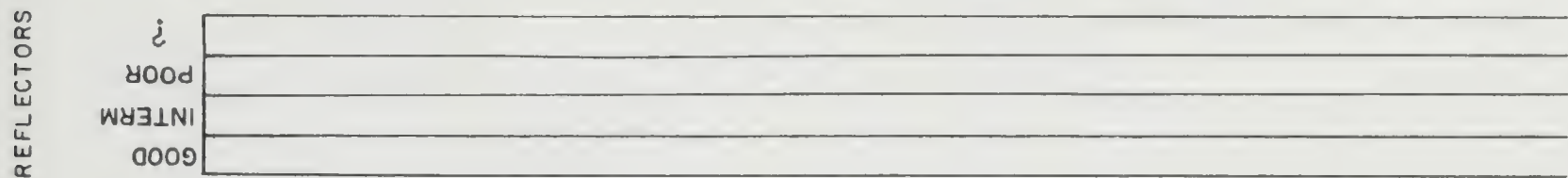
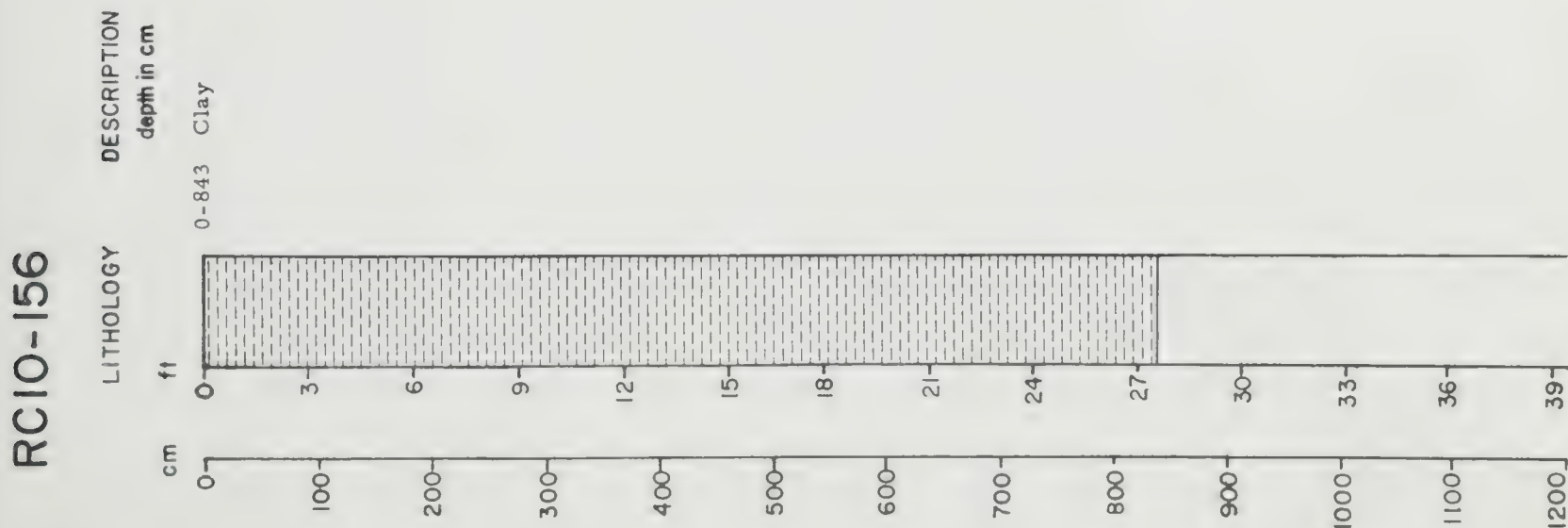
Dashed line used throughout because wet densities are predictions based on measured mean grain sizes of sediments. Wet densities are from Appendix C.

Mean grain size  
column:

Solid line connects points where actual determinations of grain size were made in the laboratory.

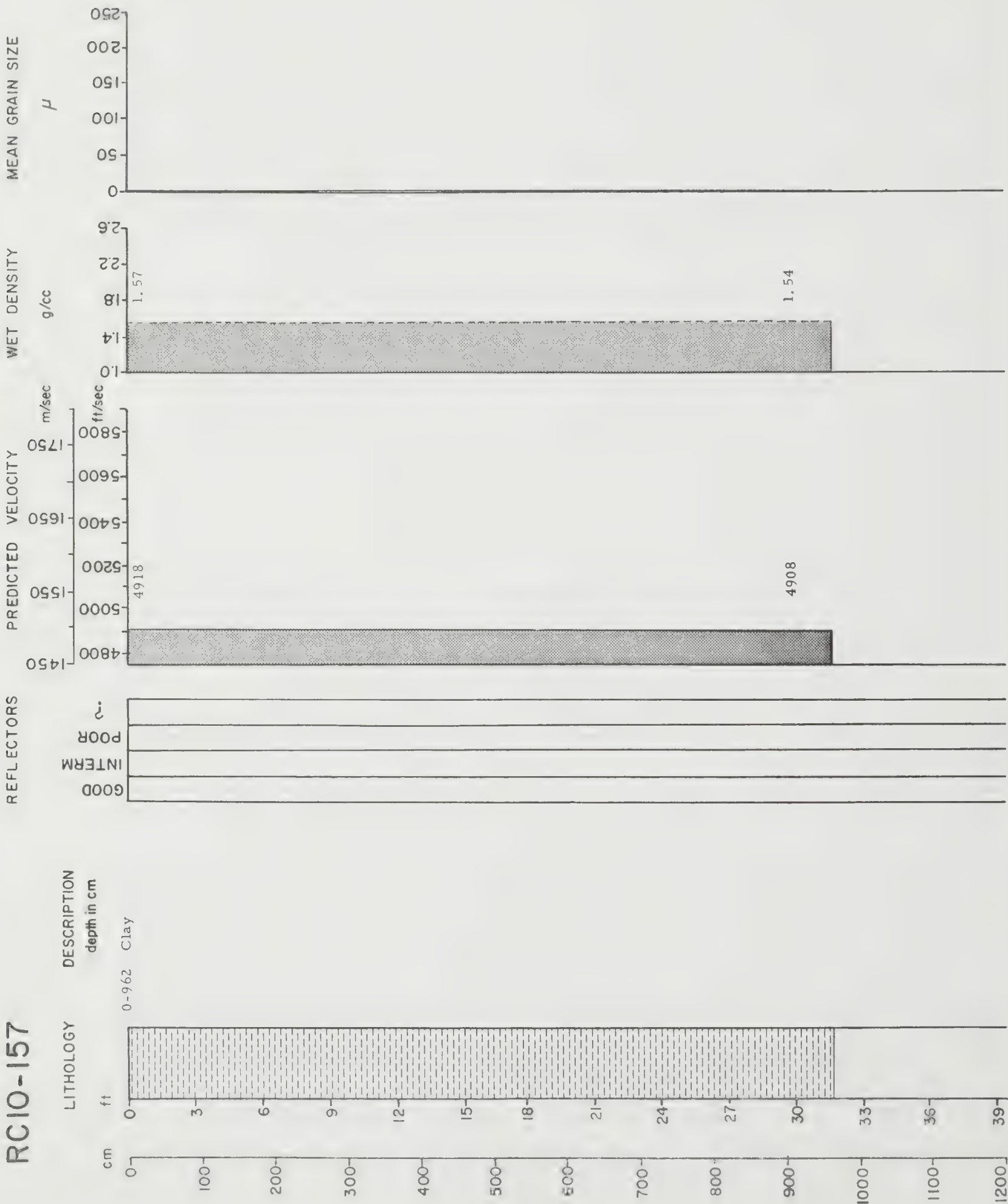


# RC10-156

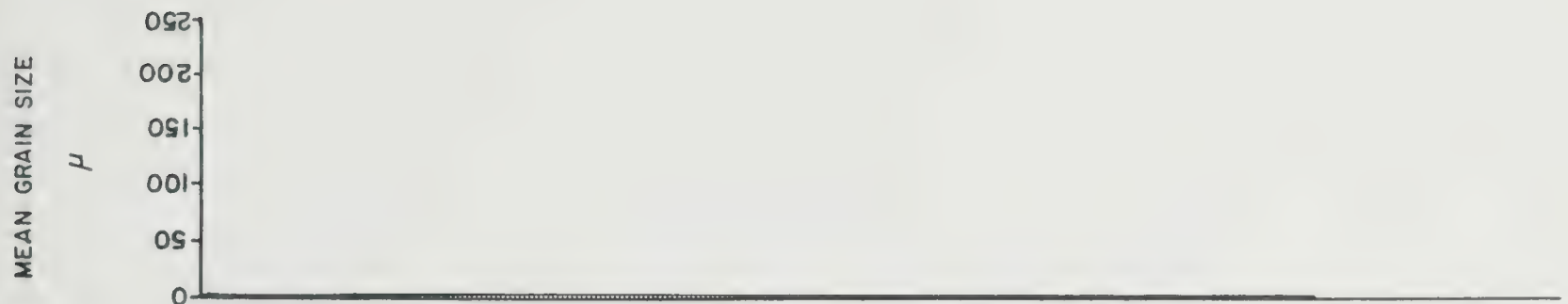
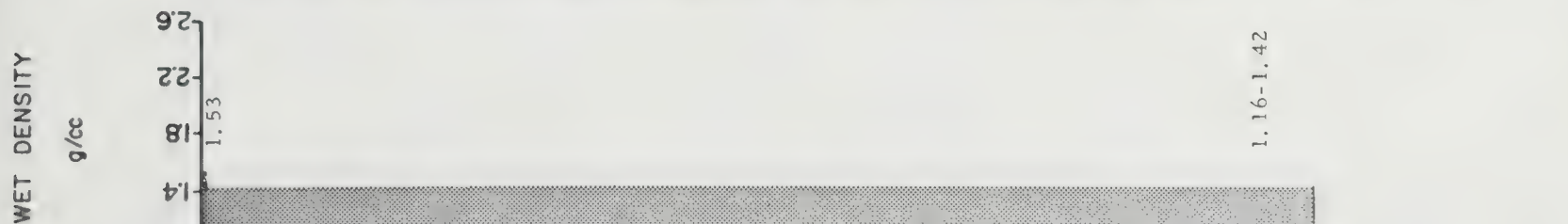
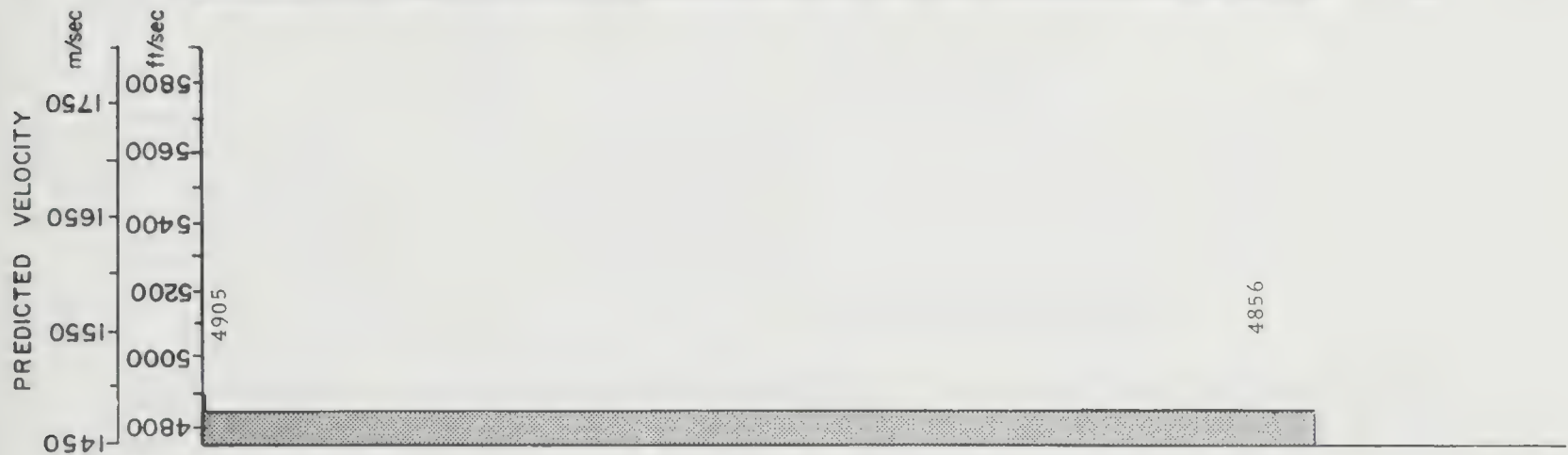
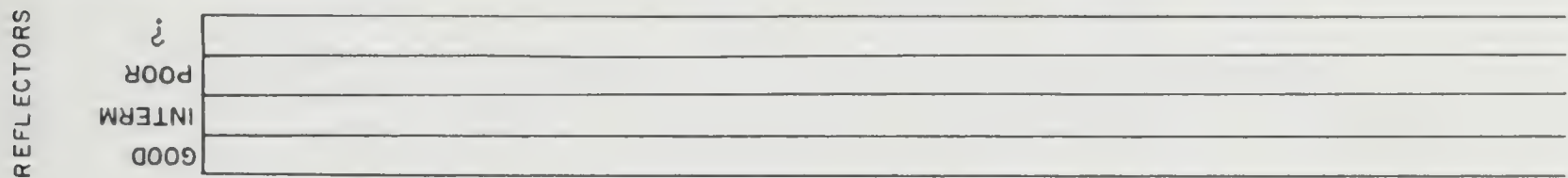
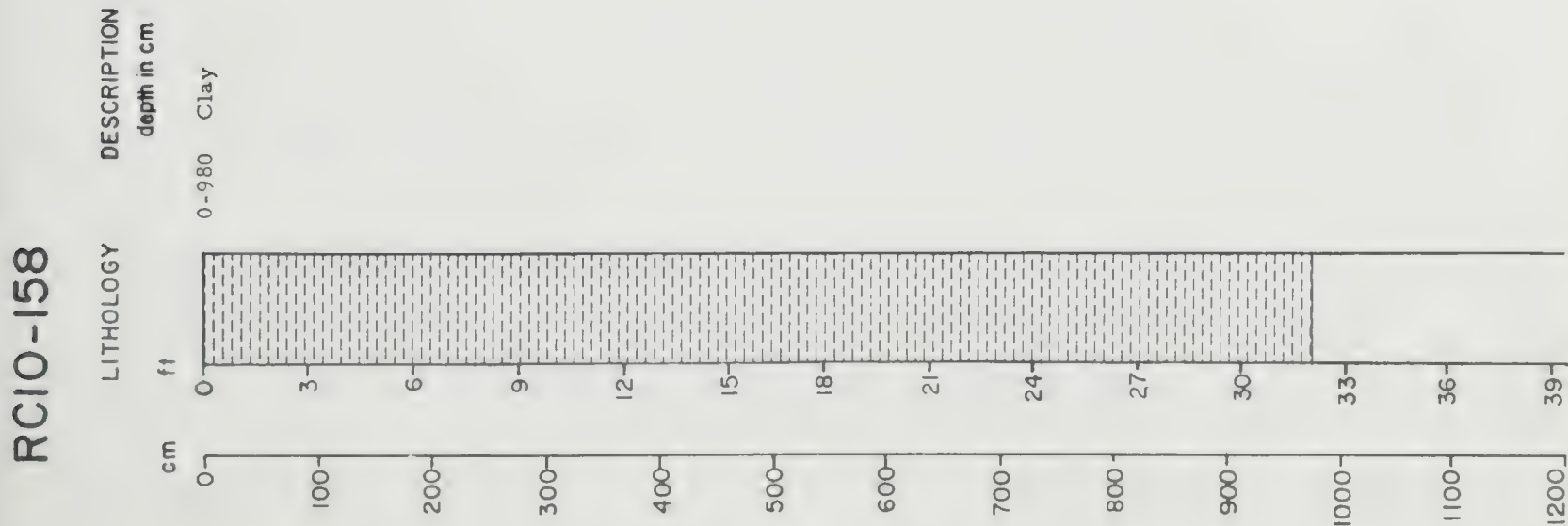


# RC10-157

D-2



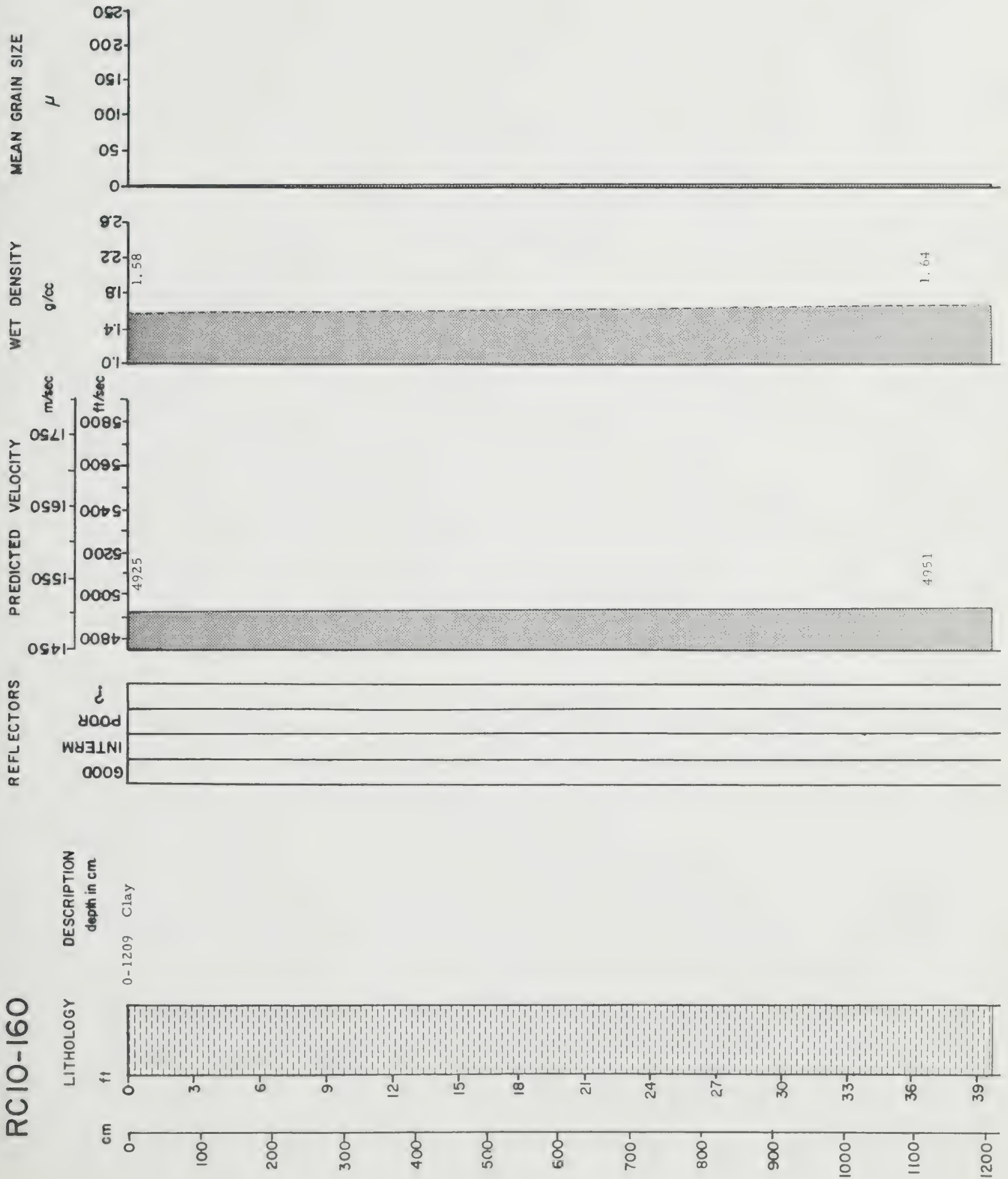
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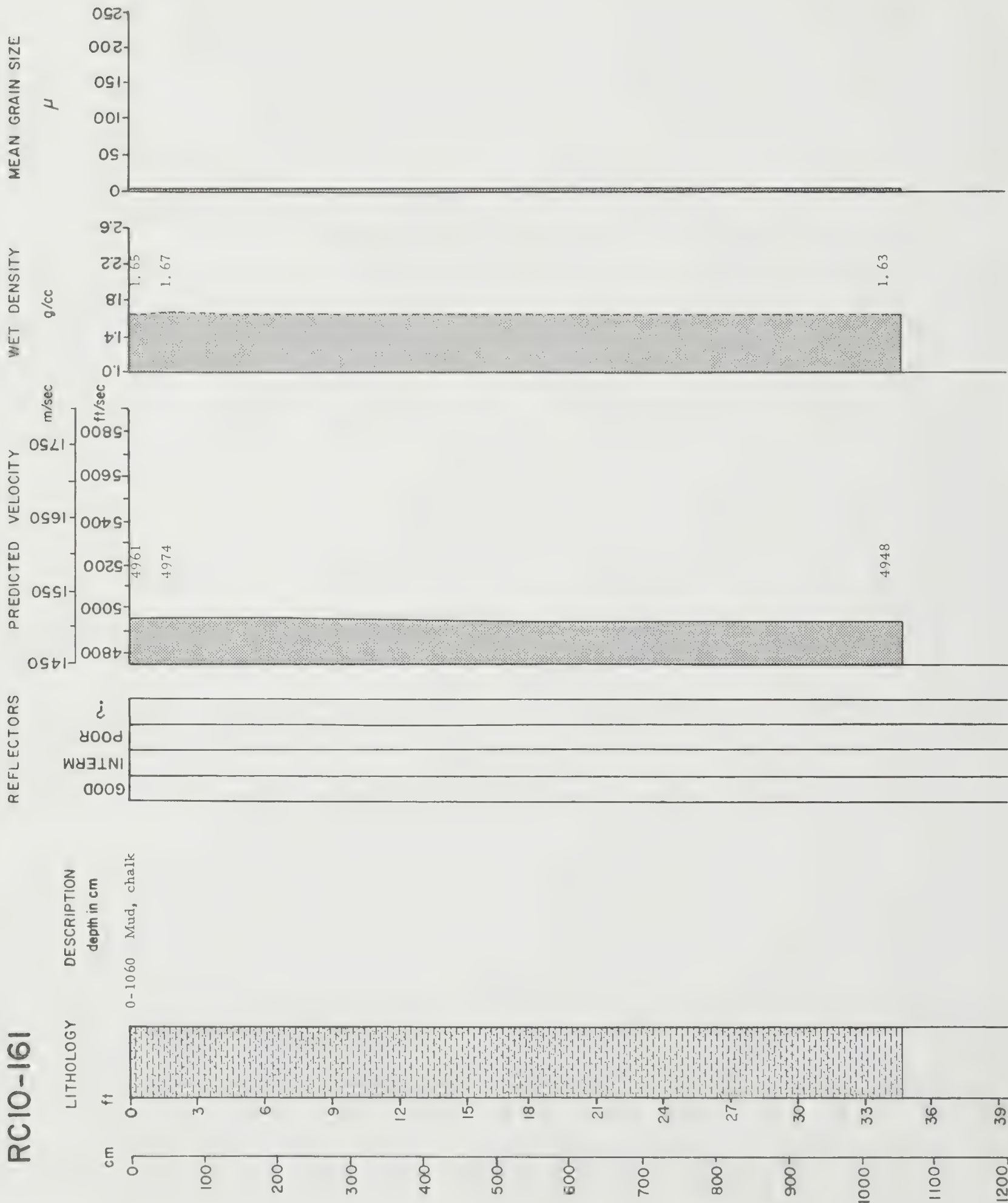
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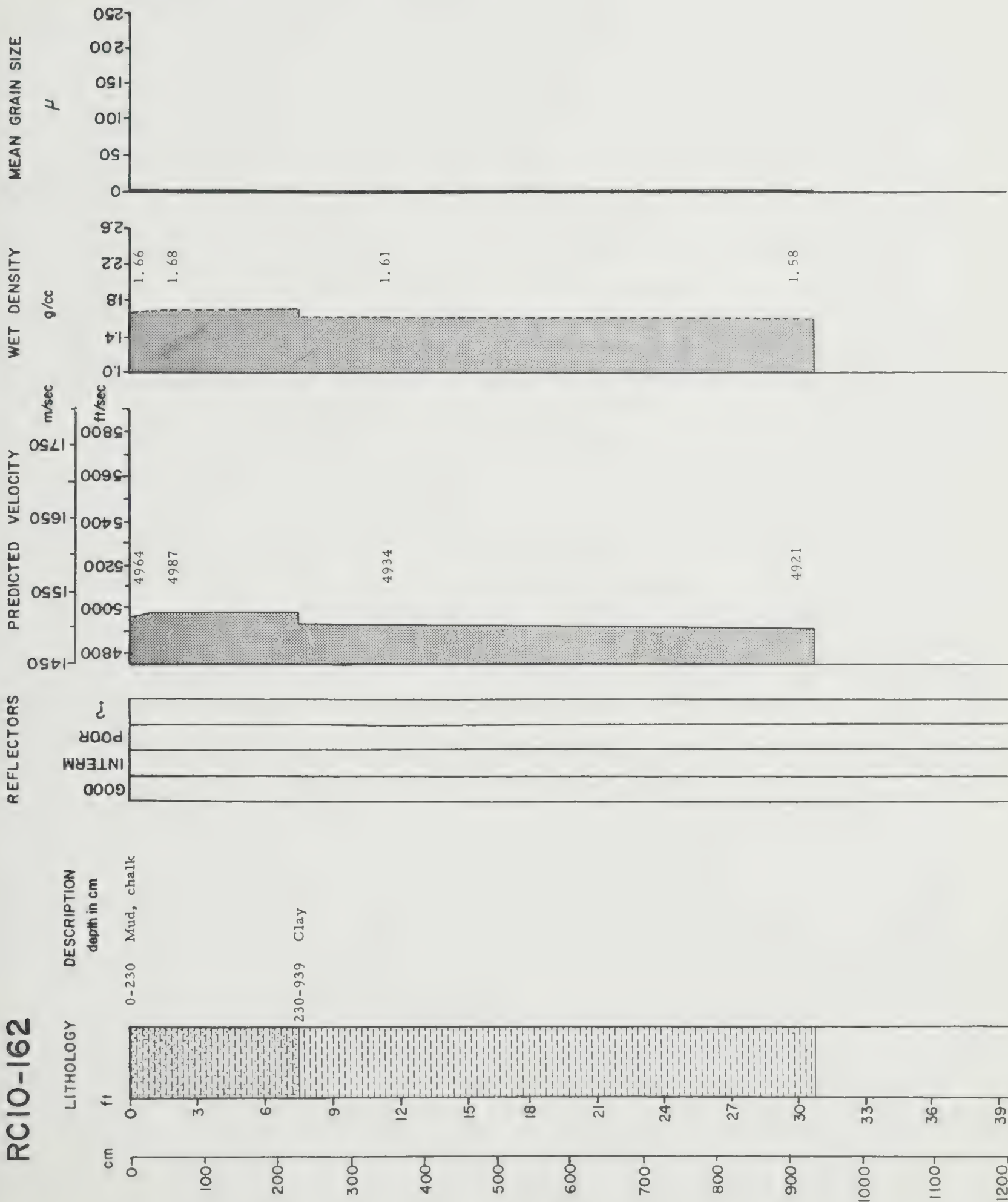




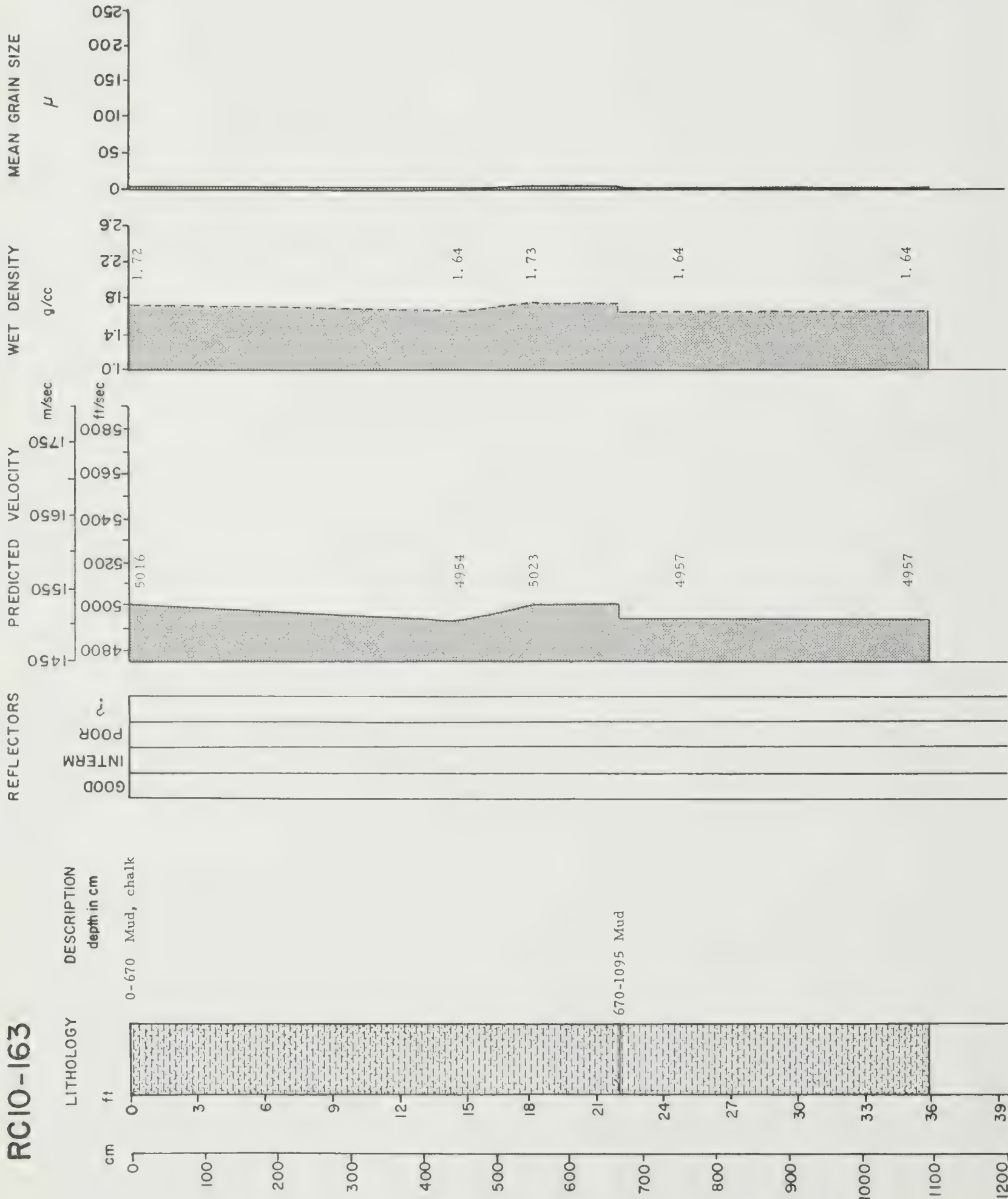
RC10-161



# RC10-162

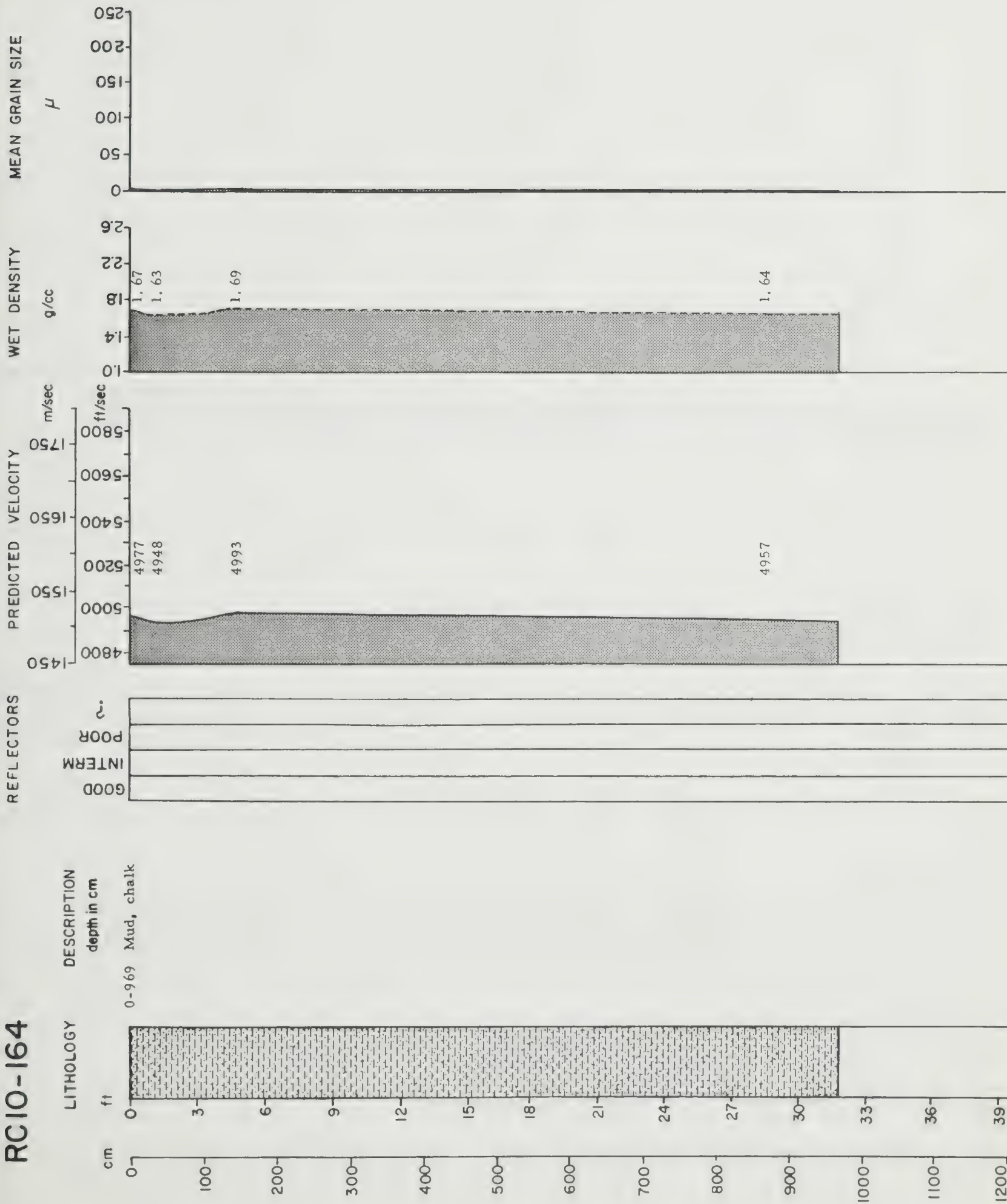


RC10-163

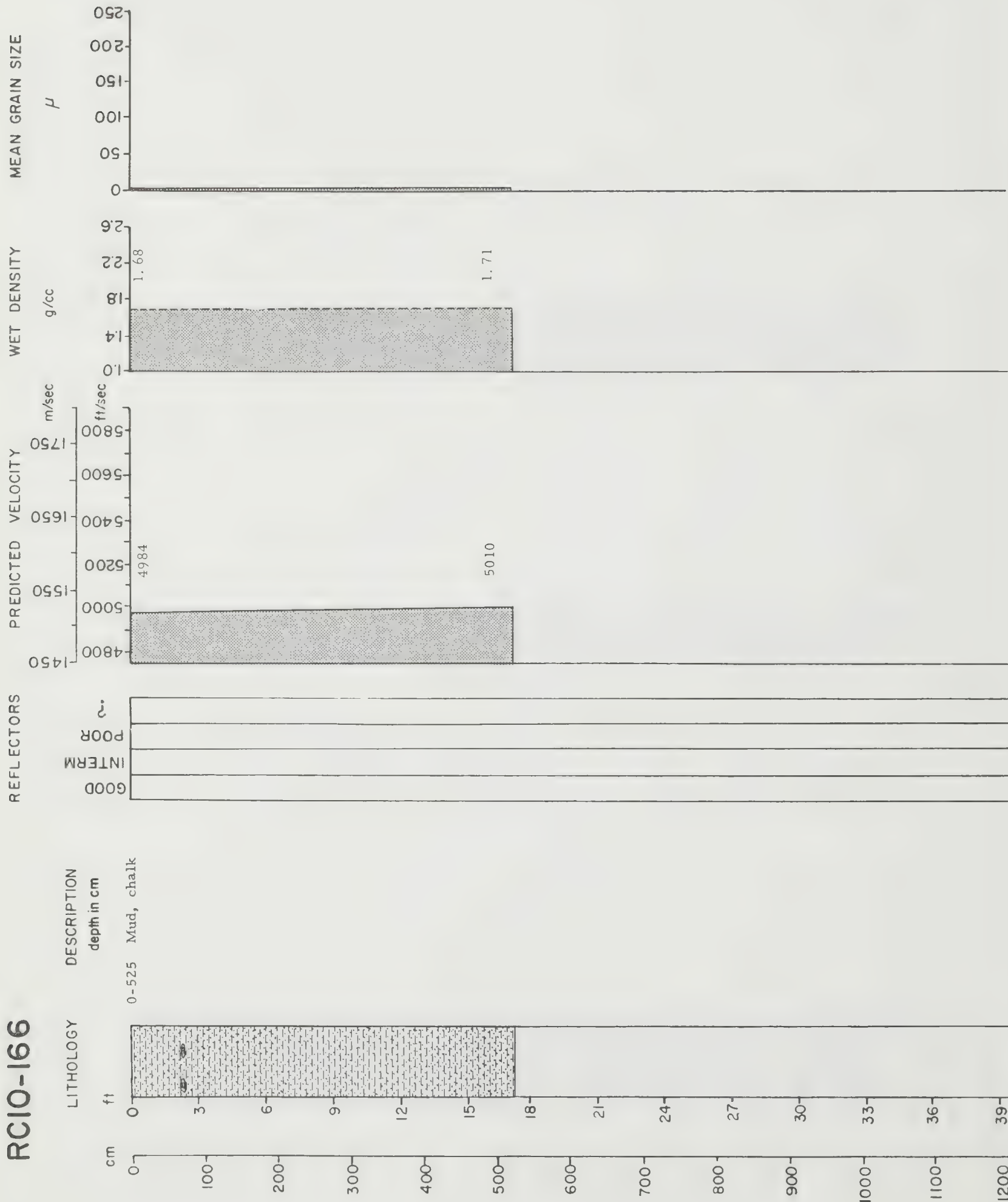




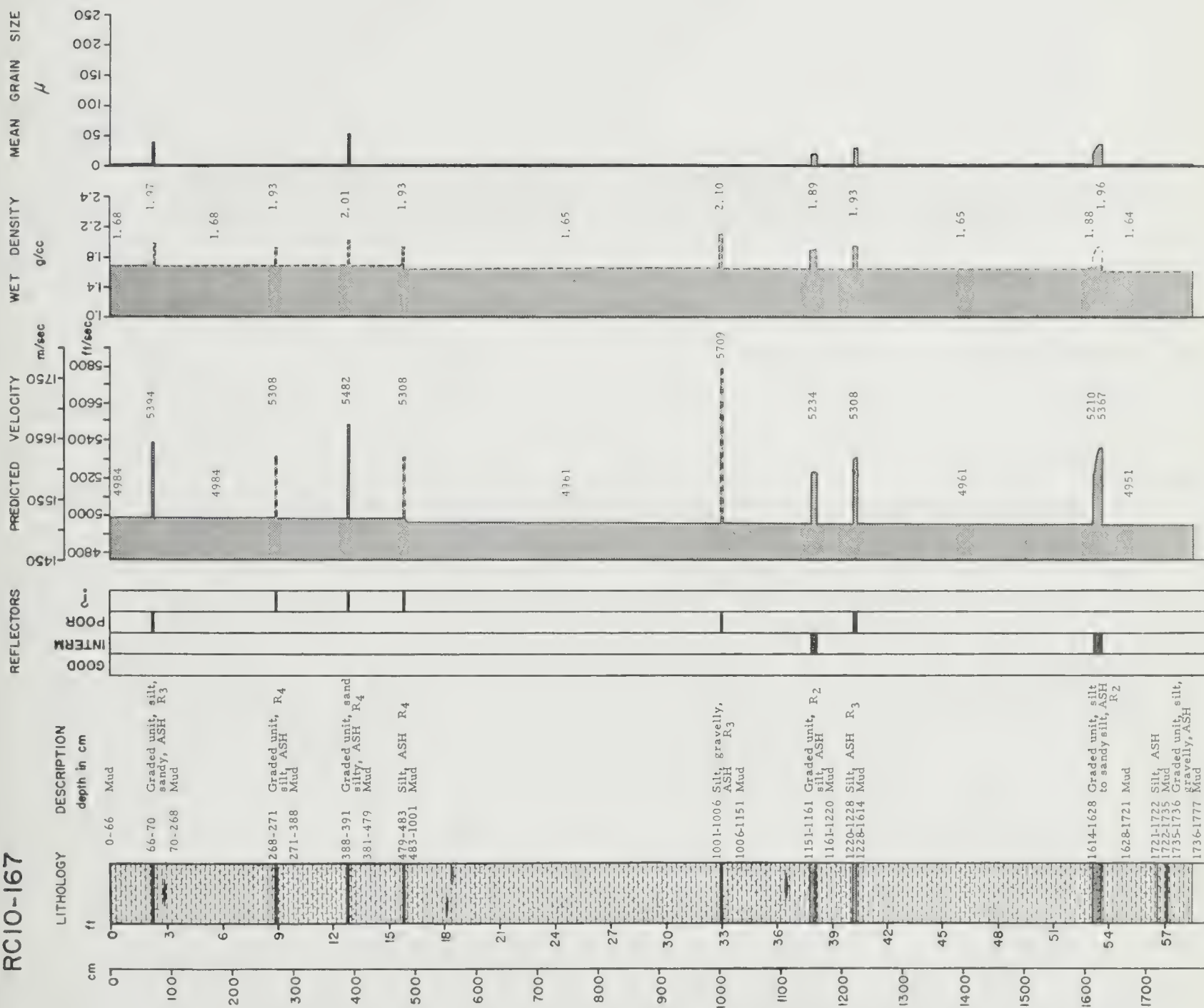
# RC10-164



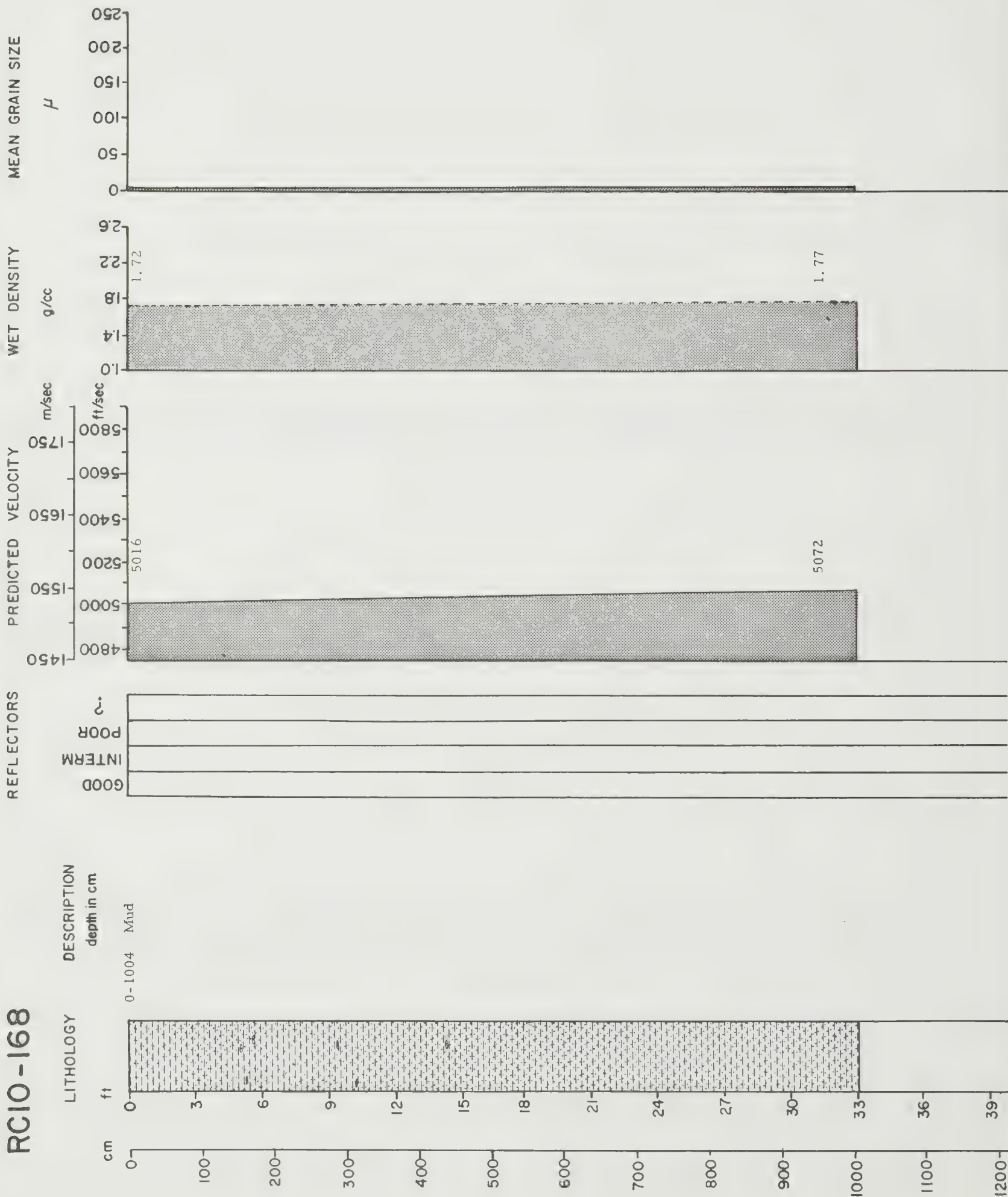
# RC10-166



RC10-167

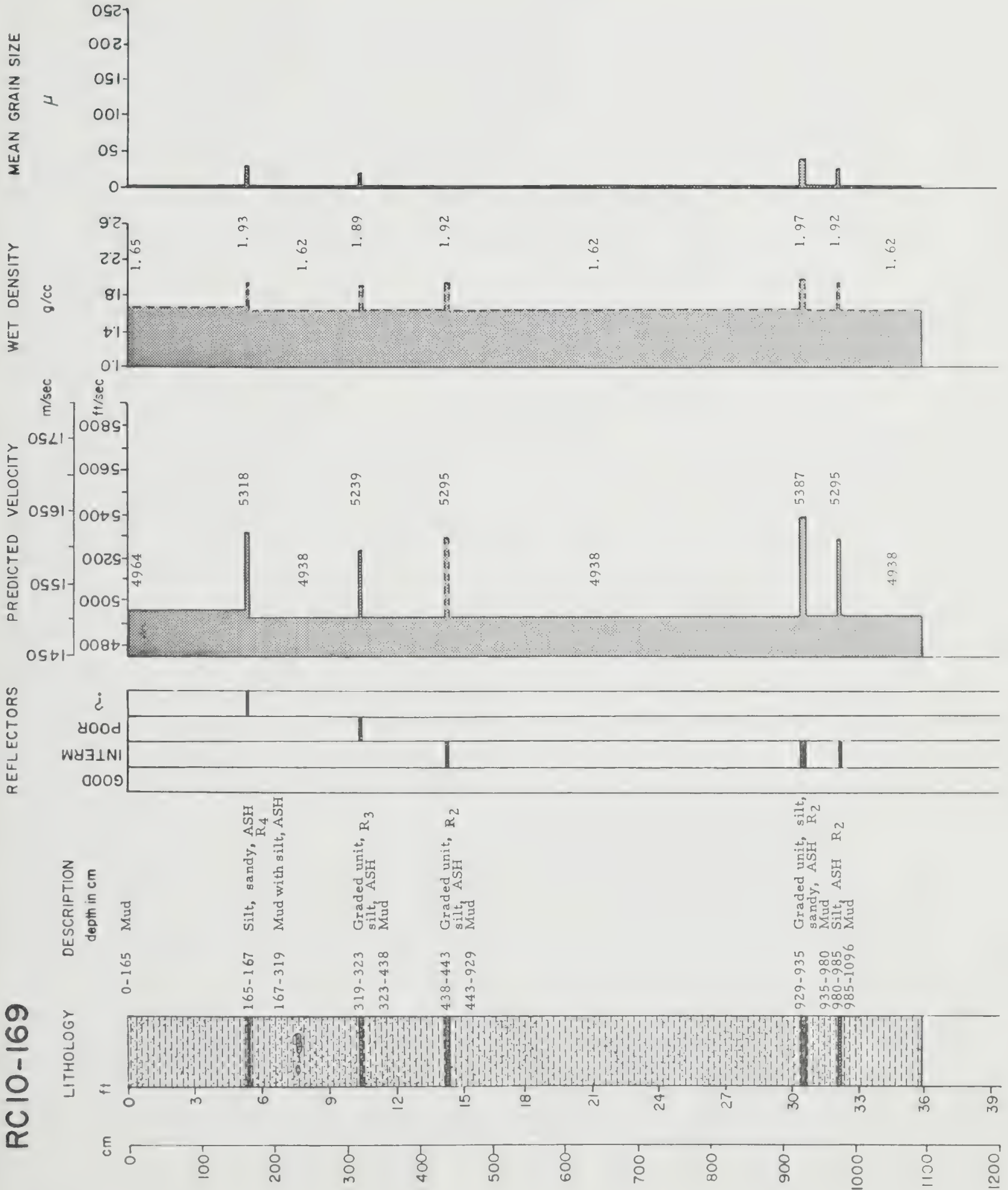


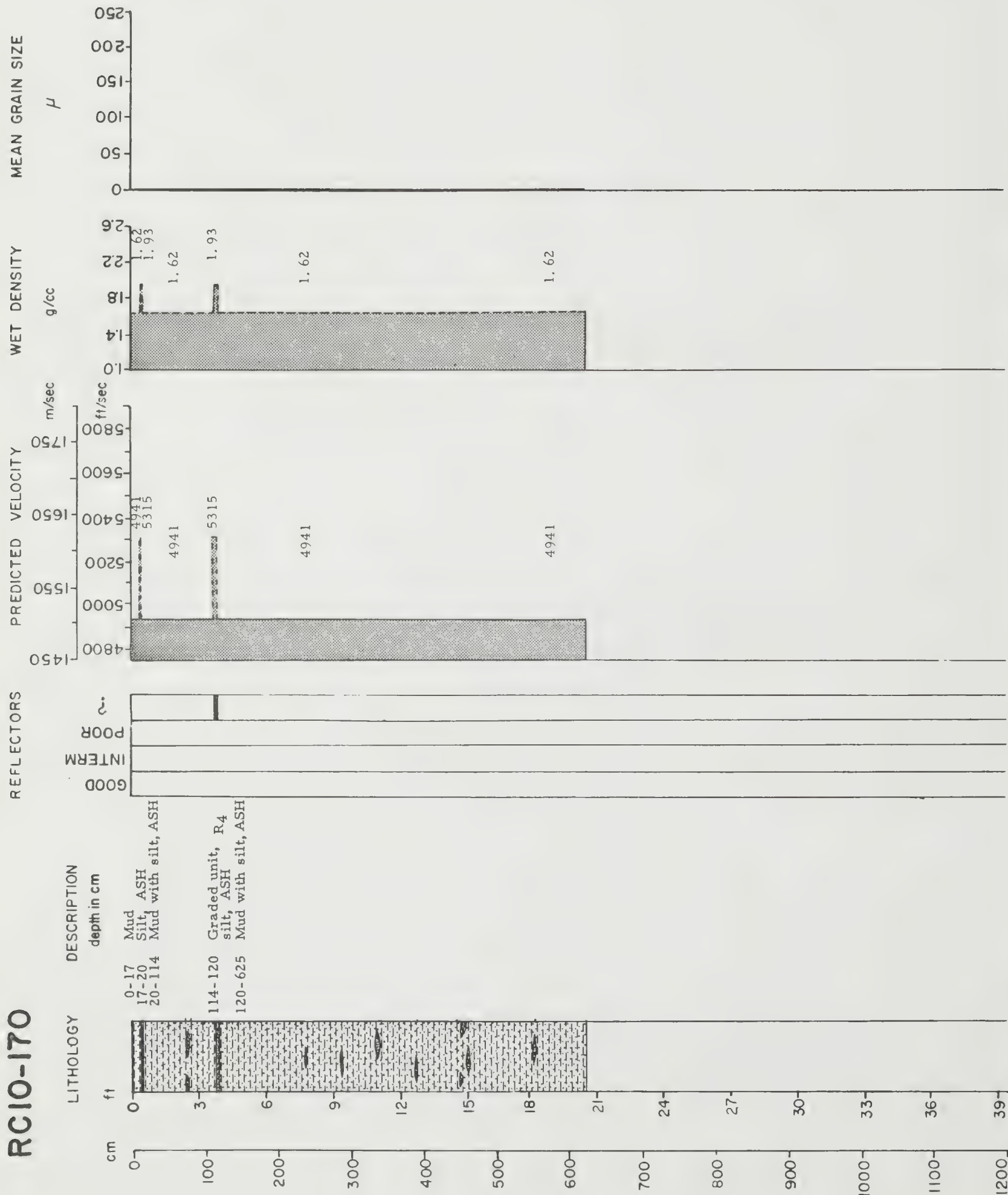
# RC10-168



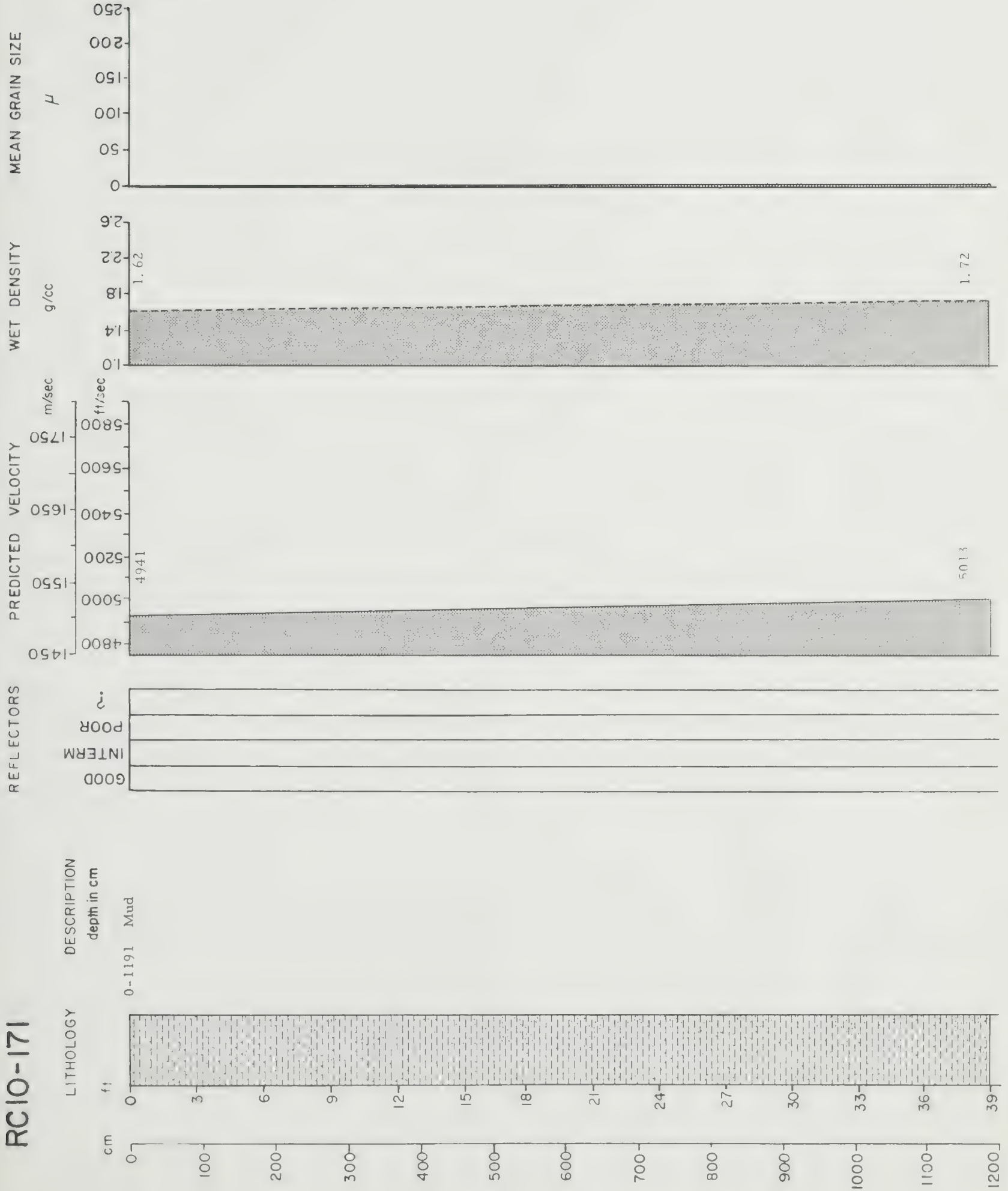


# RC10-169

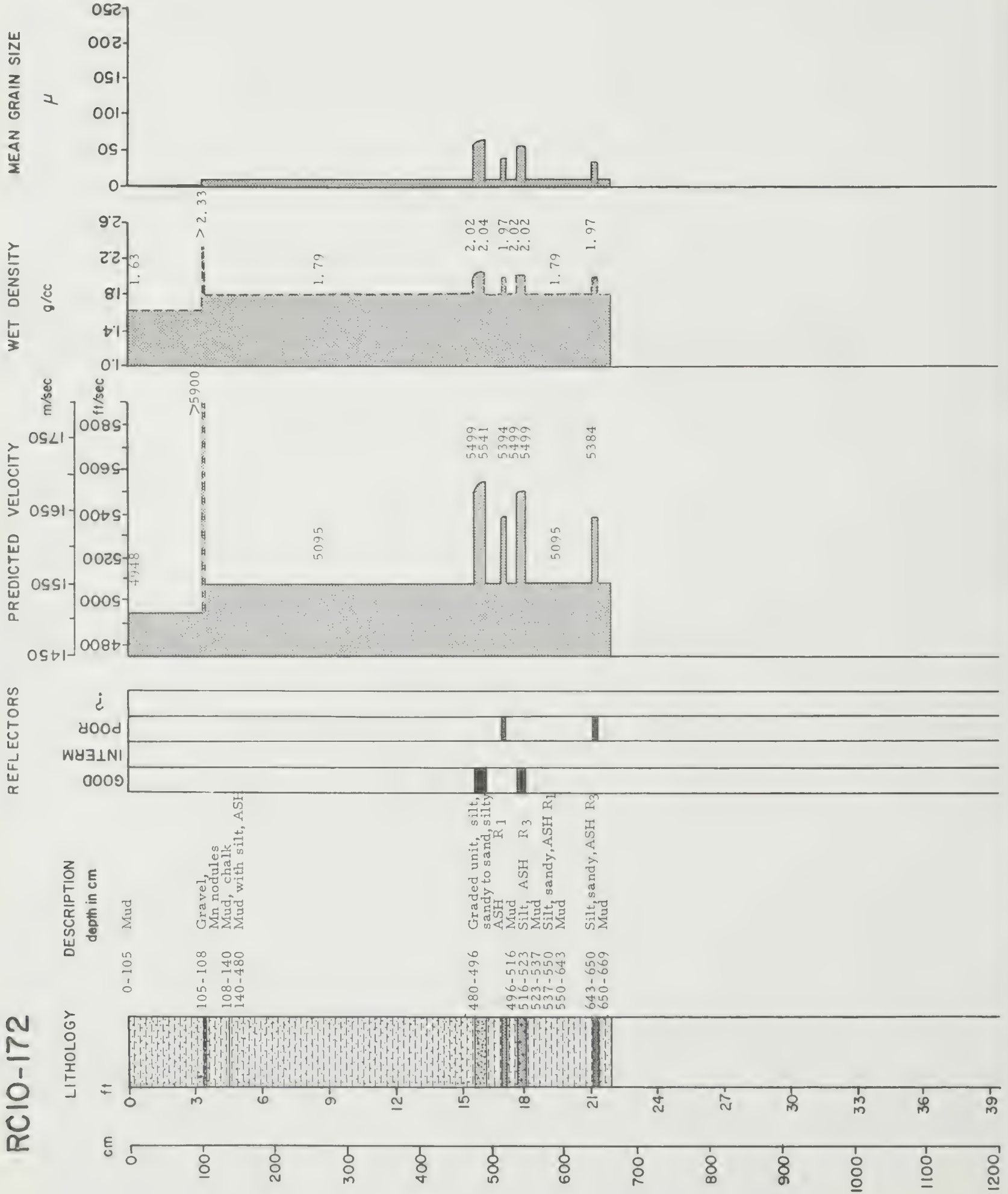




RC10-171

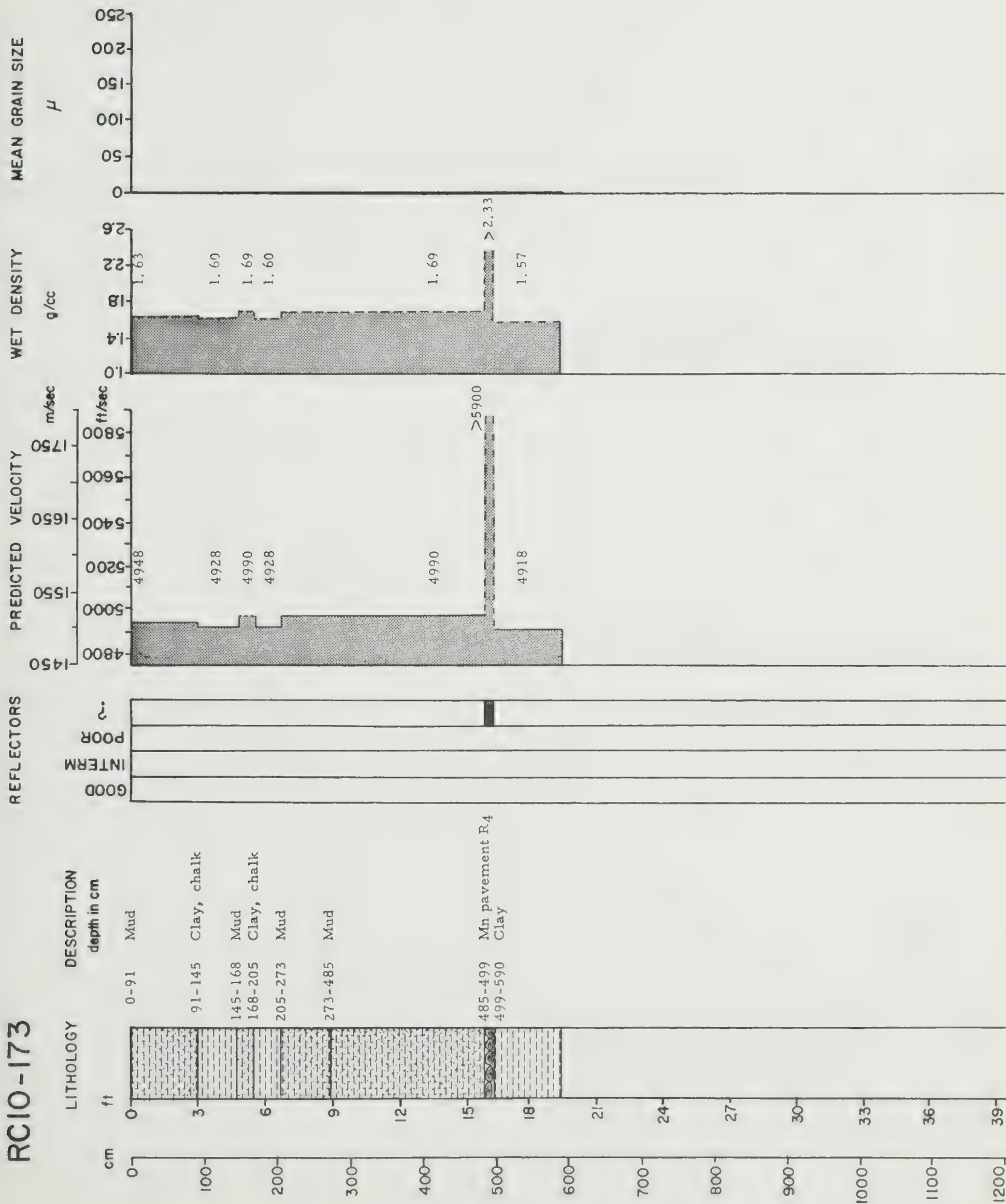


RC10-172

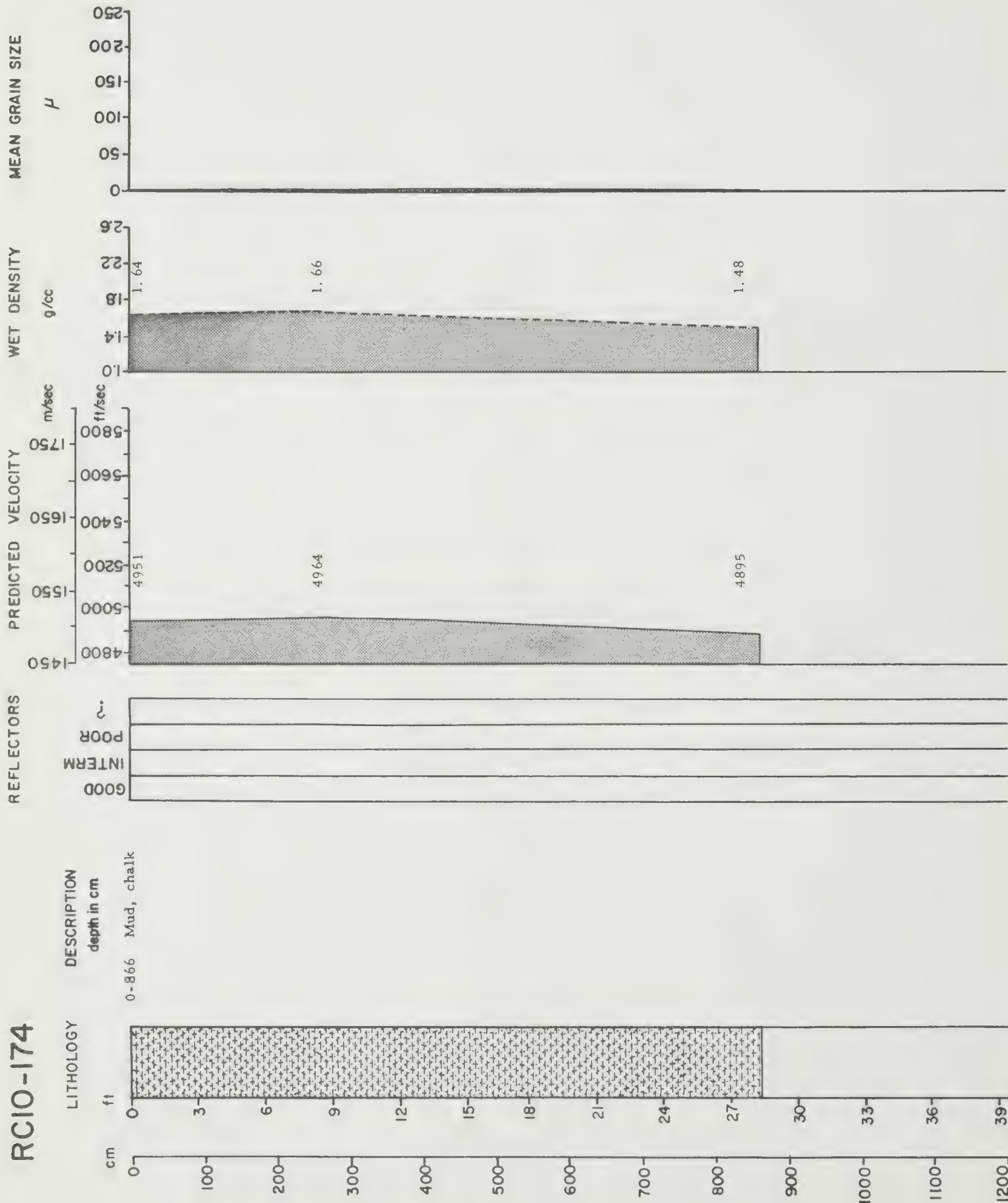




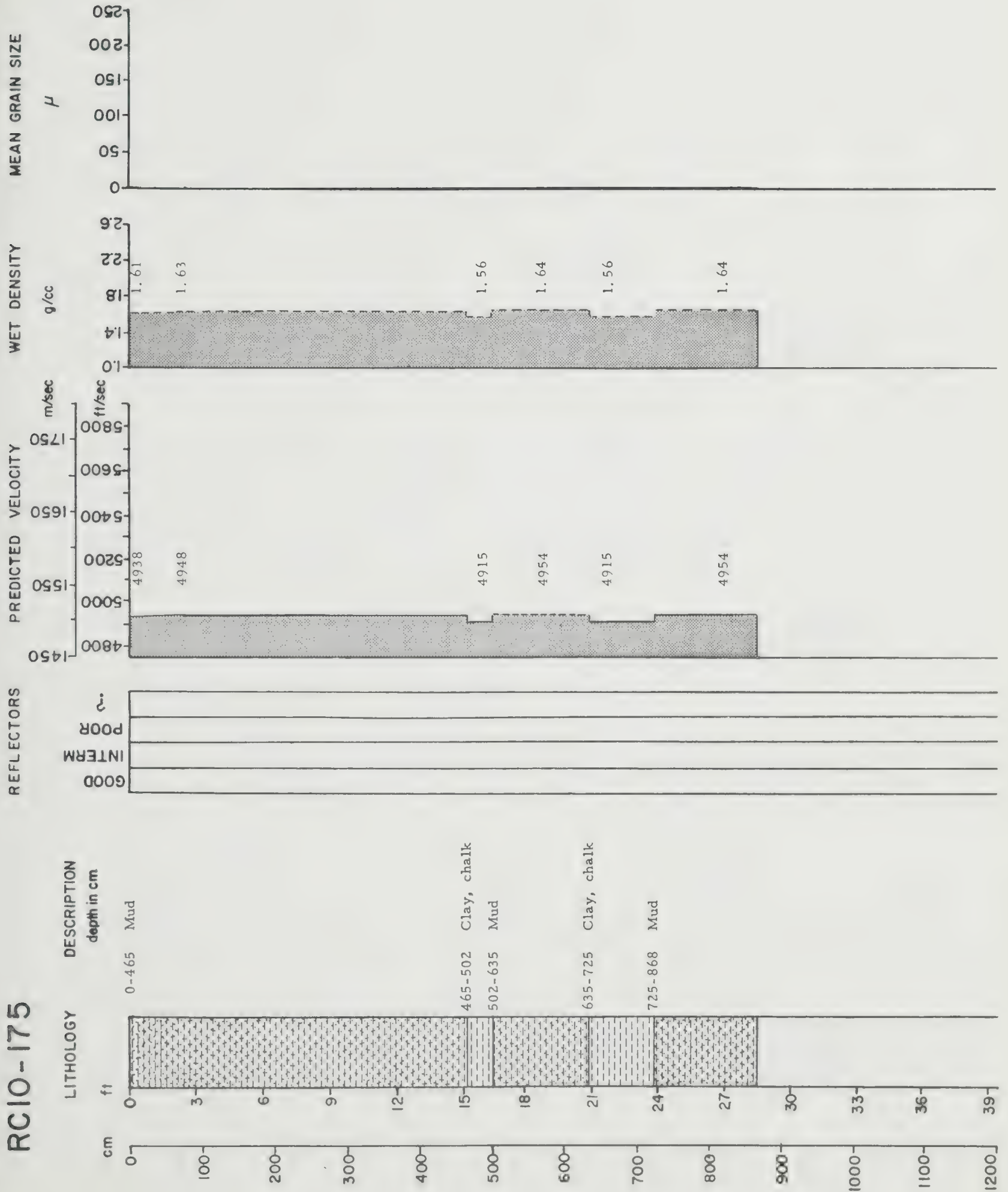
RC10-173



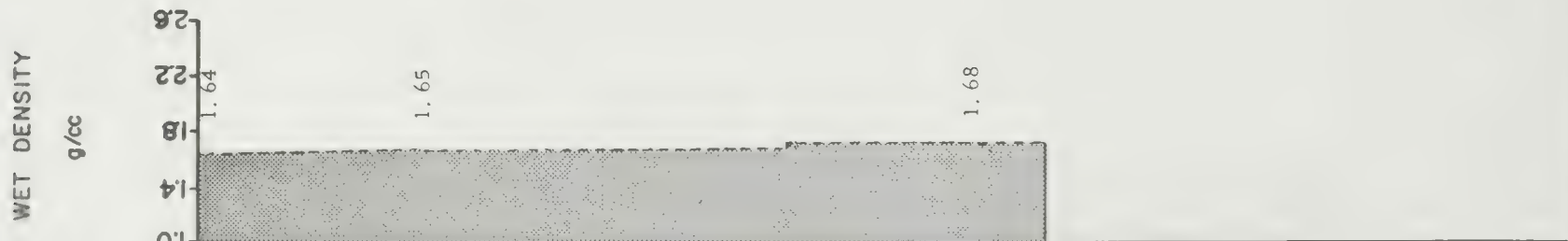
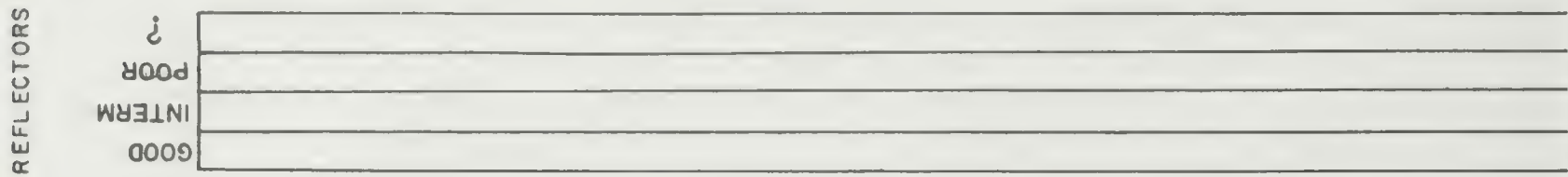
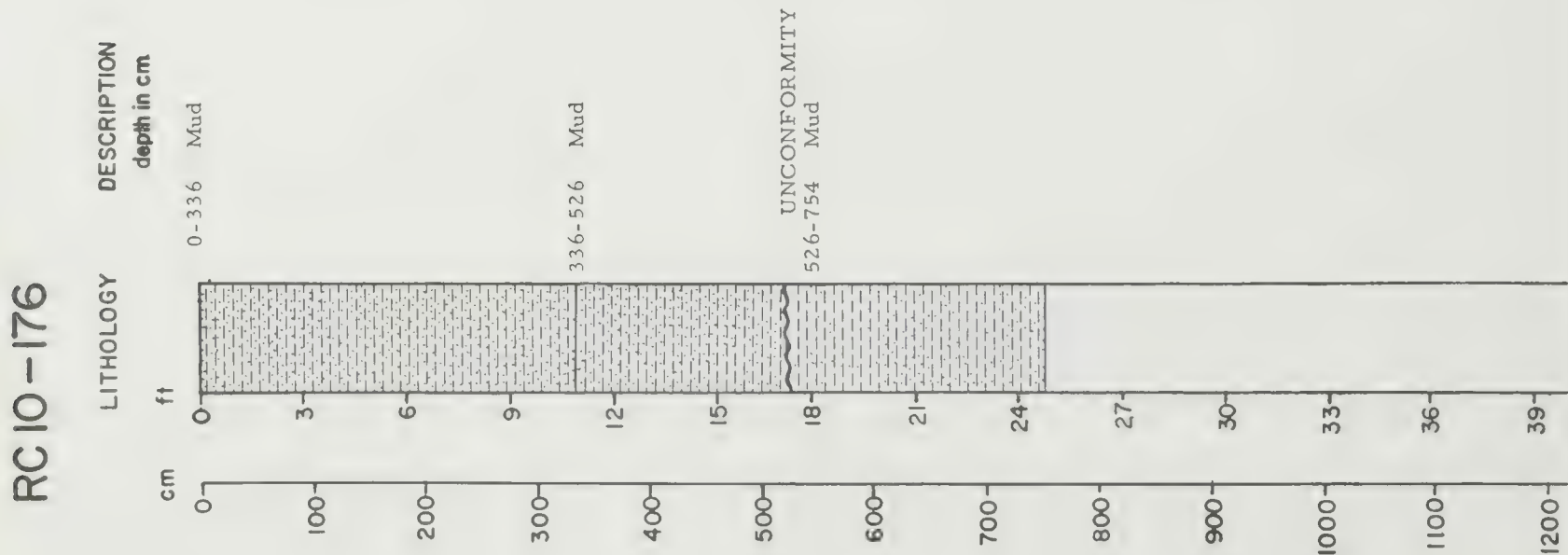
RCIO-174



RC10-175

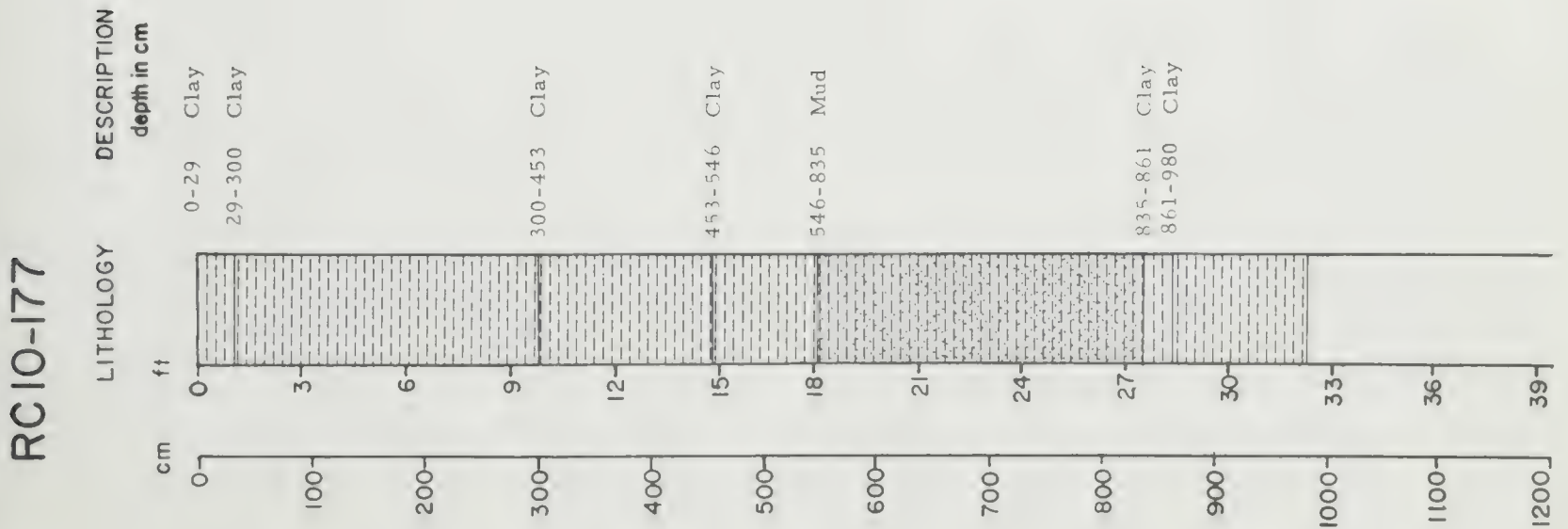


RC 10-176





RC10-177

**REFLECTORS**

GOOD  
INTERM  
POOR  
?

**PREDICTED VELOCITY**

m/sec  
ft/sec

1750  
5800  
1650  
5600  
1550  
5400  
1450  
5200  
5000  
4800

**WET DENSITY**

g/cc

2.6  
2.2  
1.8  
1.4  
1.0

**MEAN GRAIN SIZE** $\mu$ 

250  
200  
150  
100  
50  
0

1.57

1.60

1.64

1.60

1.57

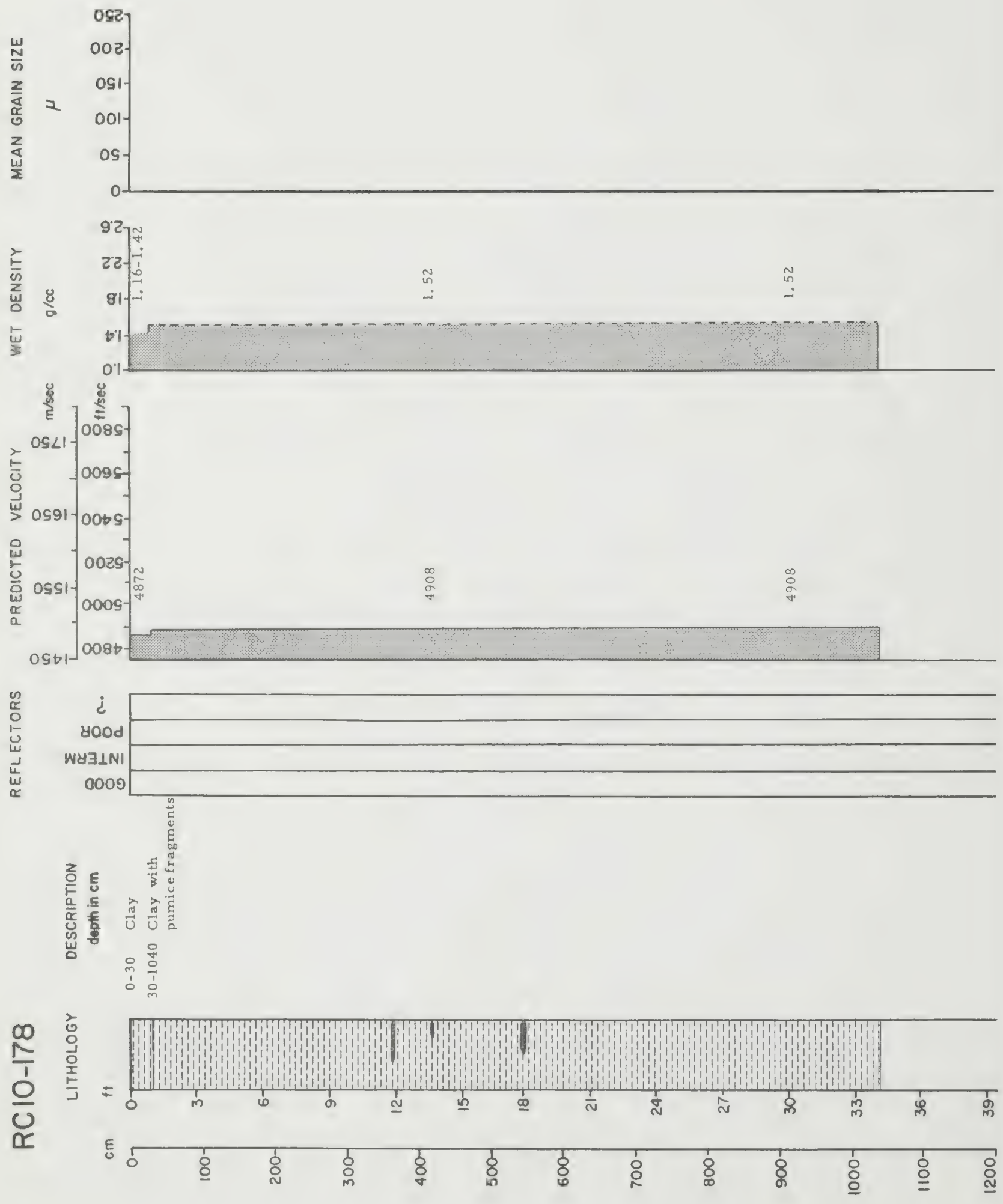
4915

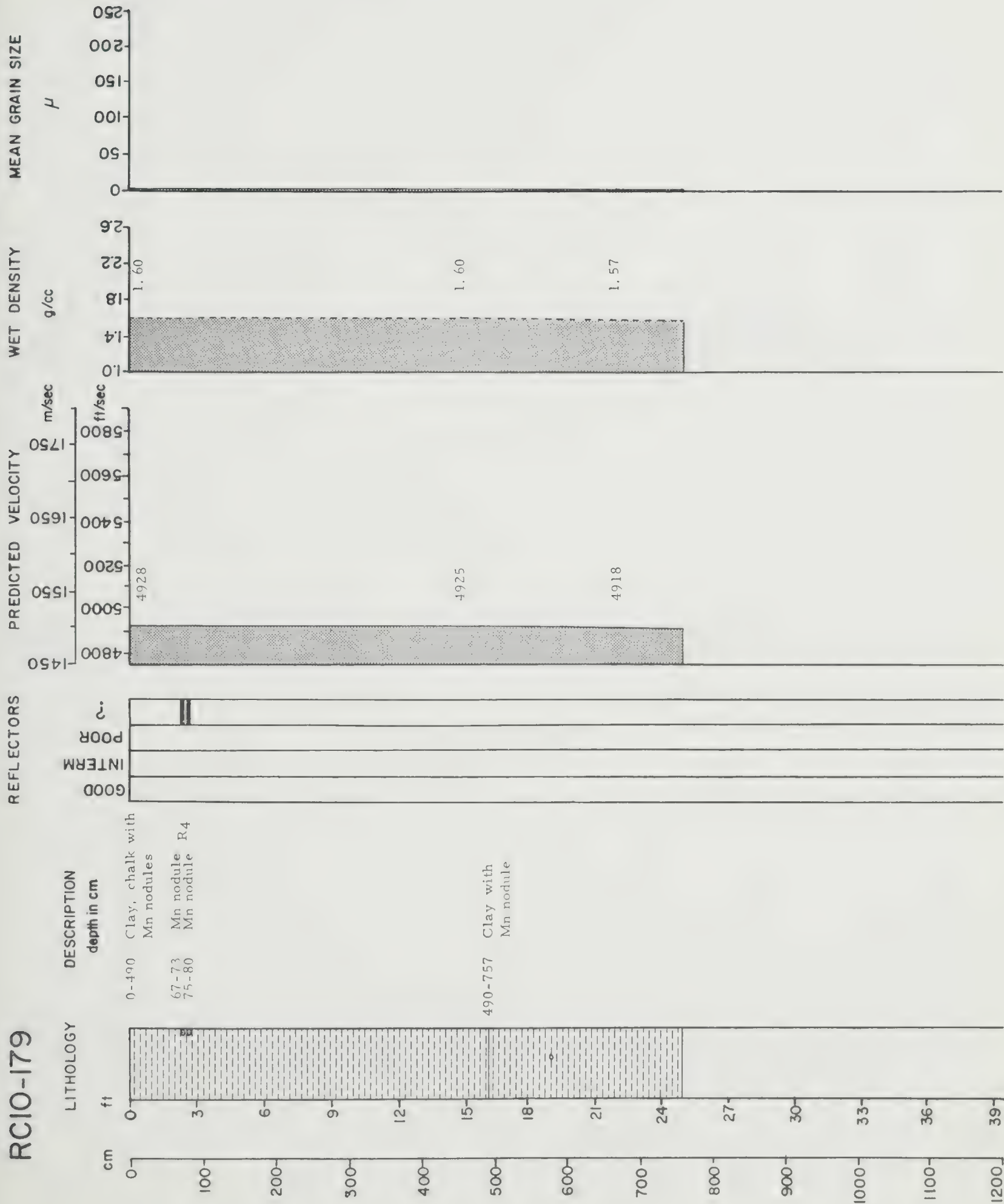
4931

4954

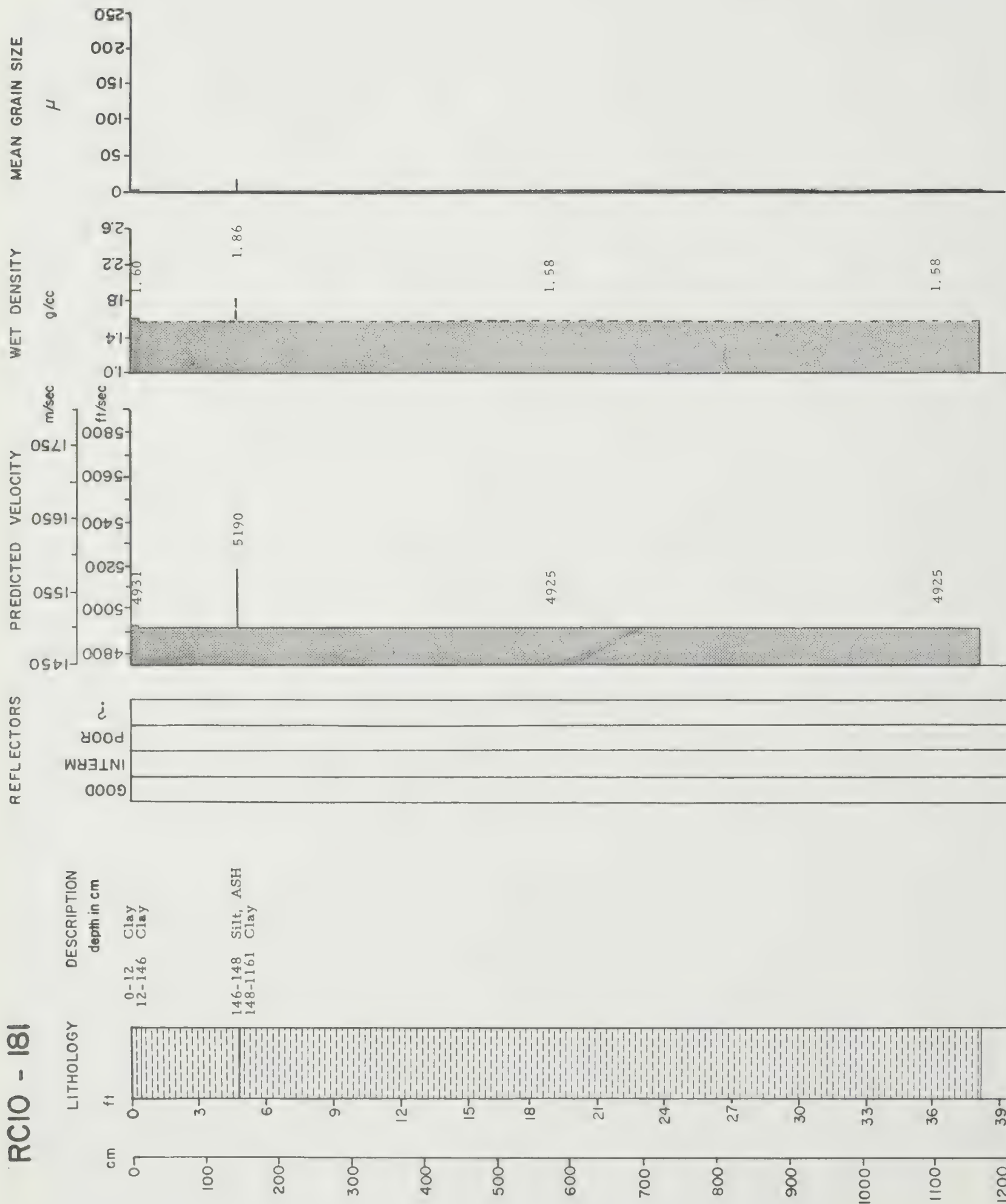
4925

4918



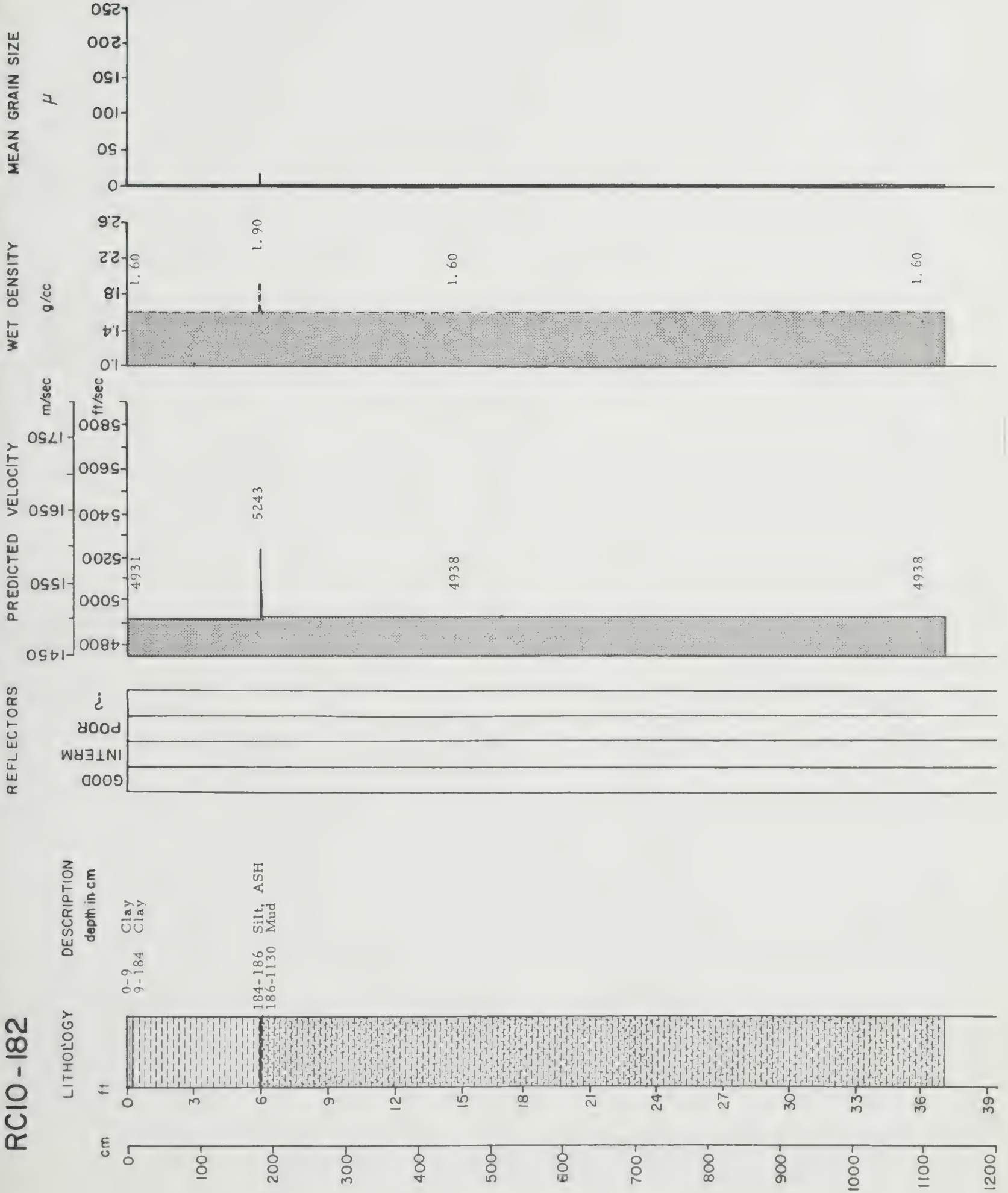


# RCIO - 181

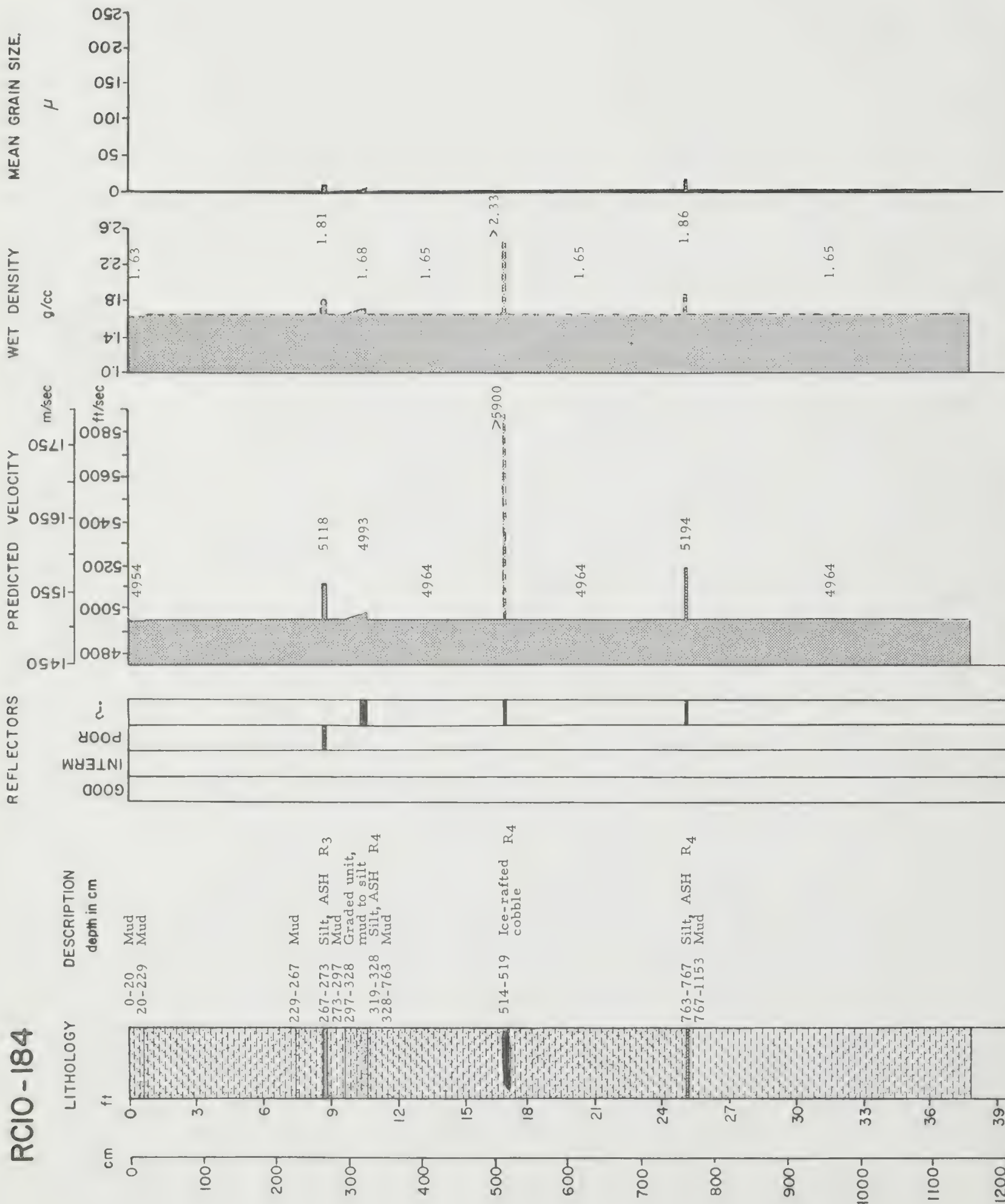




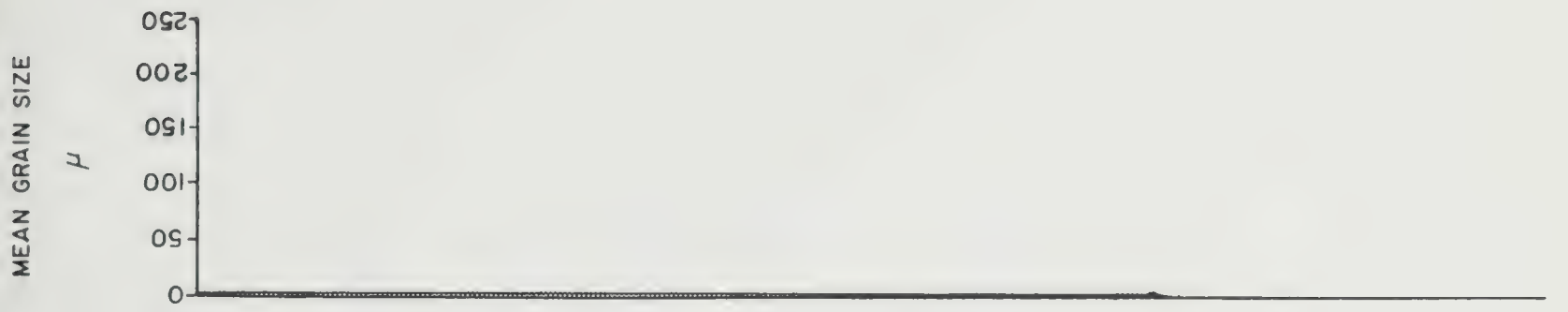
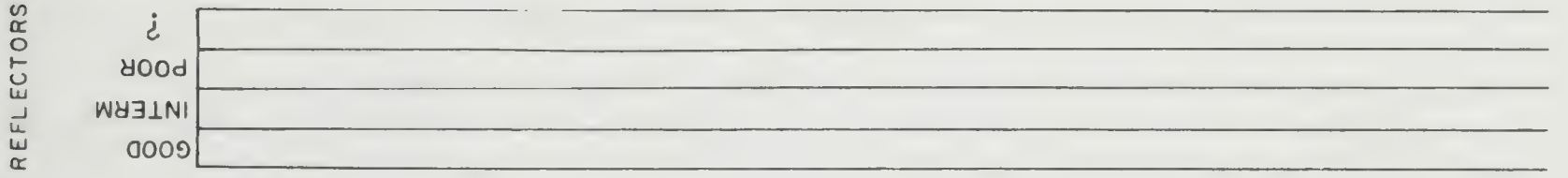
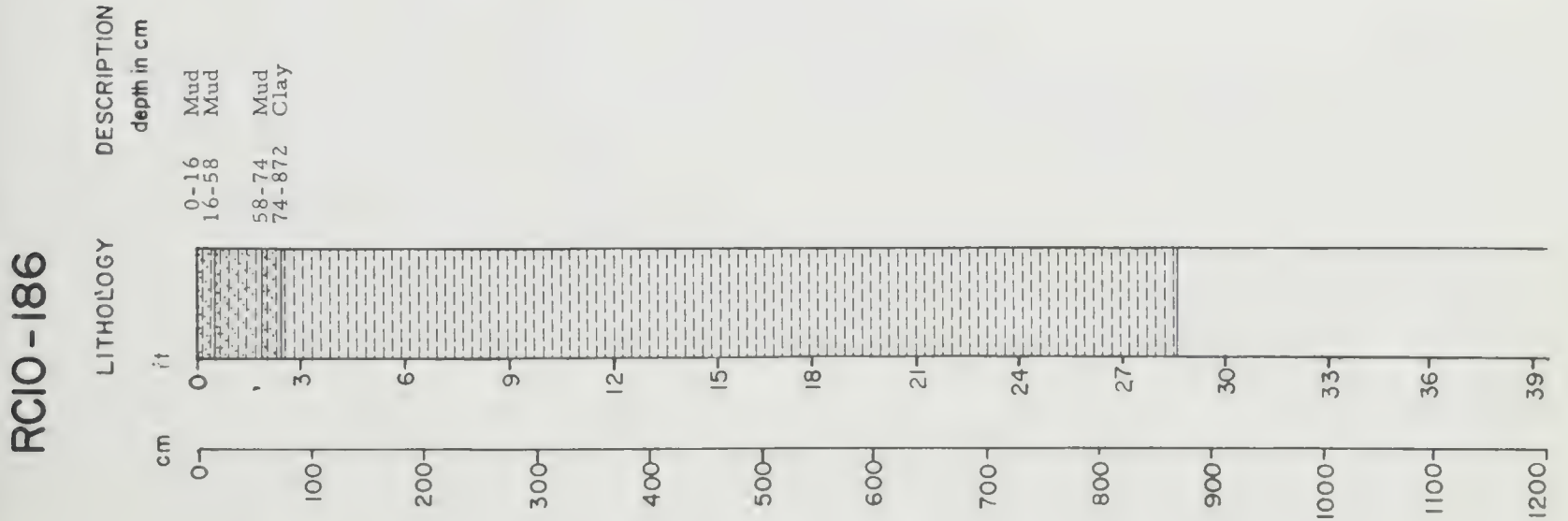
# RC10-182



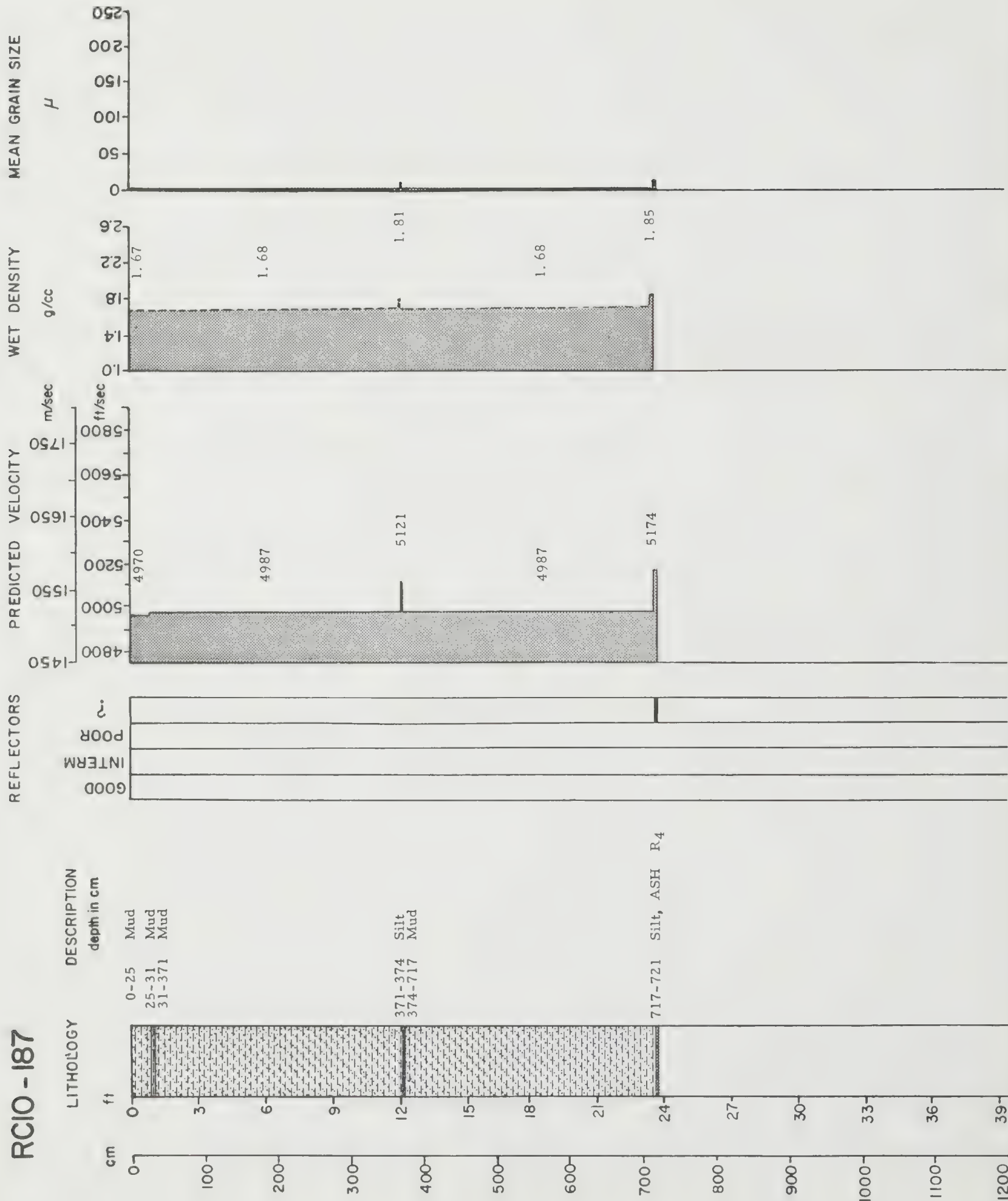
# RCIO-184



RCIO-186

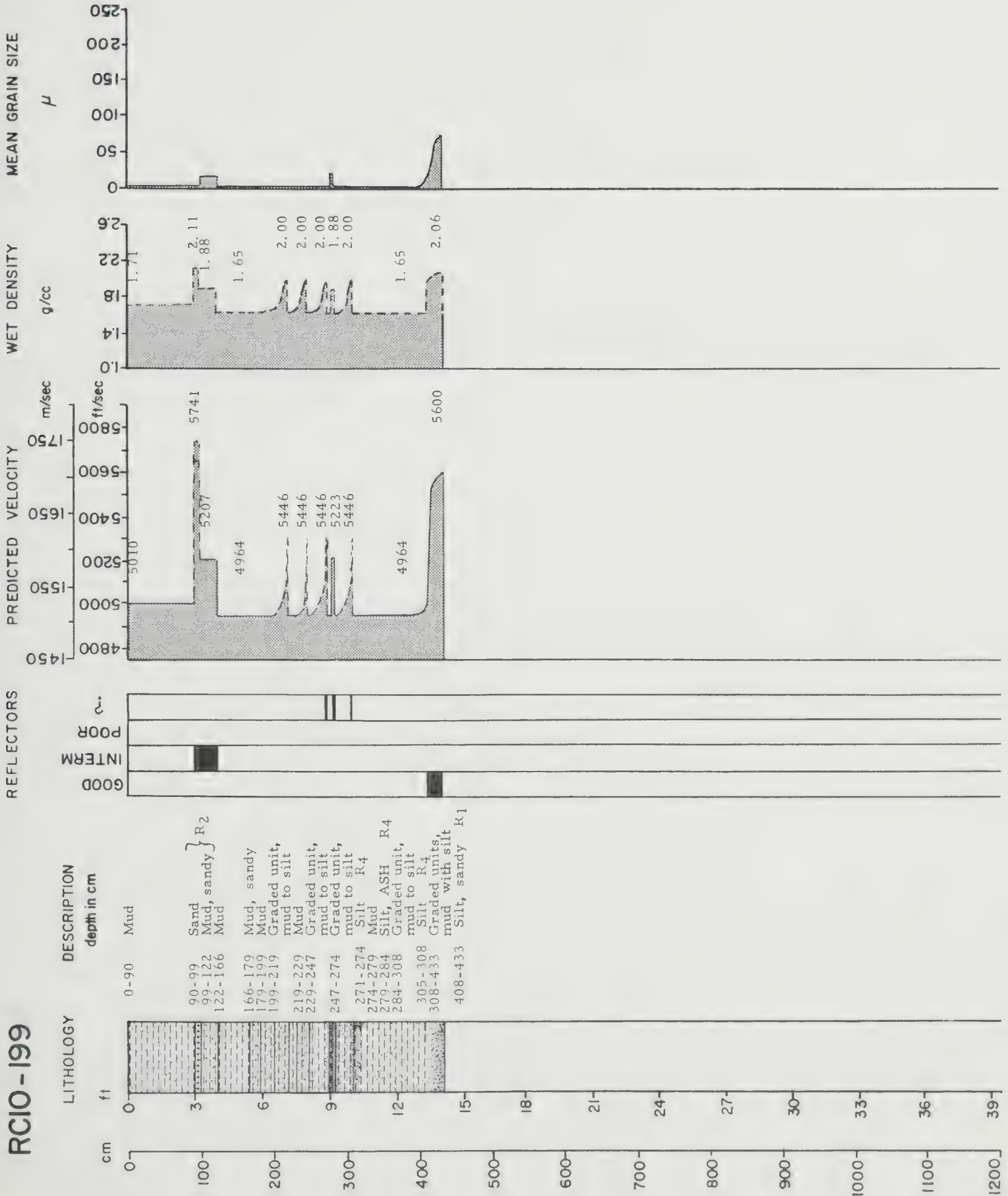


# RC10 - 187

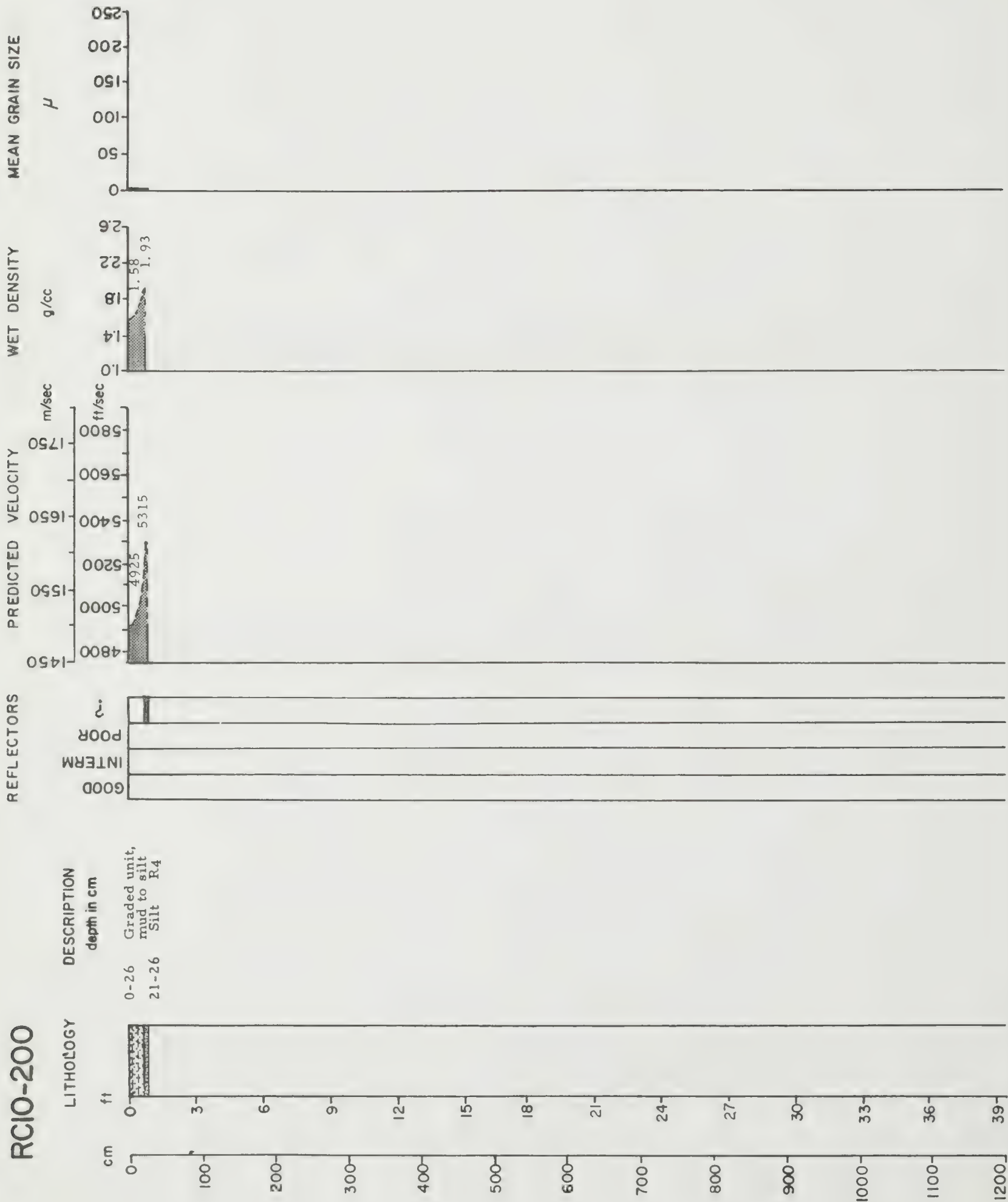




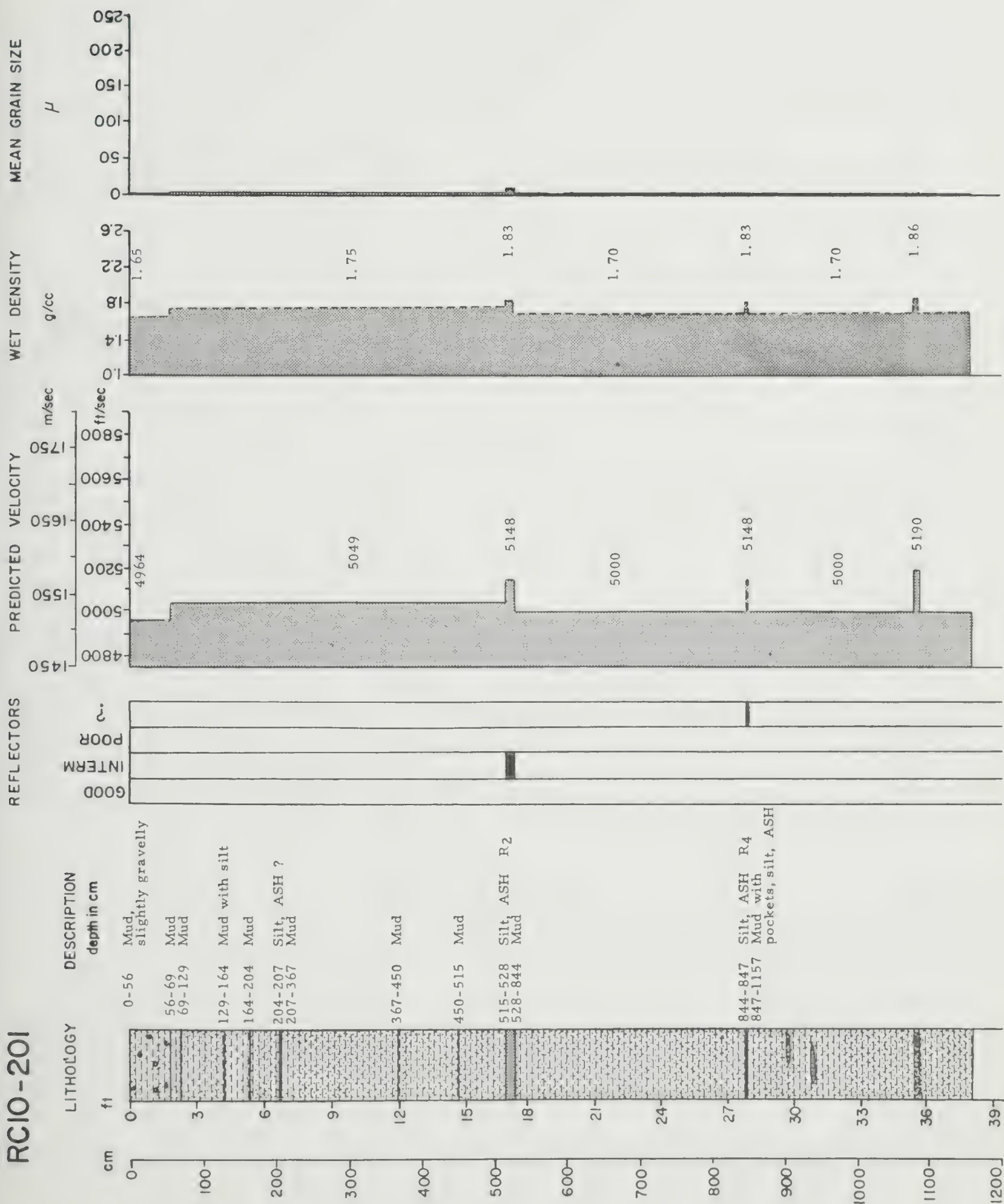
# RCIO-199



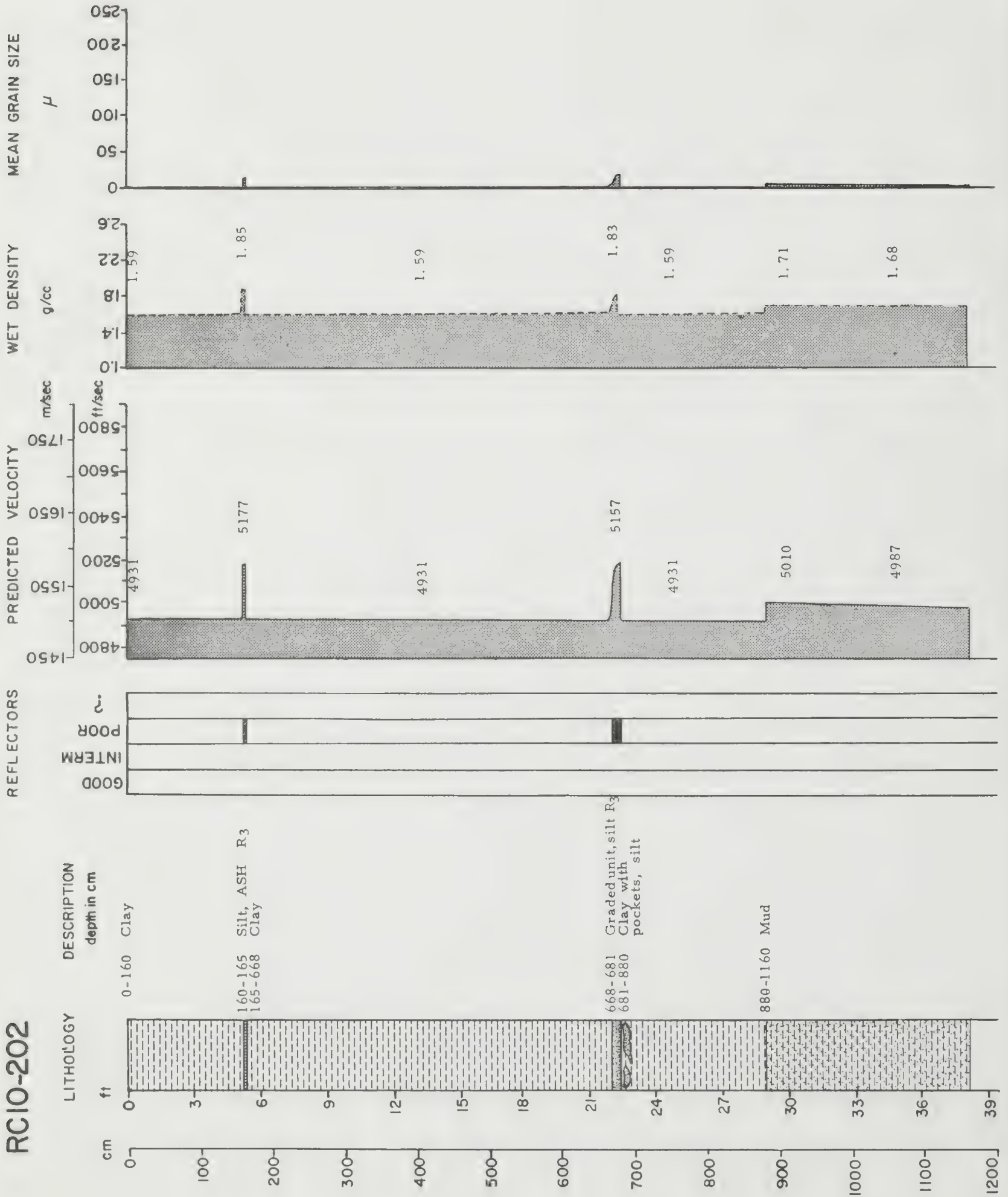
RC10-200



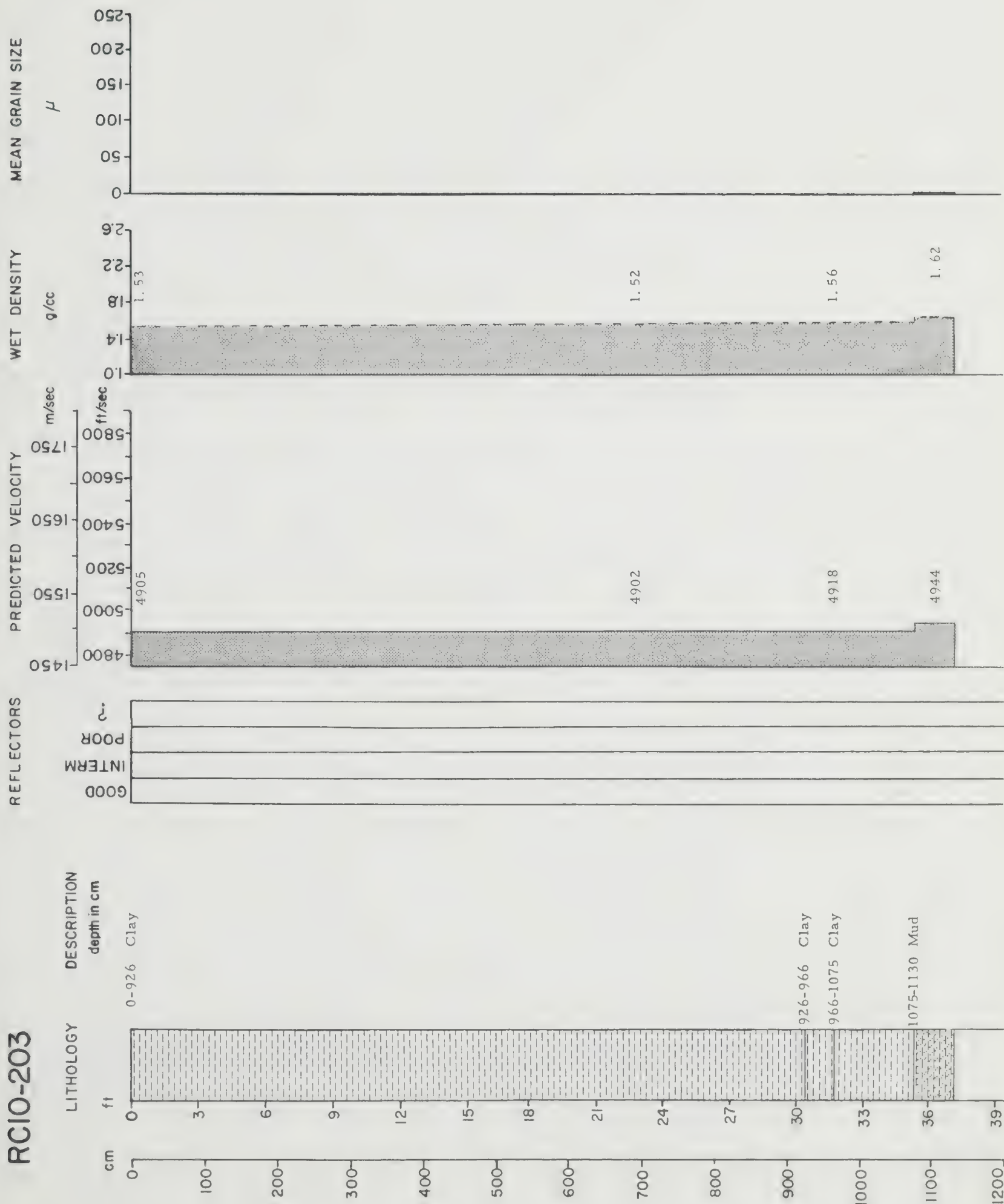
RC10-201

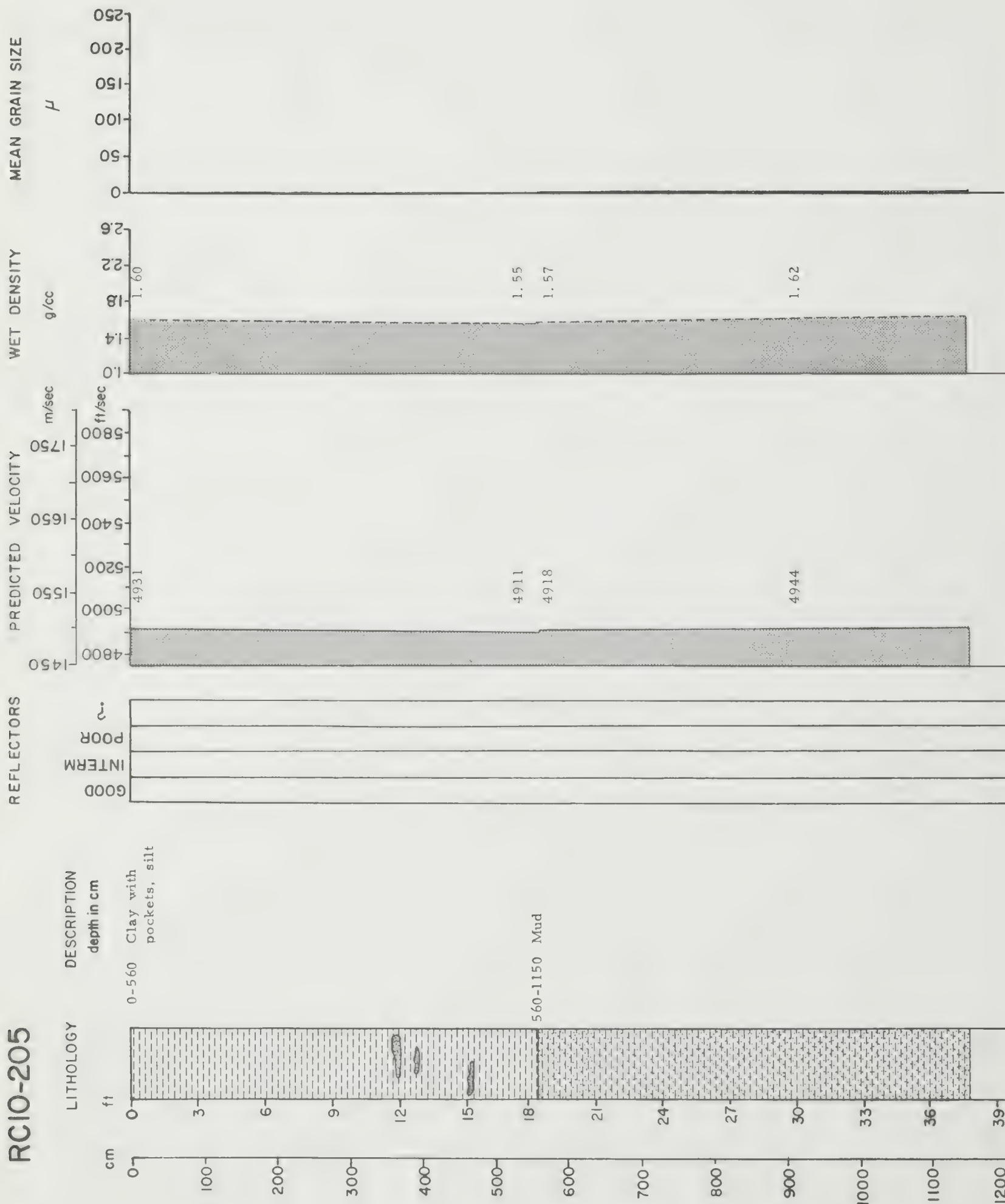


RC10-202

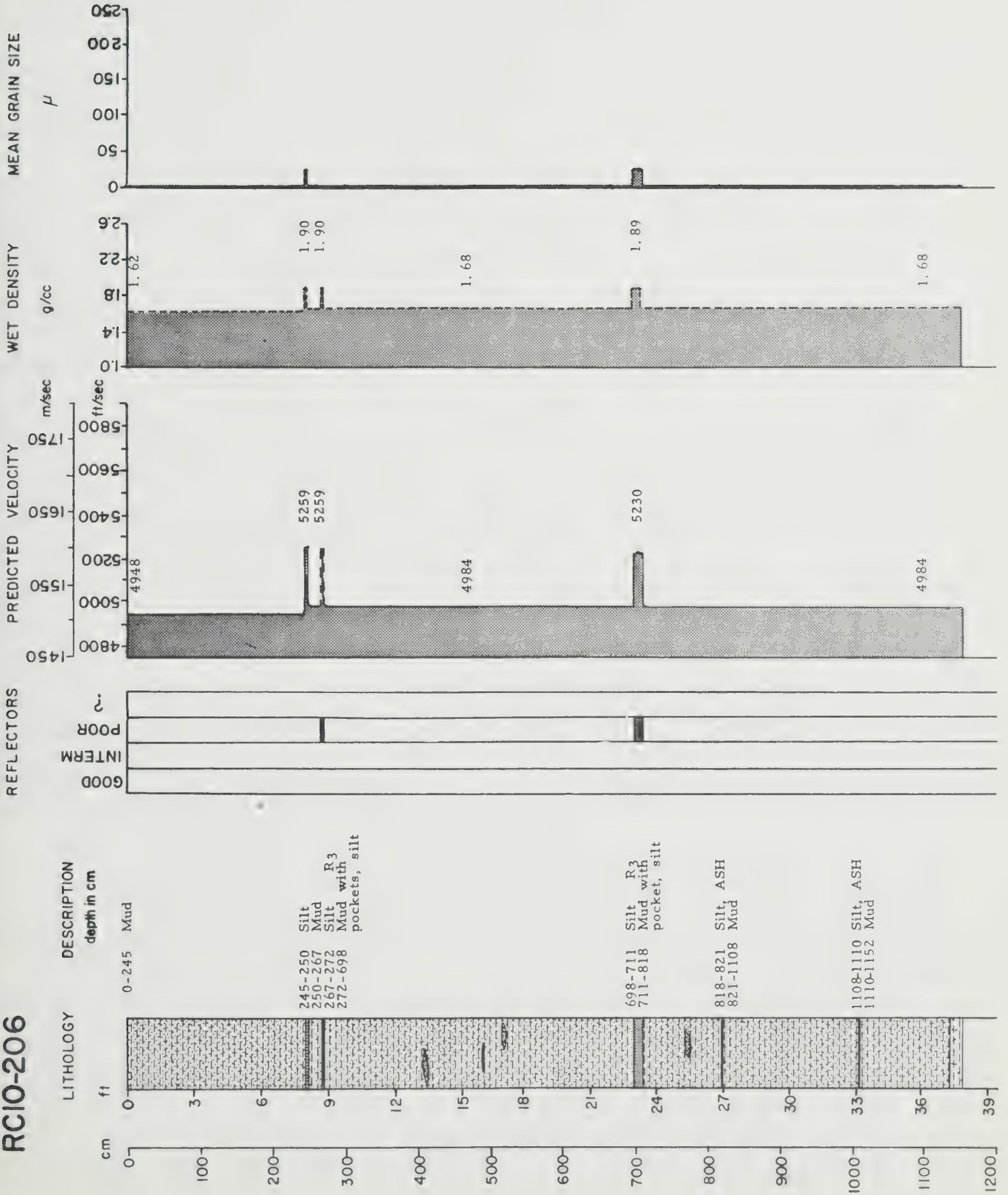




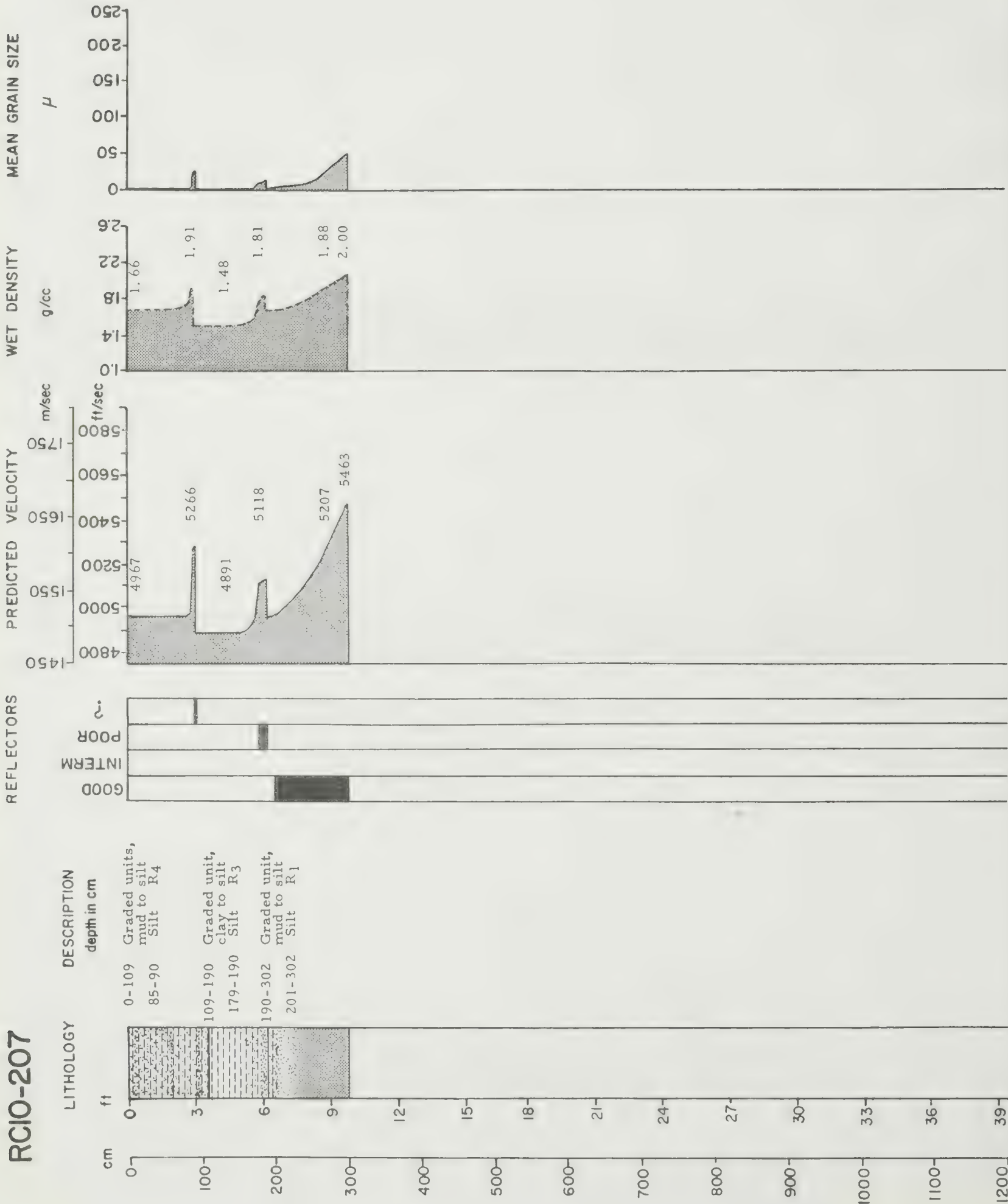




# RC10-206

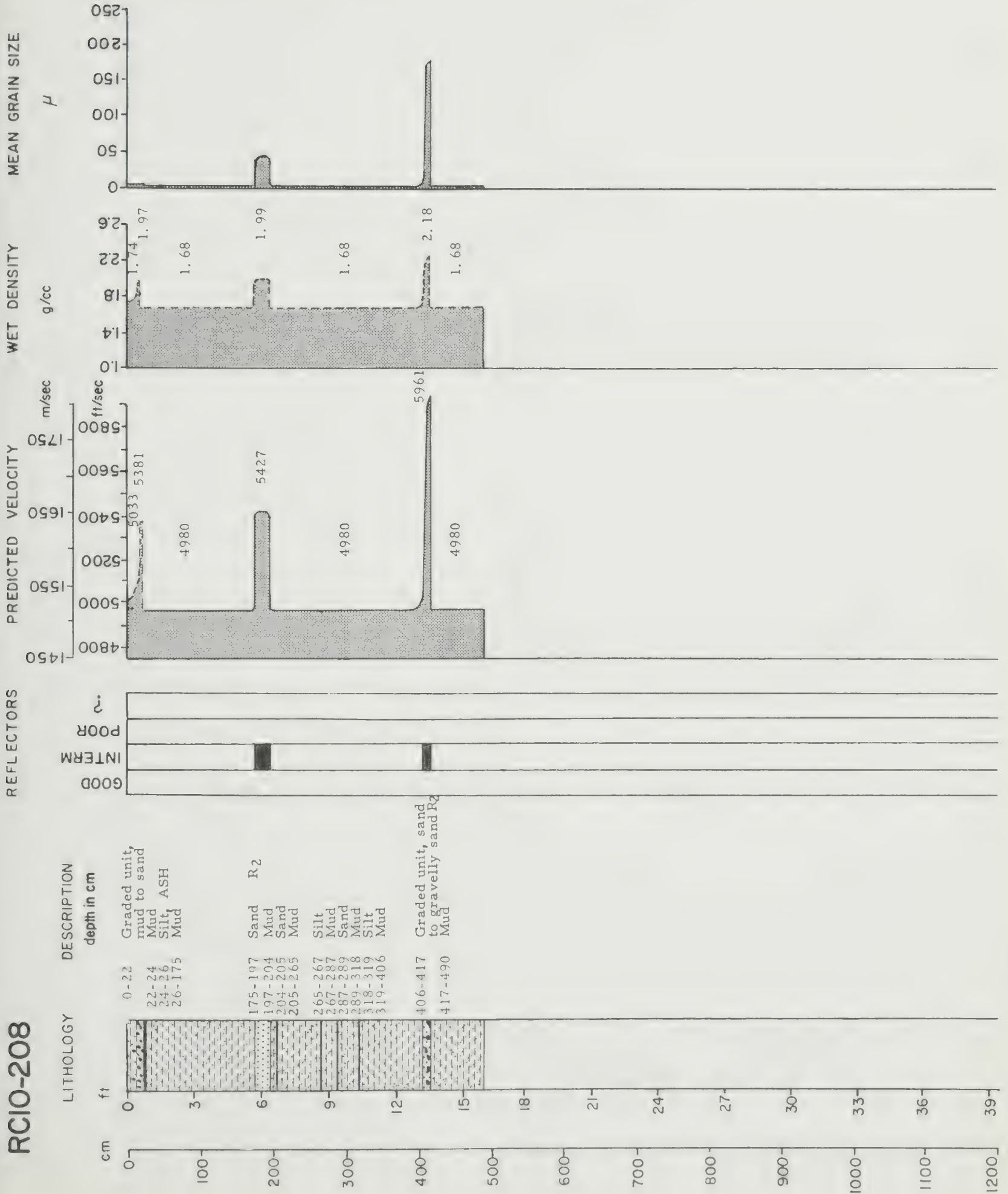


RCIO-207





# RCIO-208



RC10 - 210

REFLECTORS

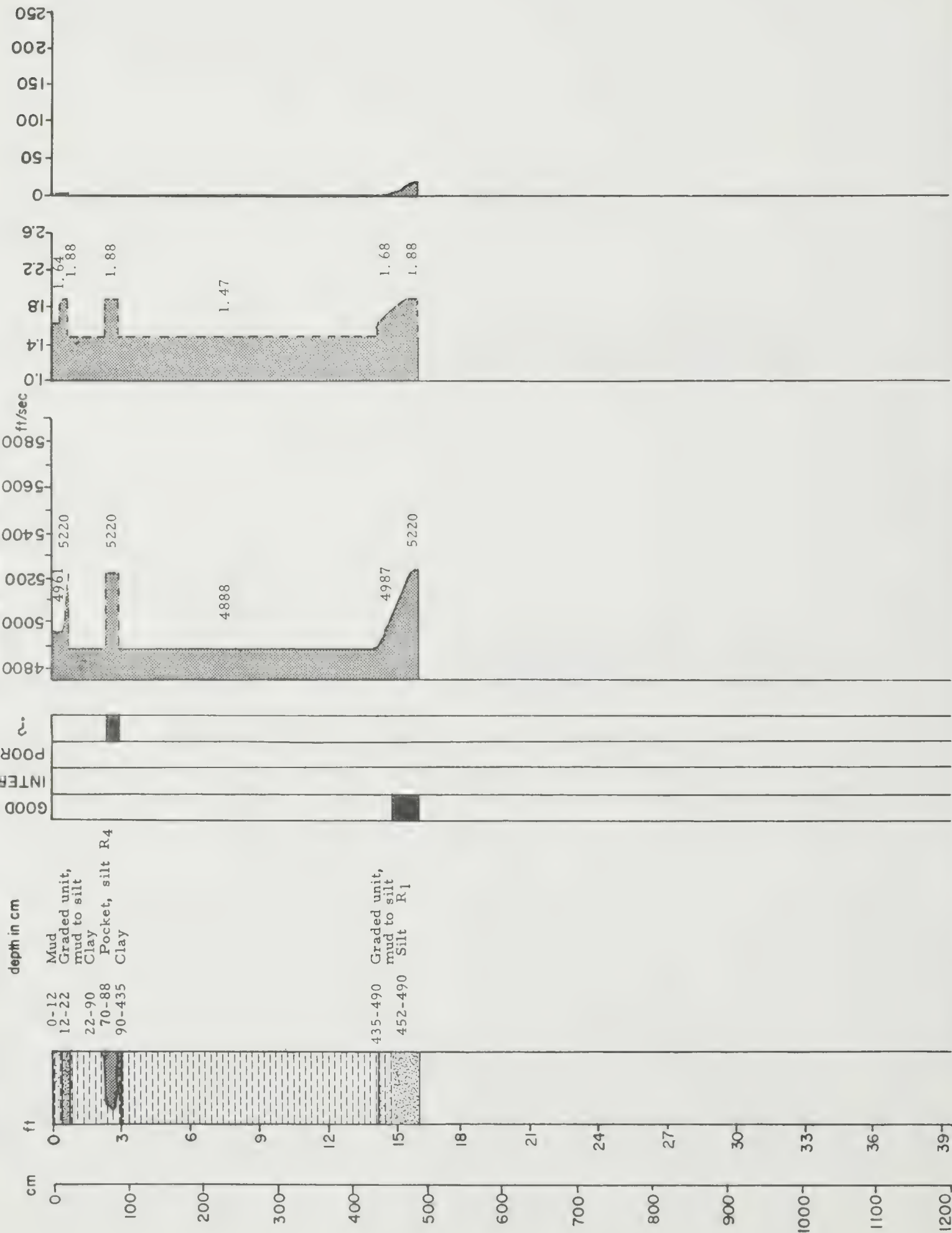
PREDICTED VELOCITY

WET DENSITY

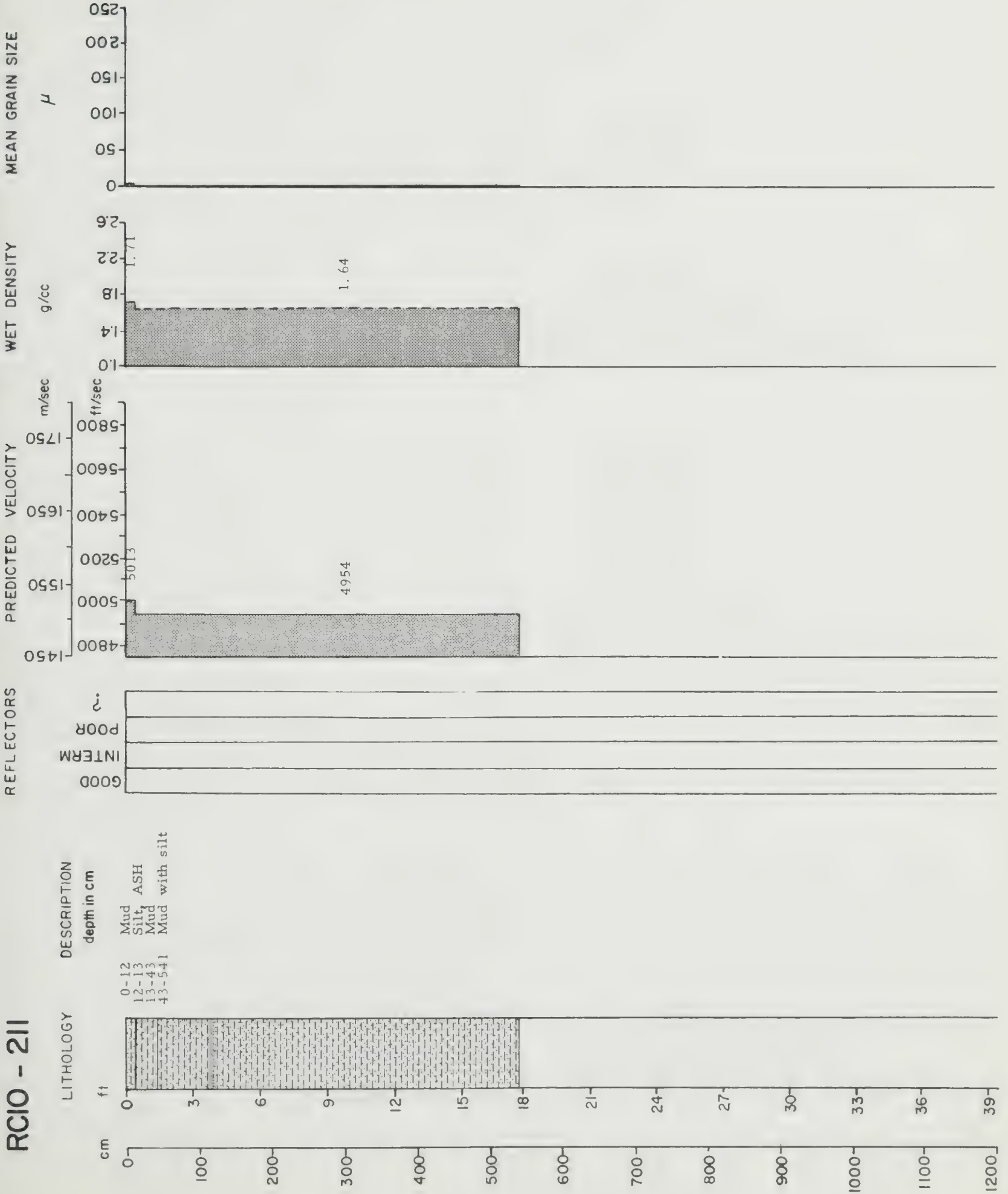
MEAN GRAIN SIZE

DESCRIPTION

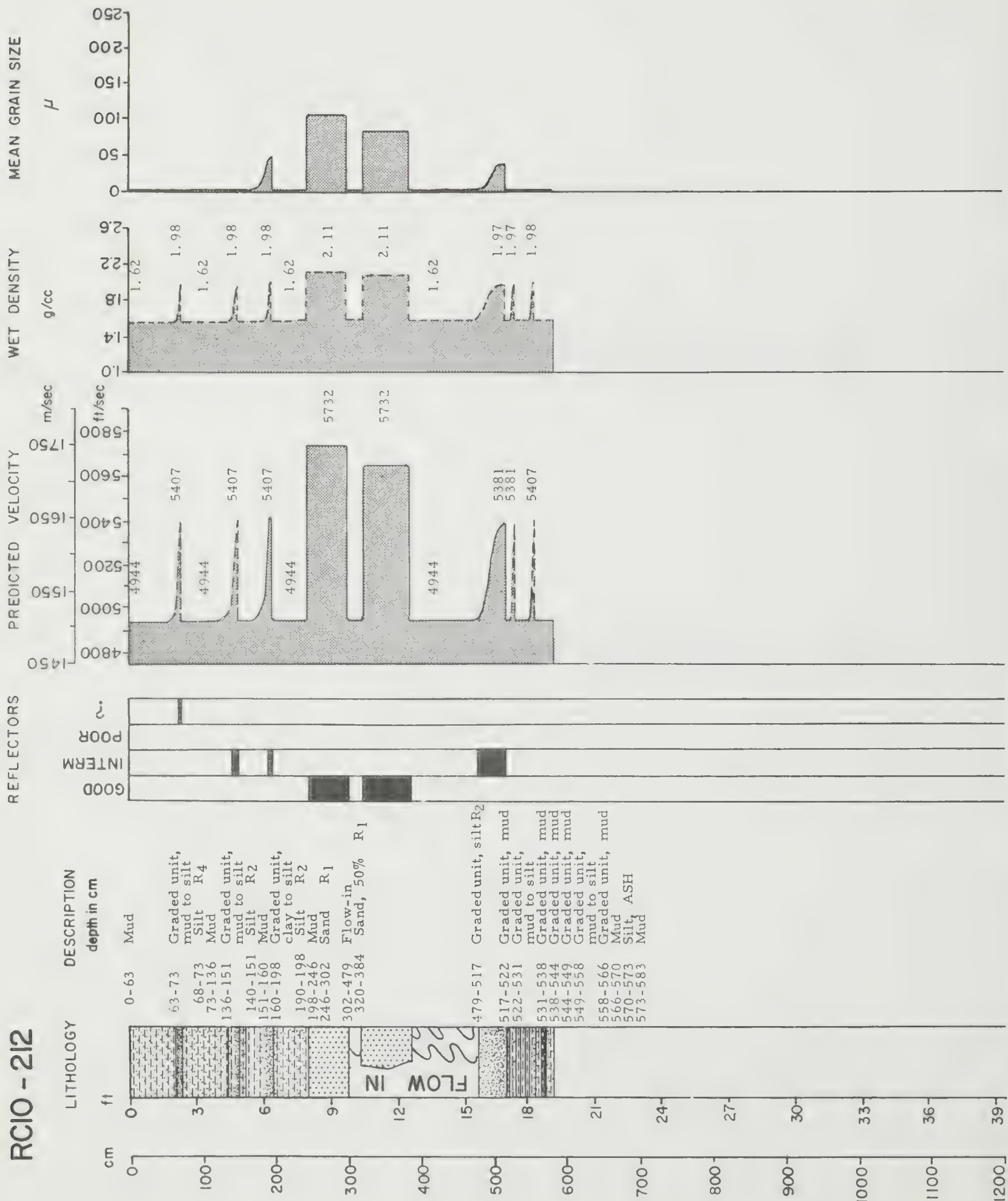
LITHOLOGY



RCIO - 211

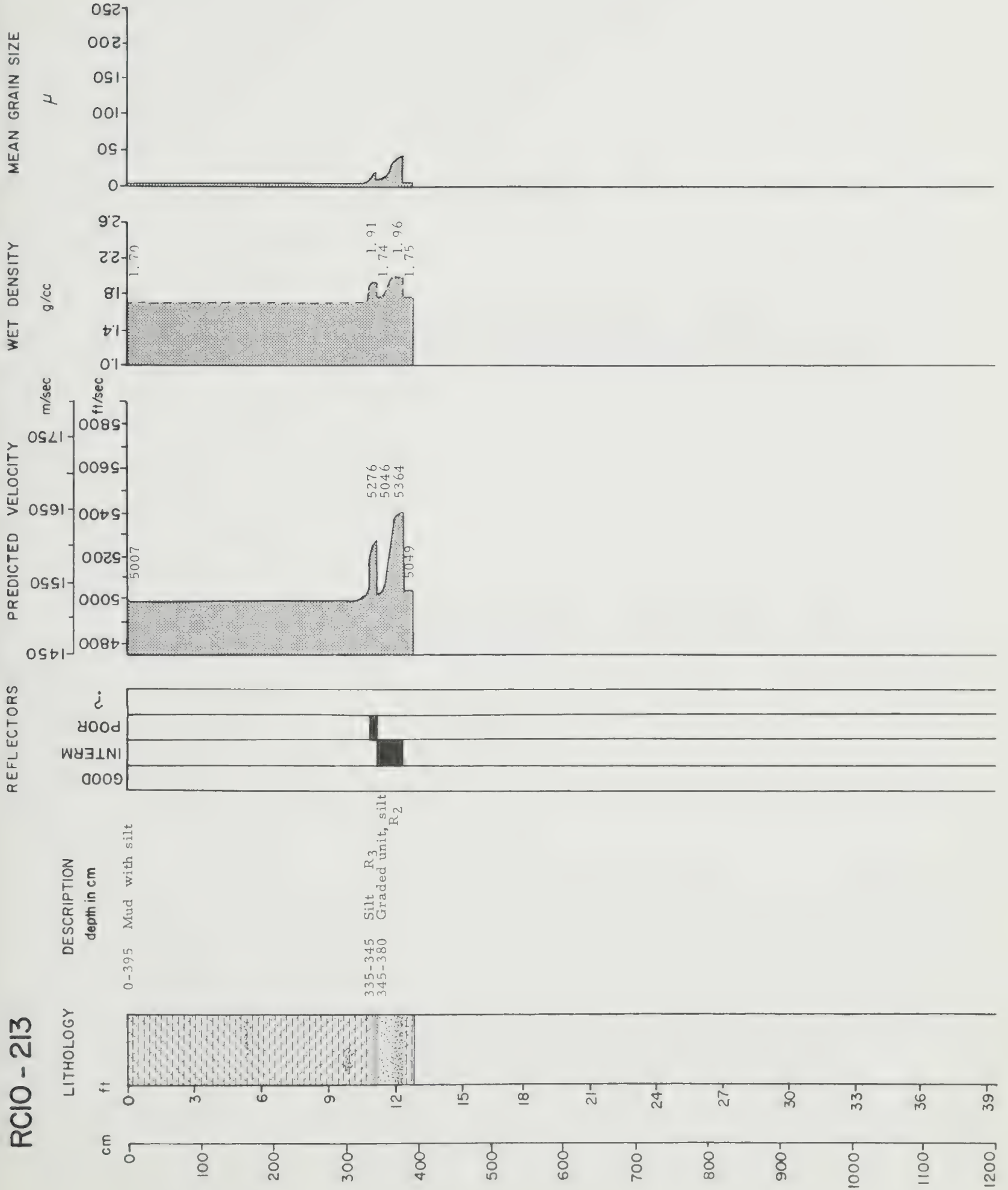


# RCIO - 212

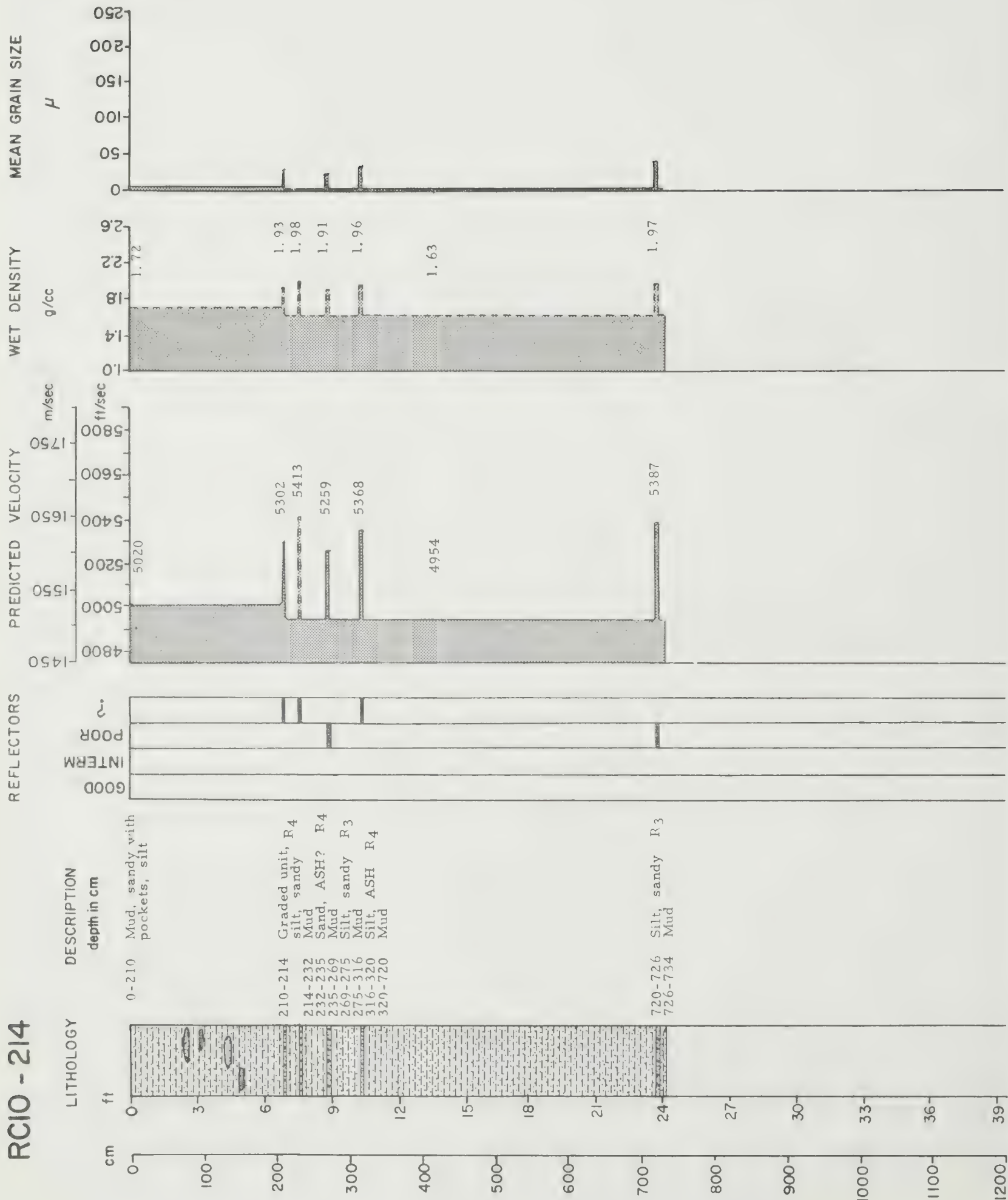


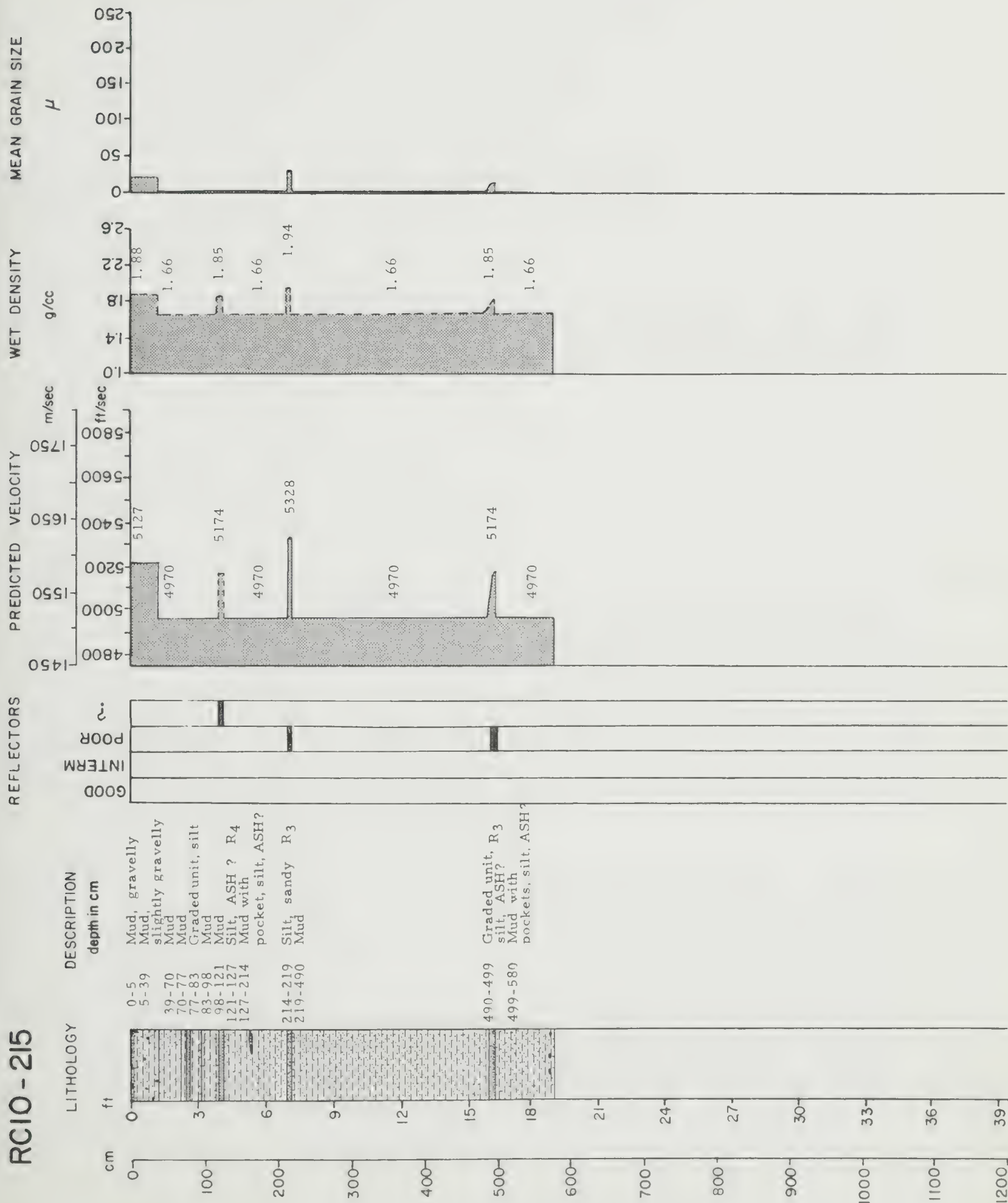


RCIO - 213

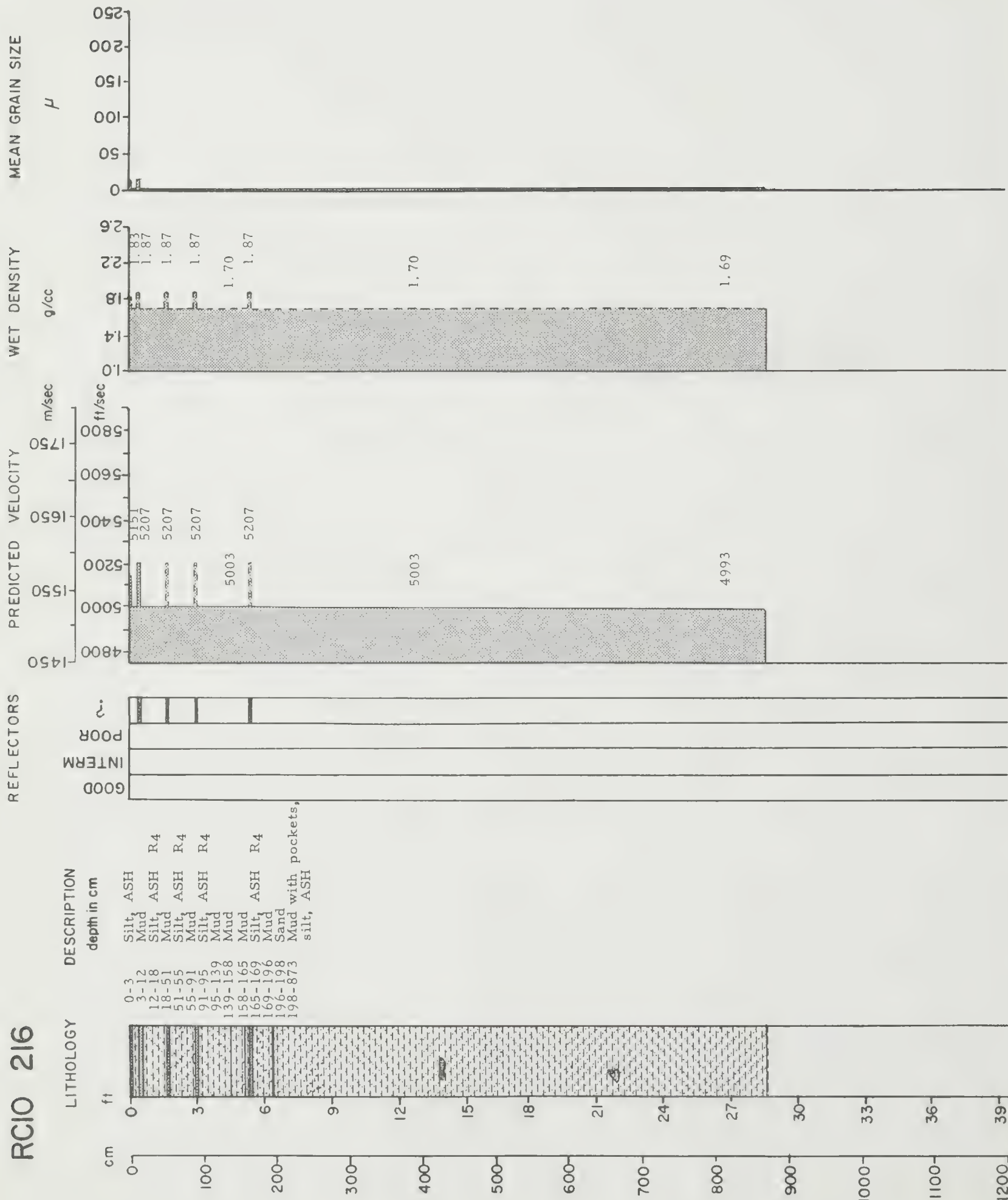


# RCIO - 214



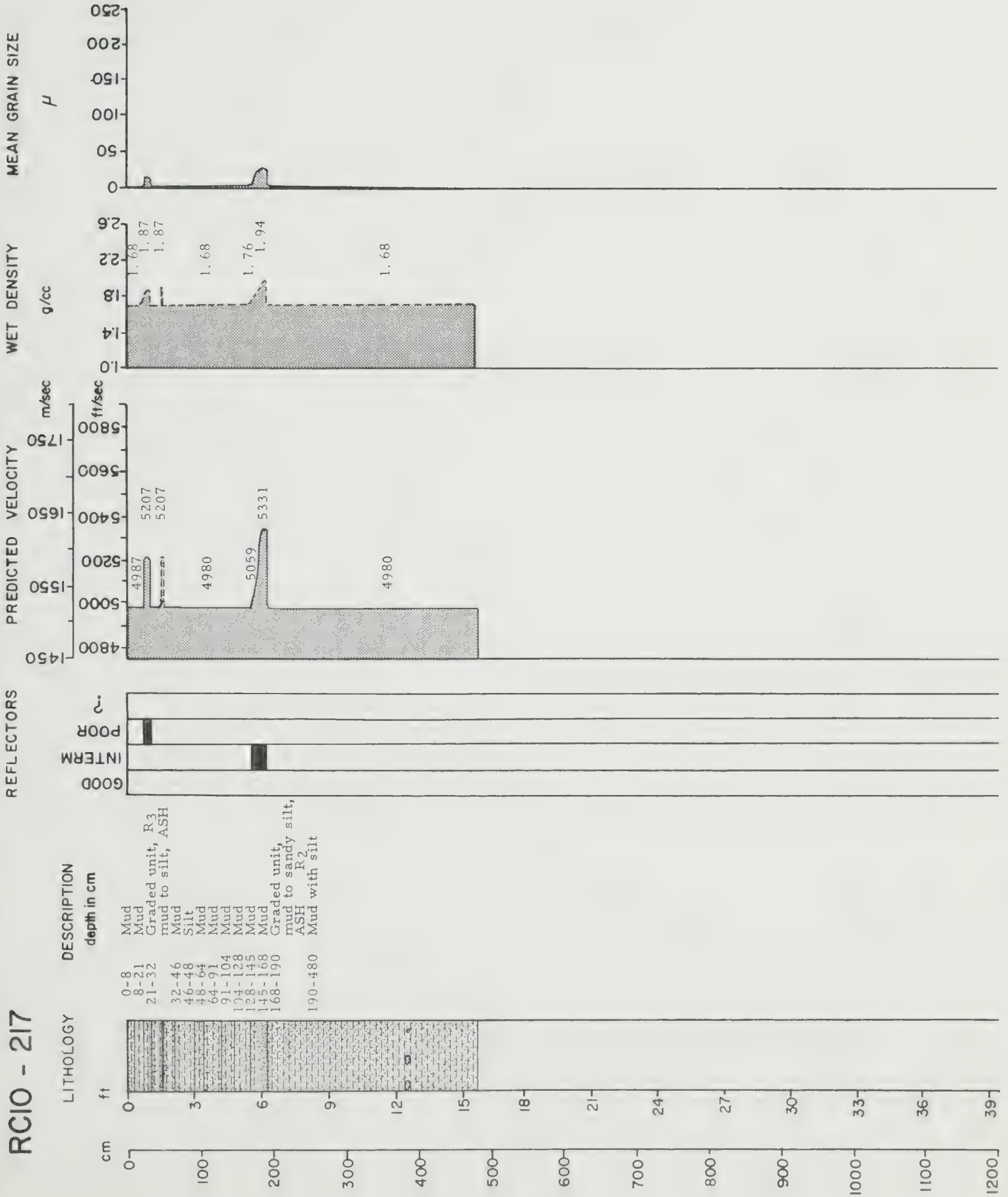


RCIO 216

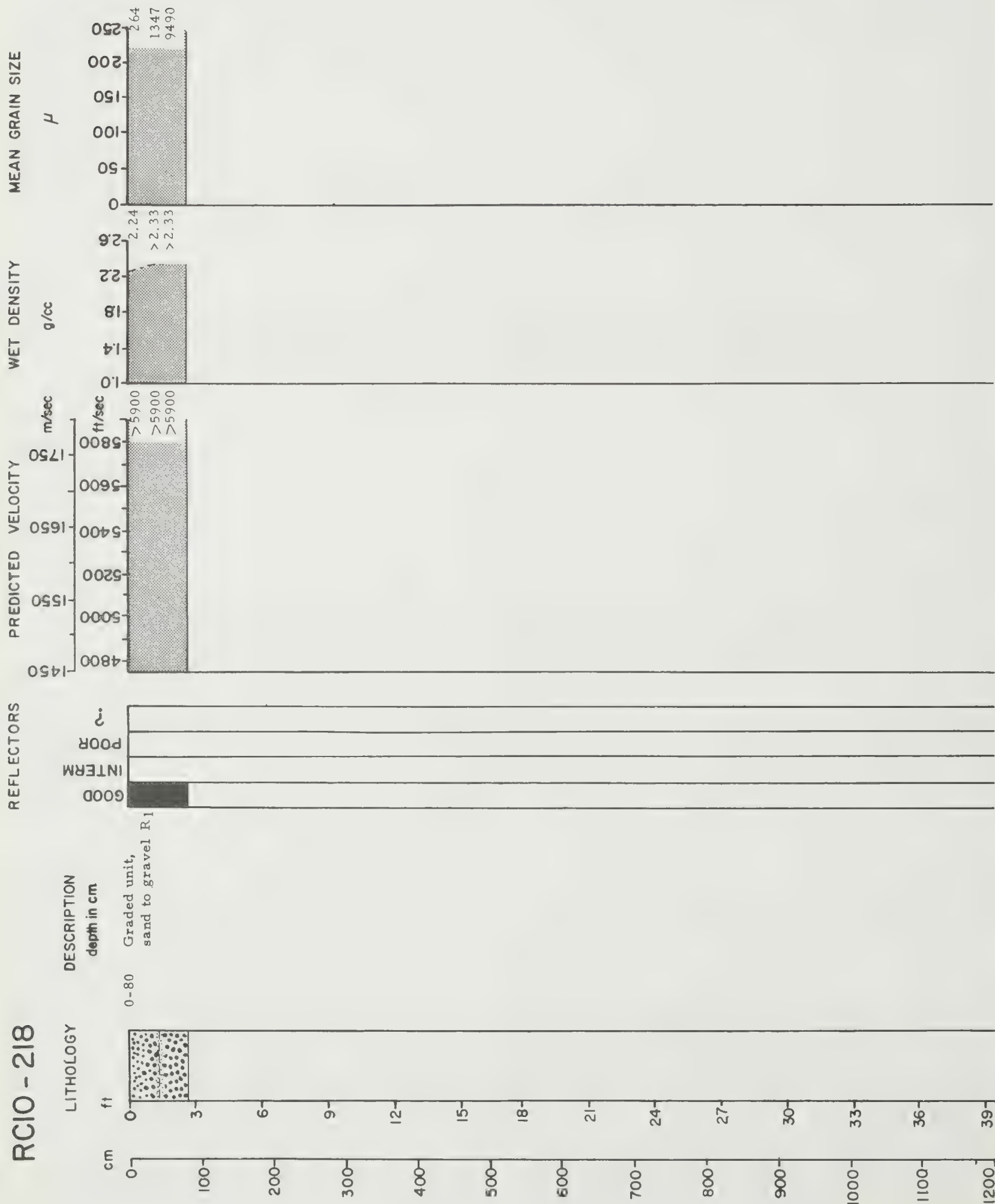


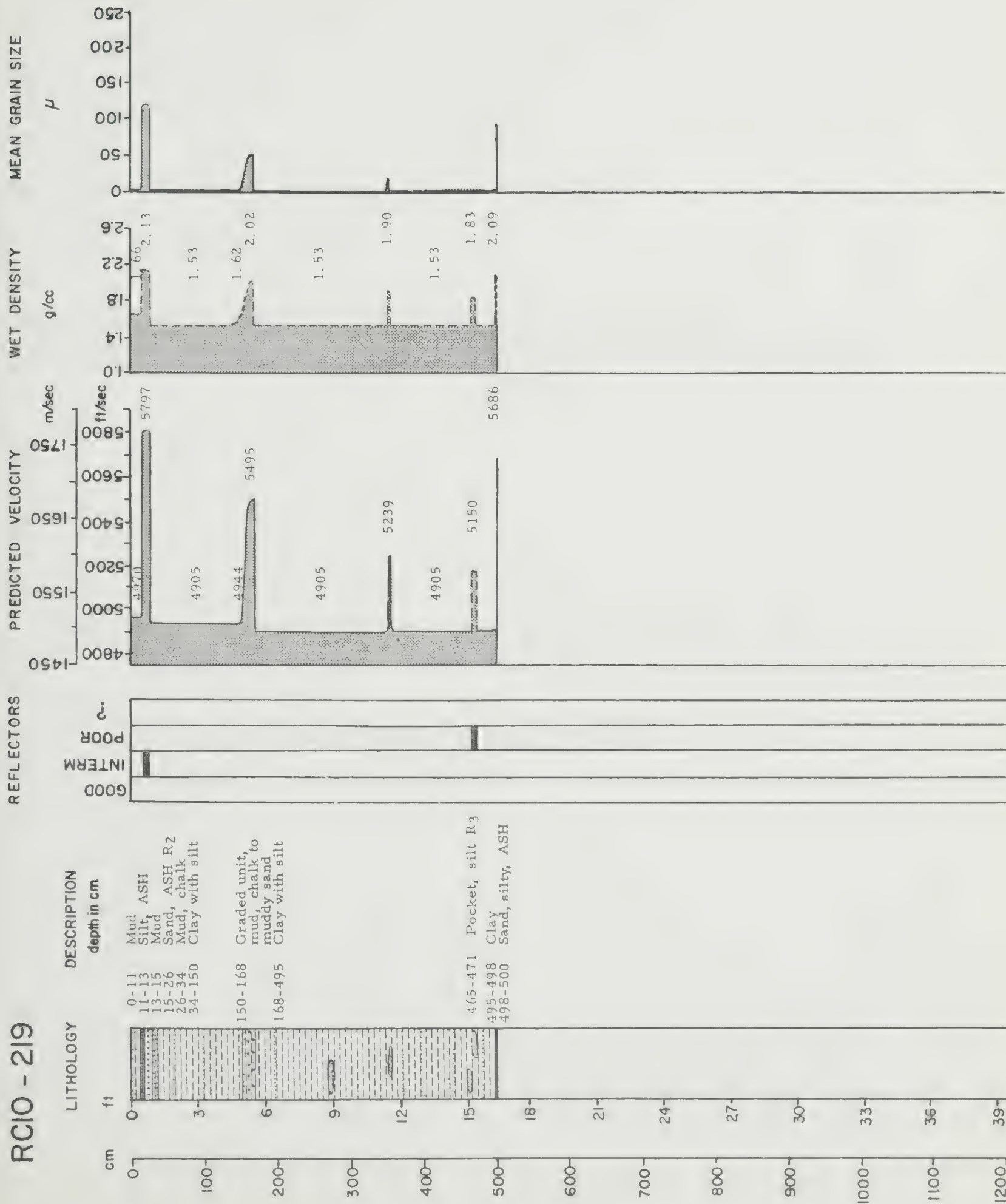


# RCIO - 217

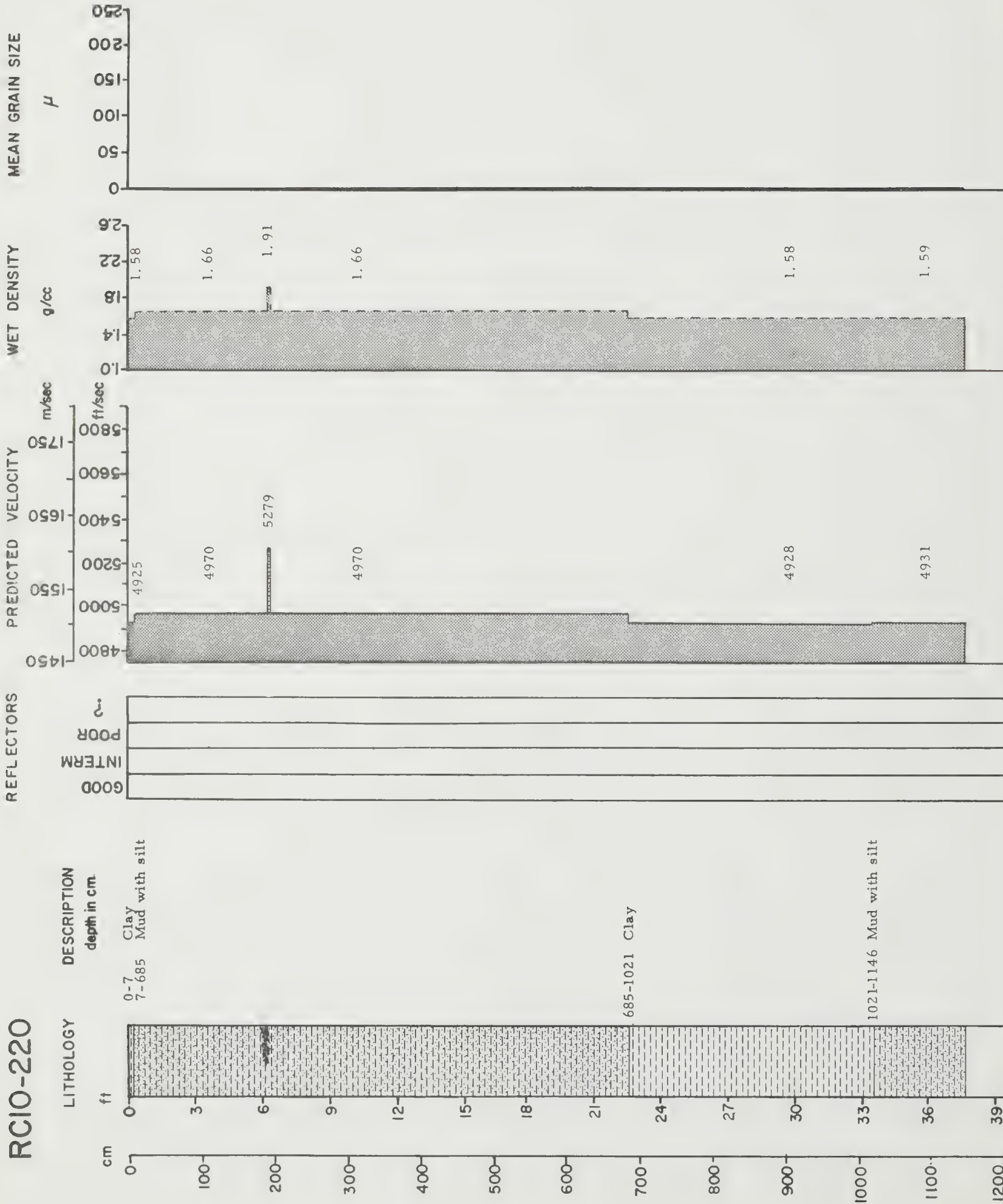


RCIO - 218



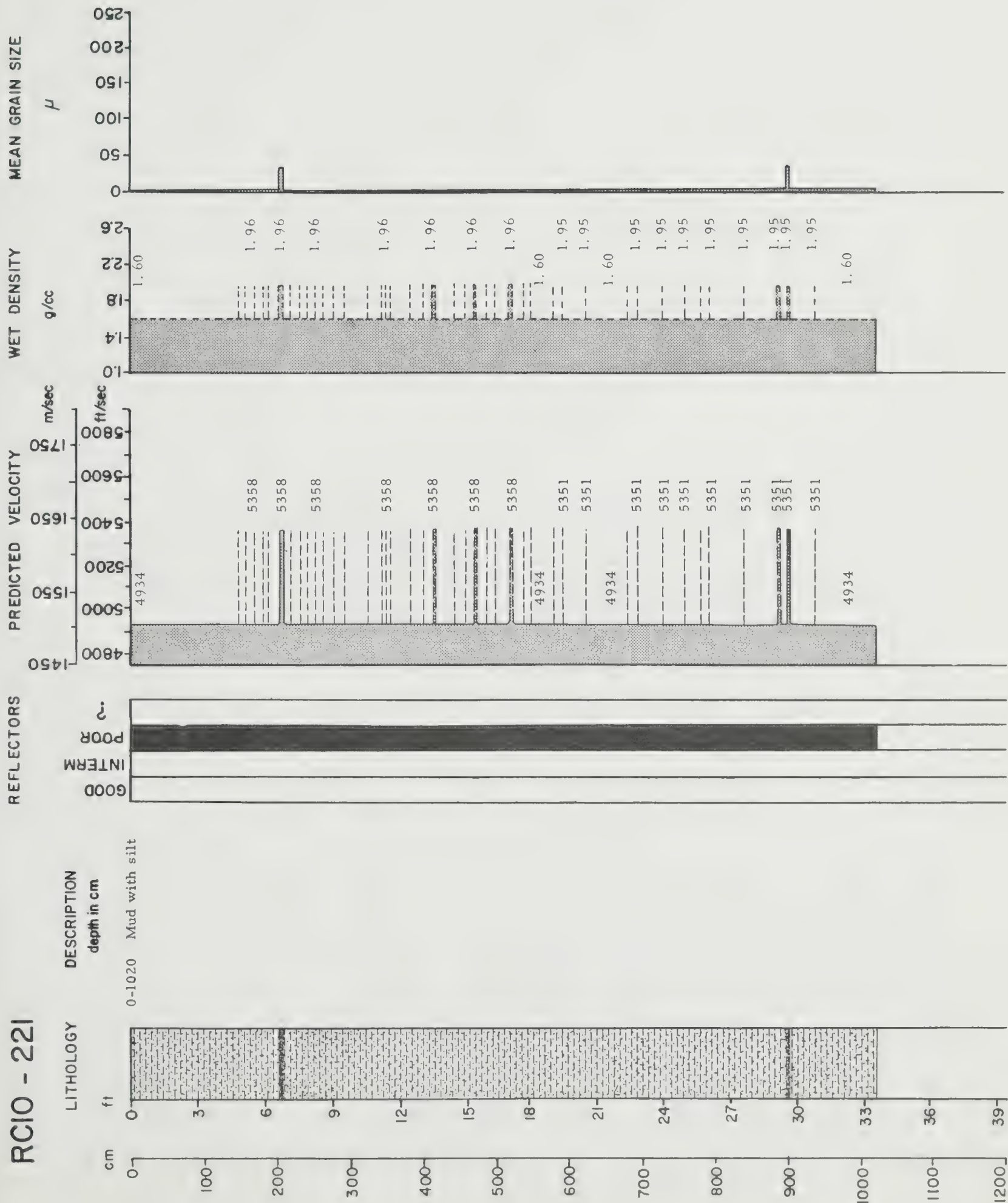


# RCIO-220

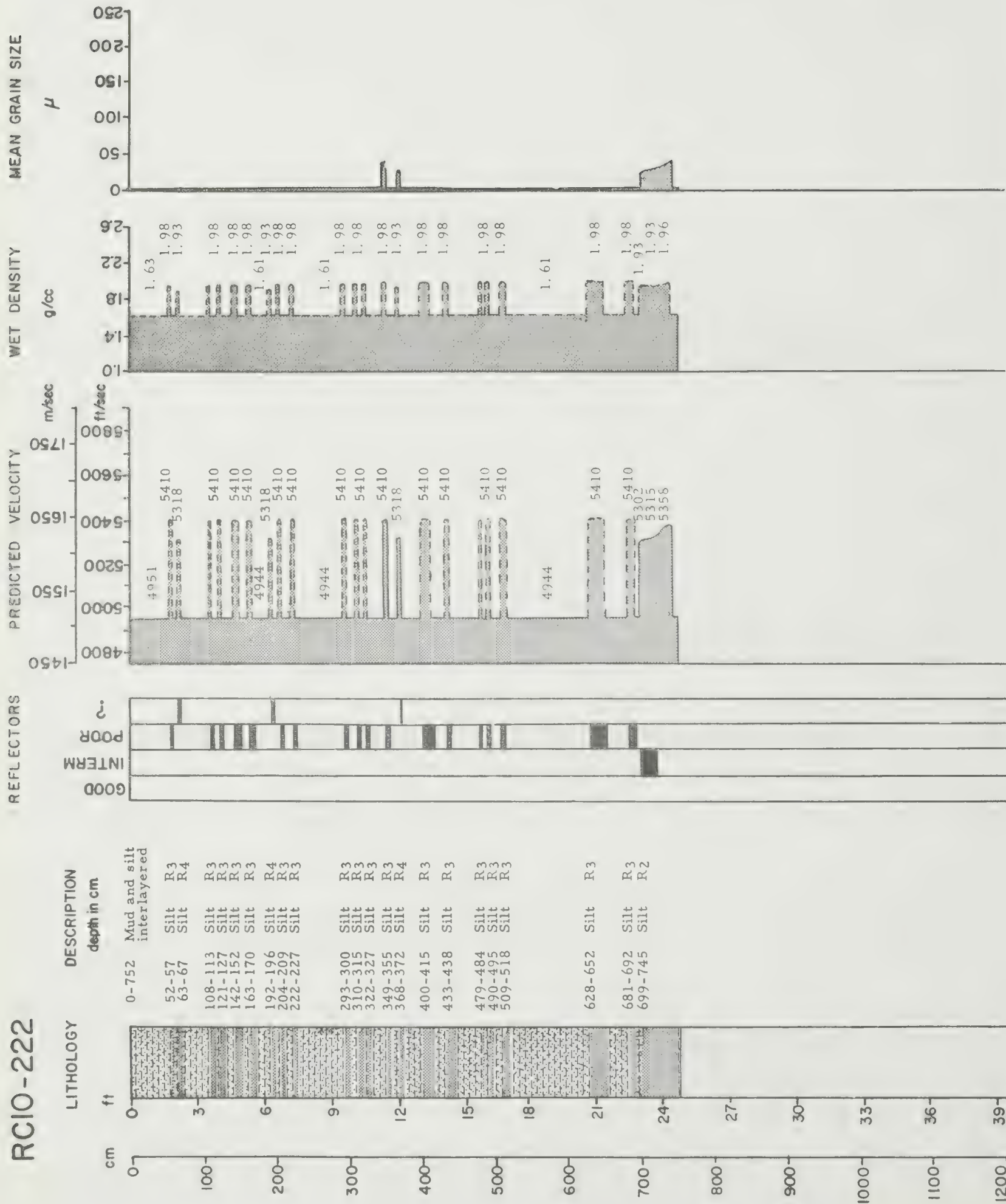


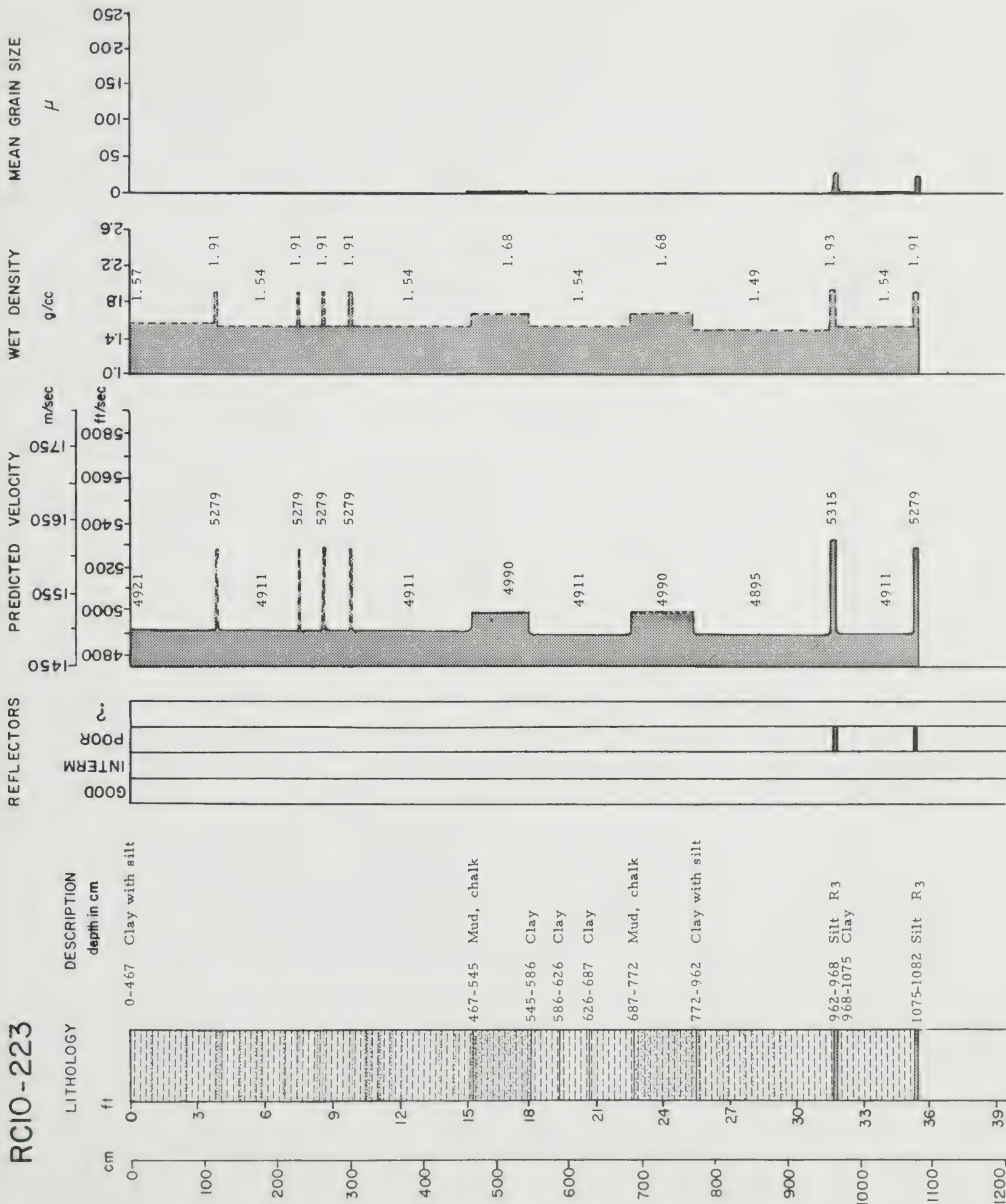


# RCIO - 221

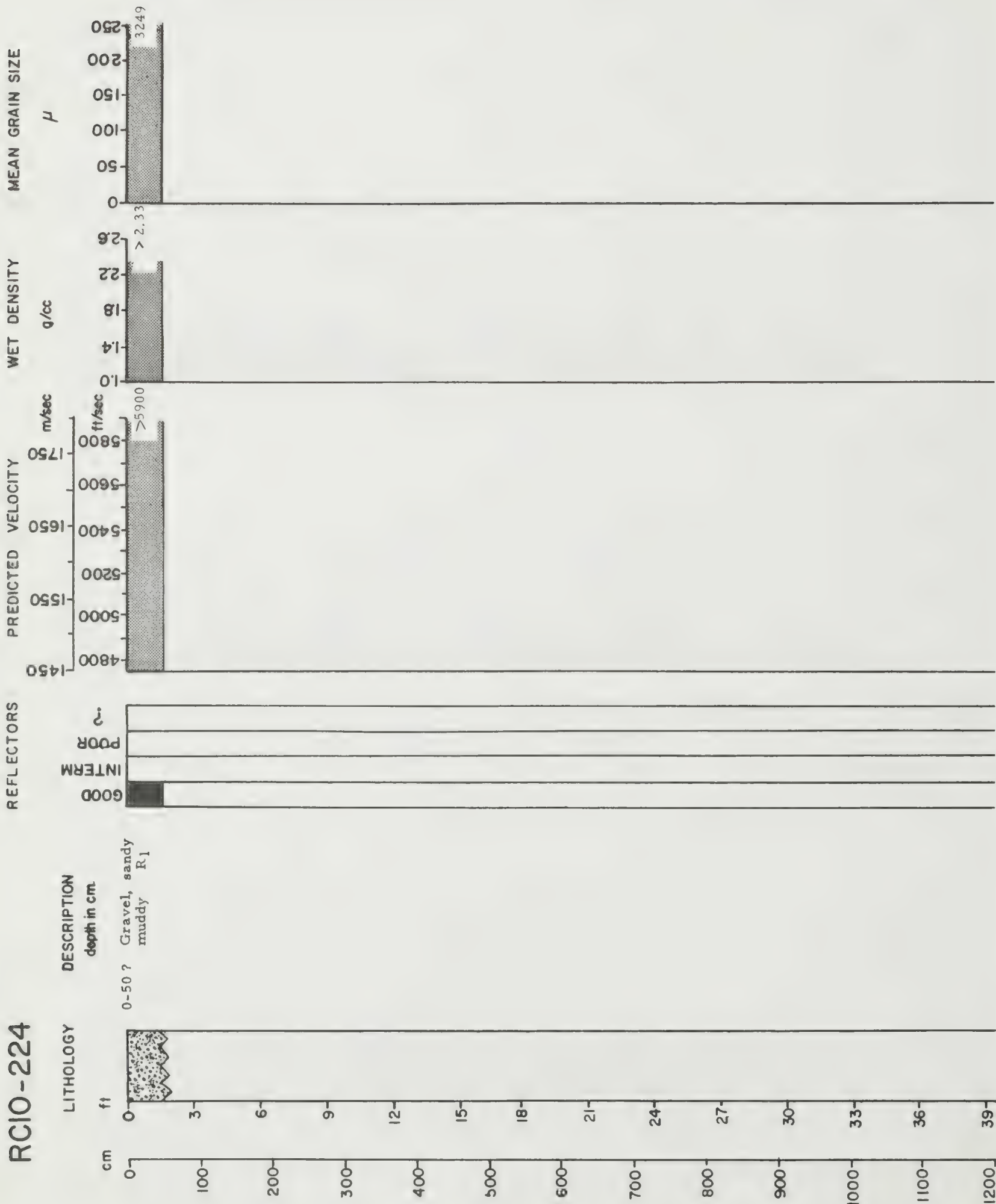


# RC10-222

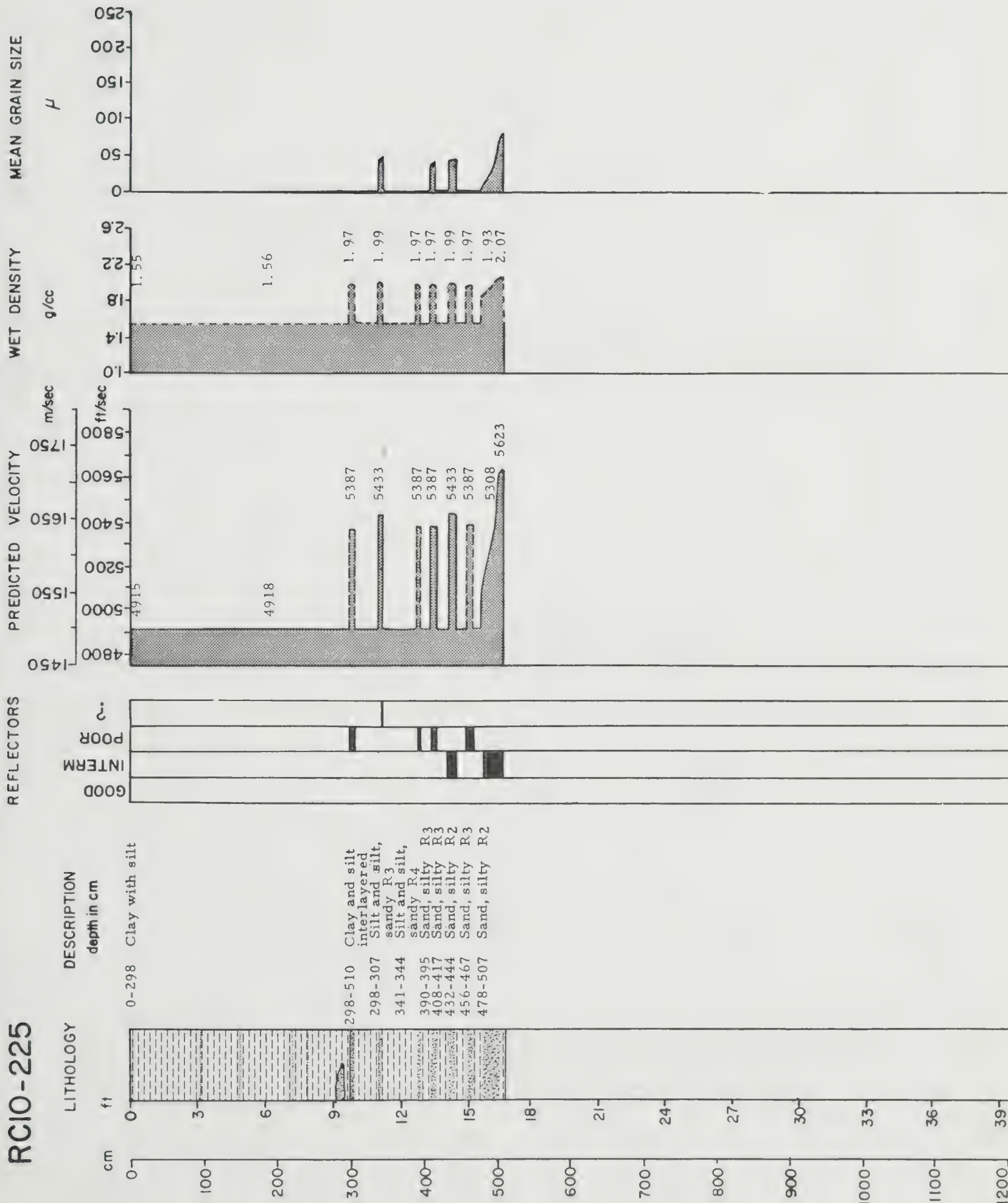




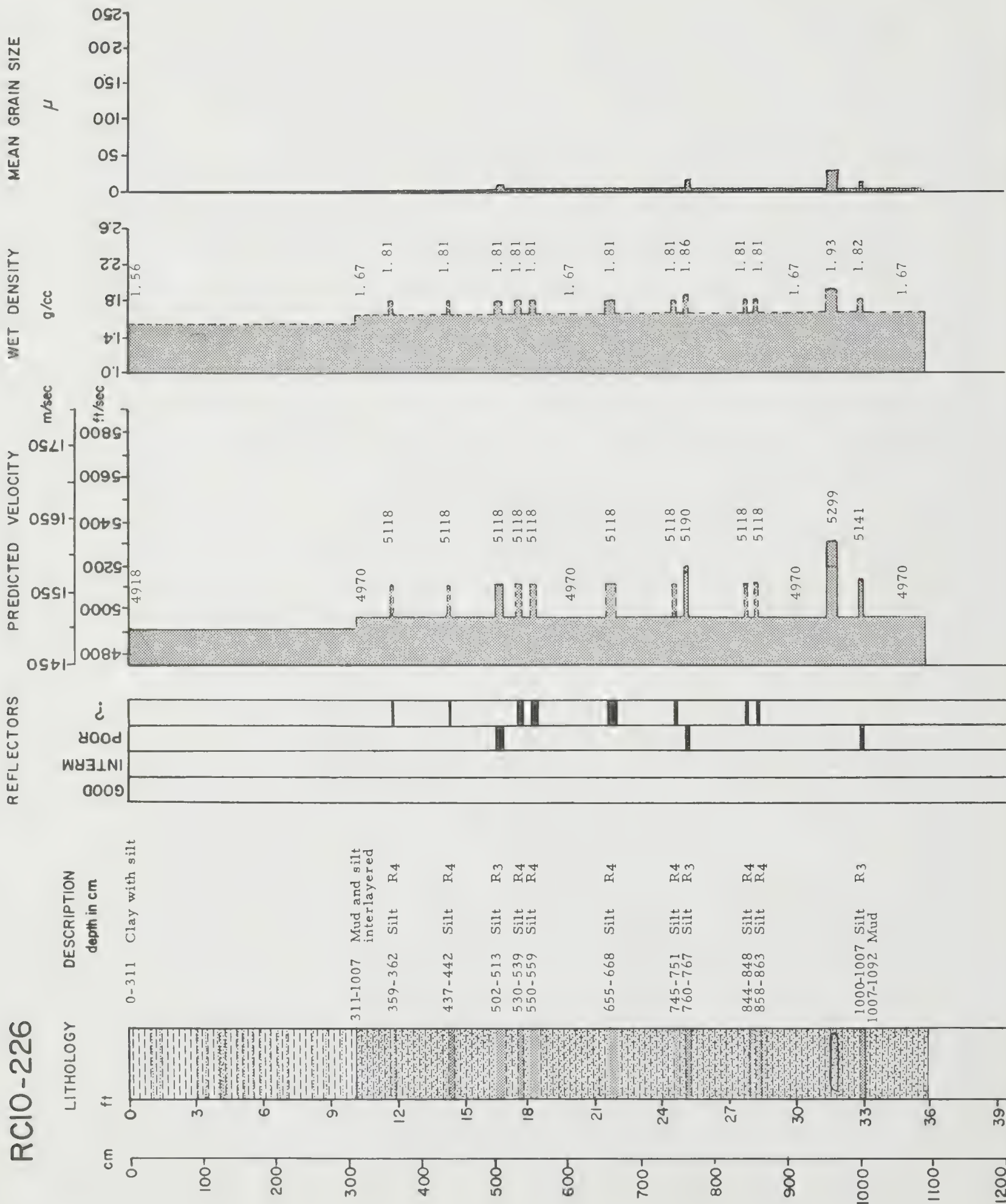






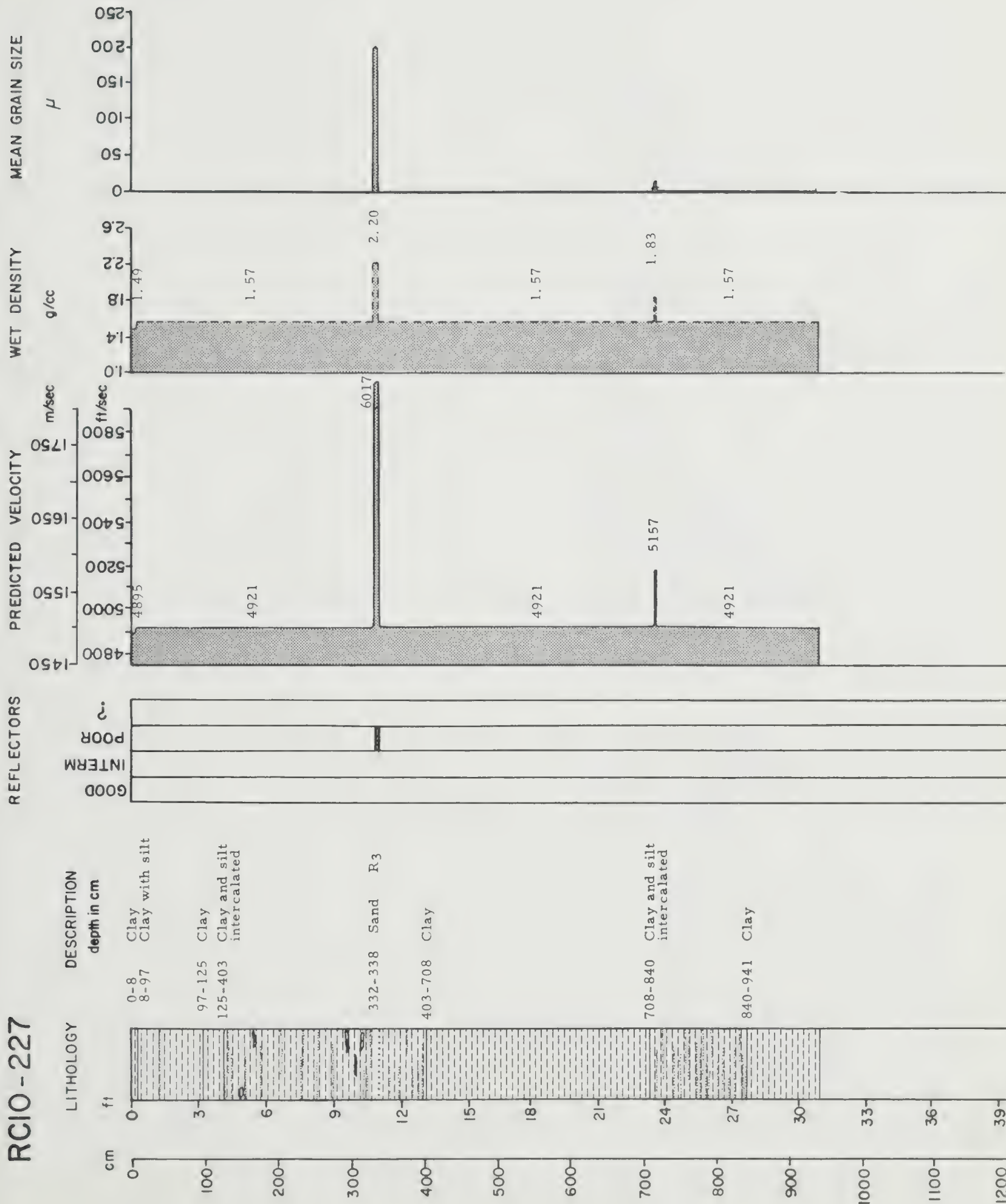


# RC10-226



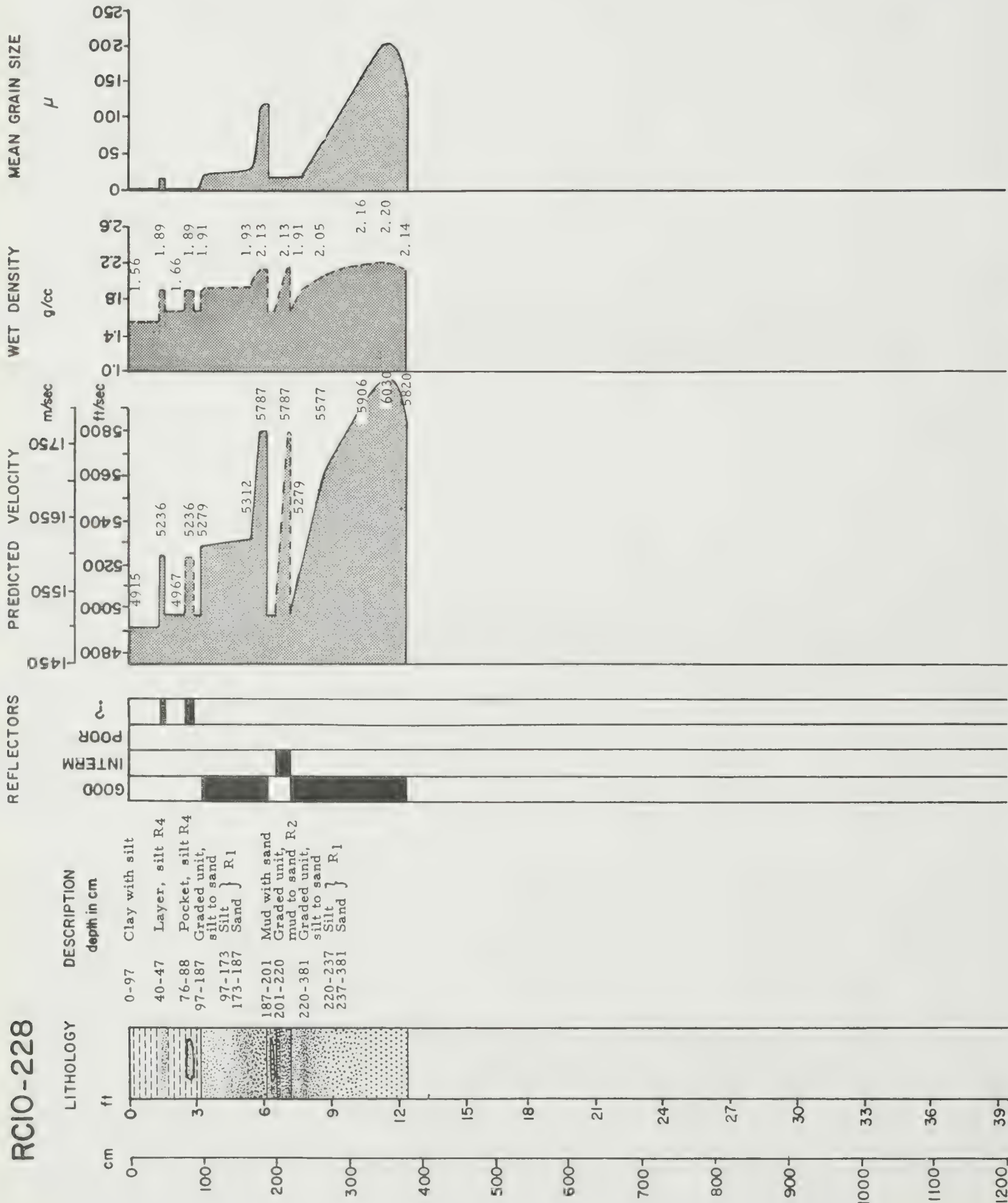
# RCIO - 227

D-55

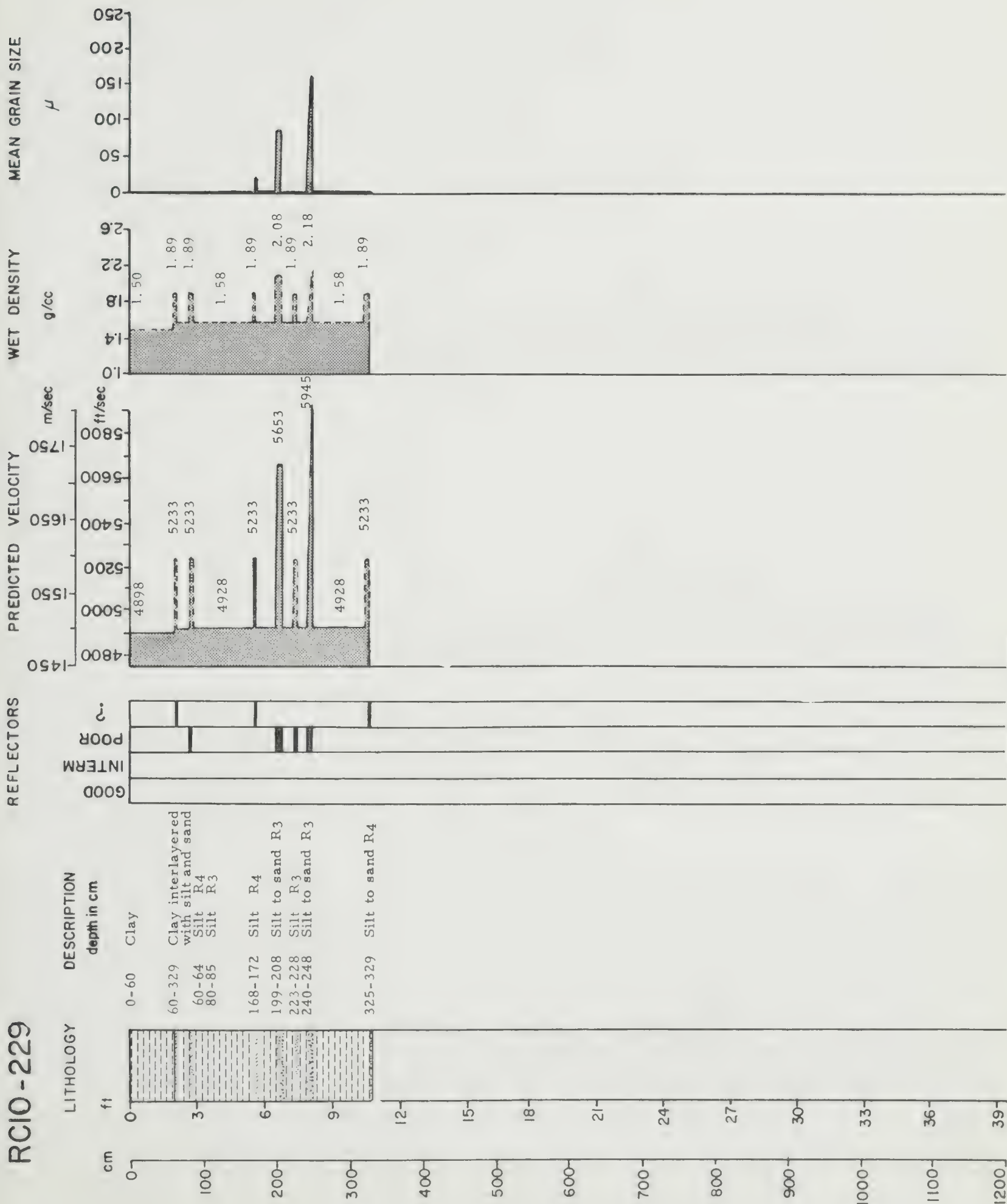




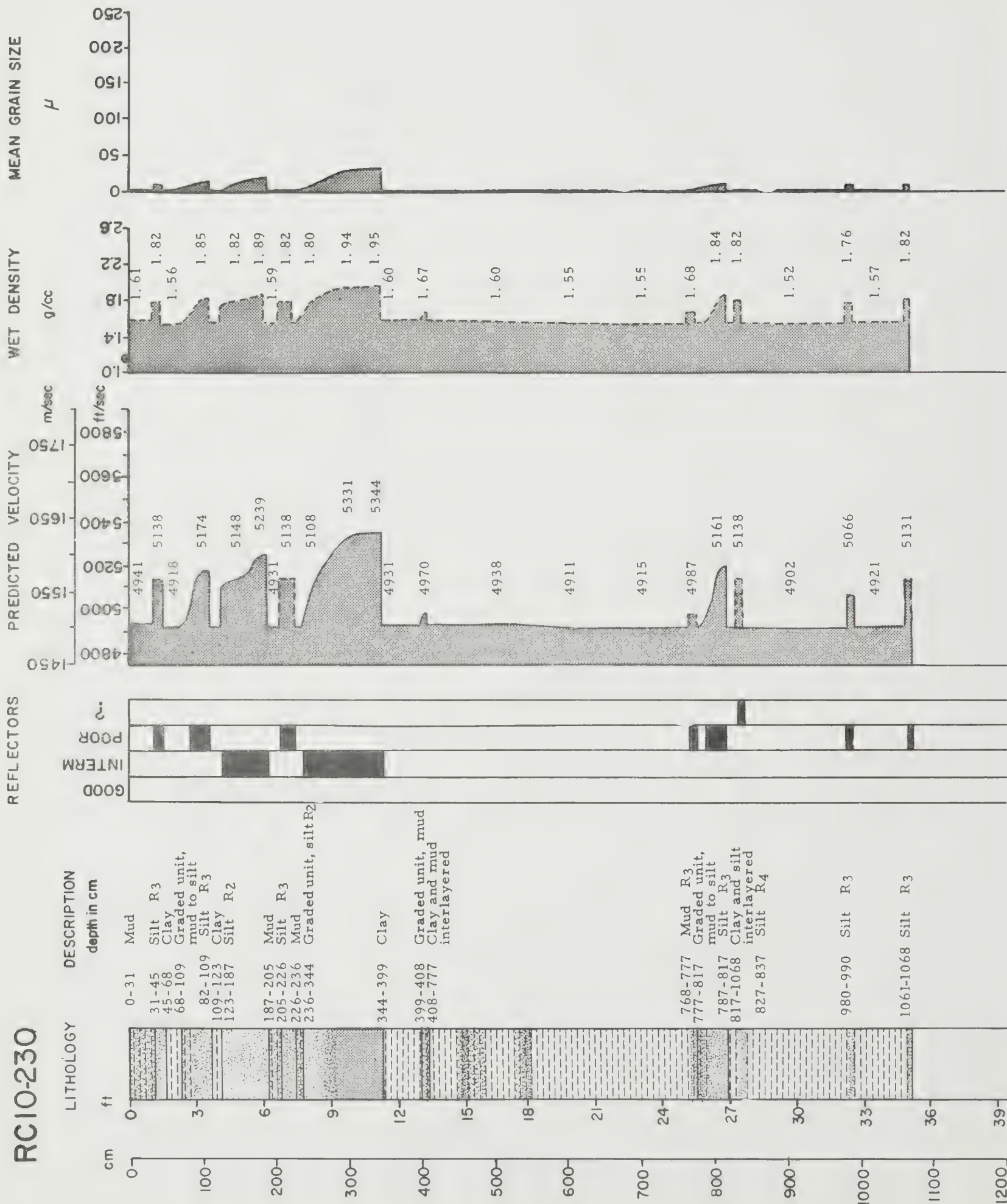
RCIO-228



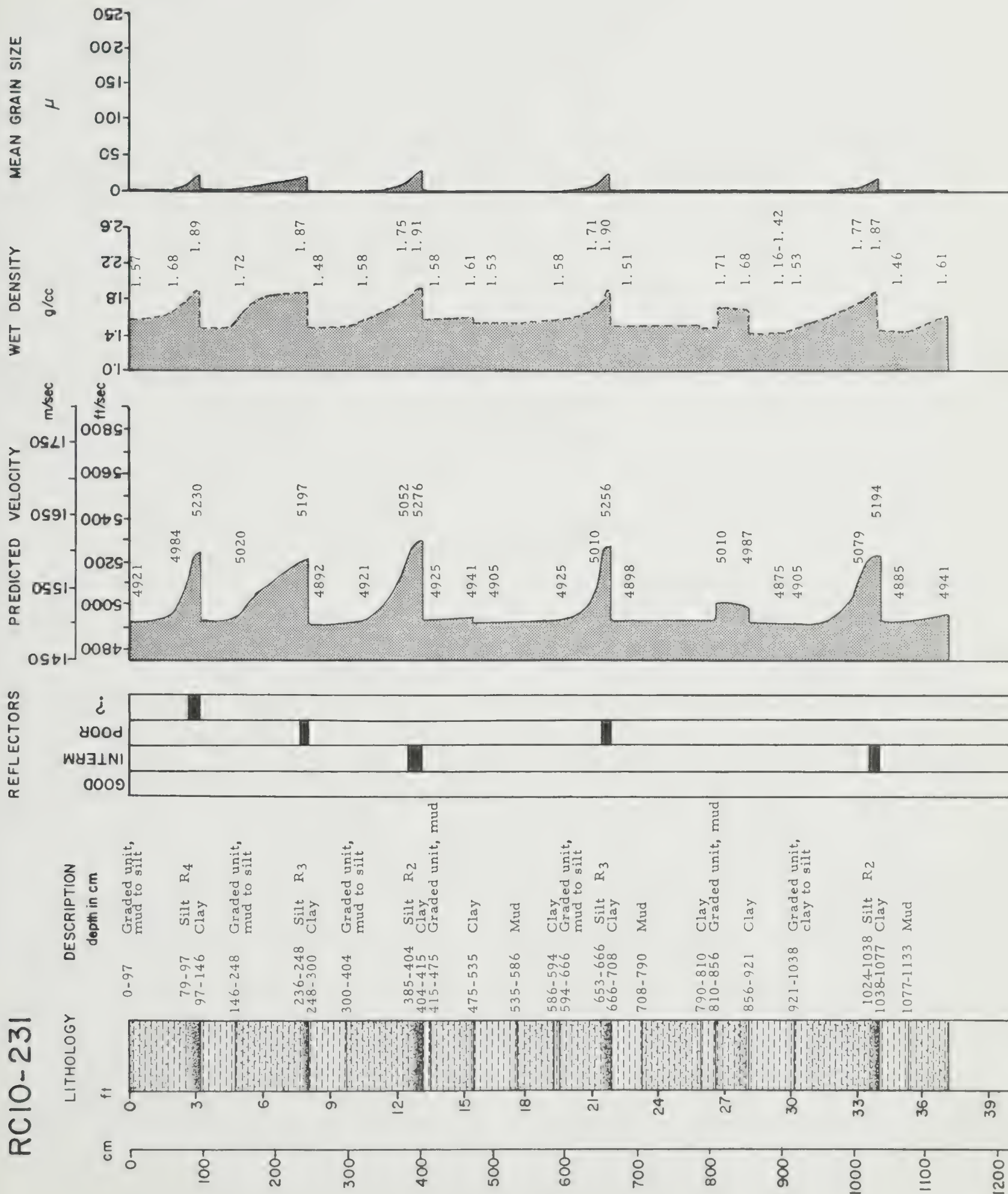




# RC10-230

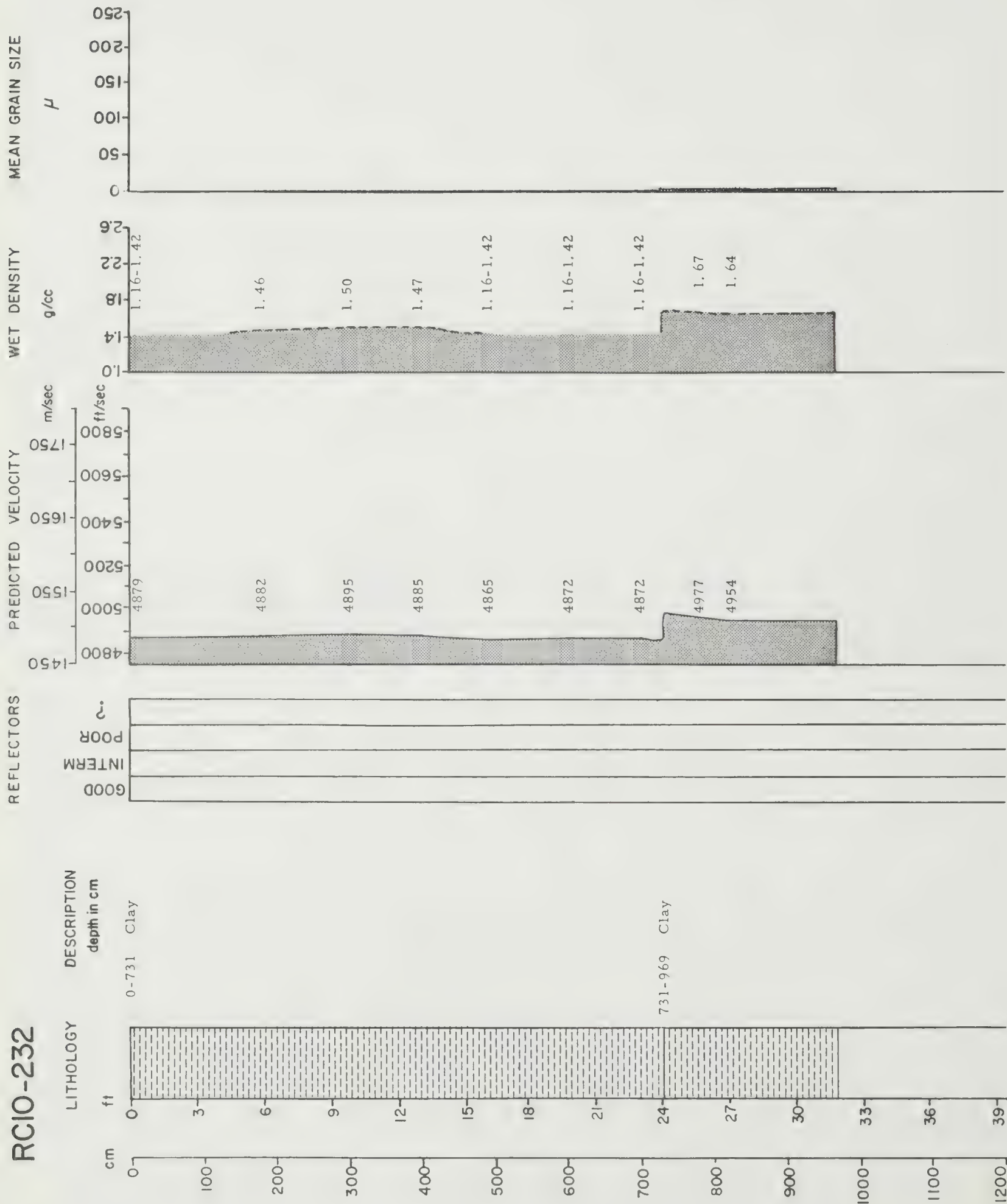


## RC10-231



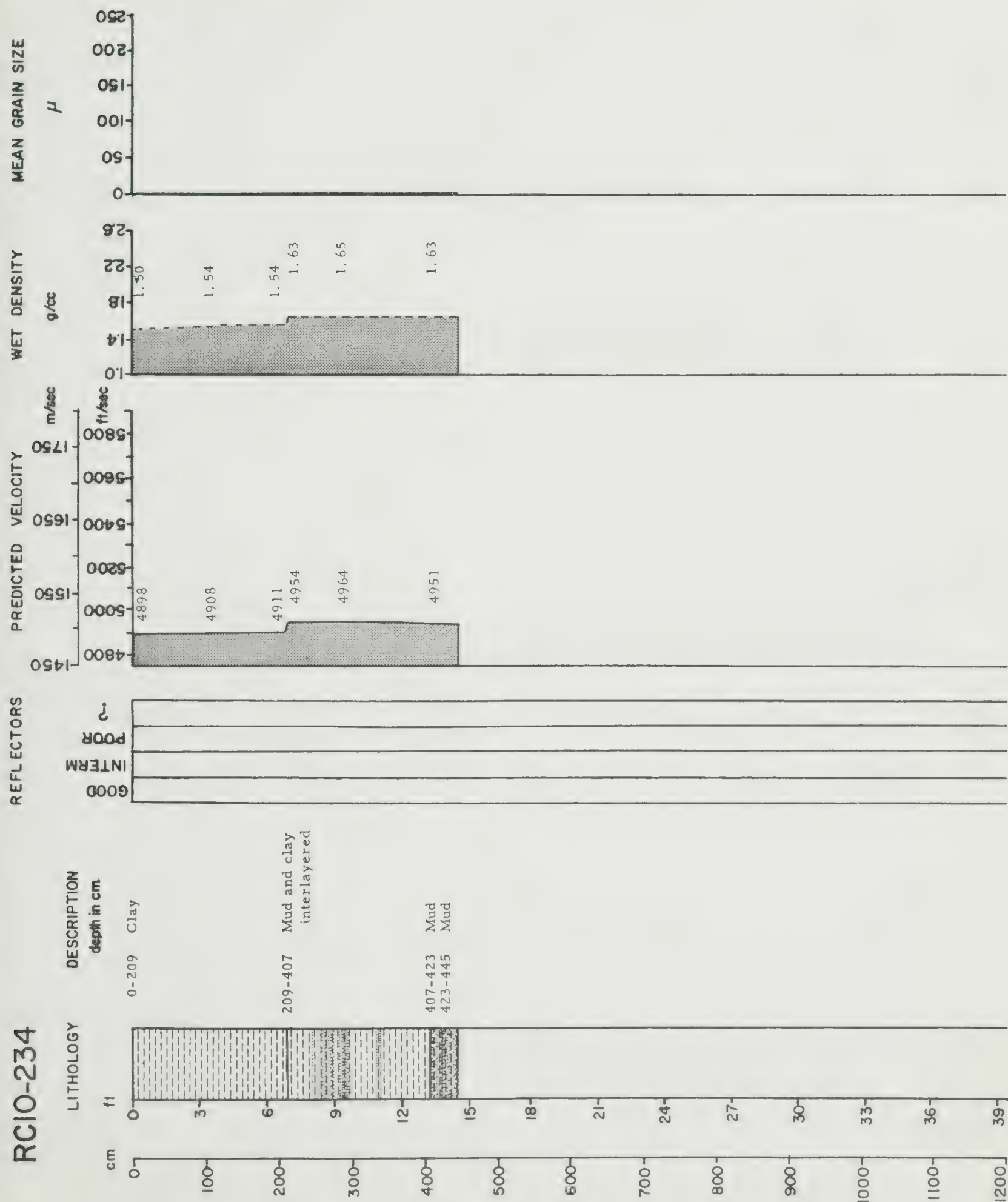


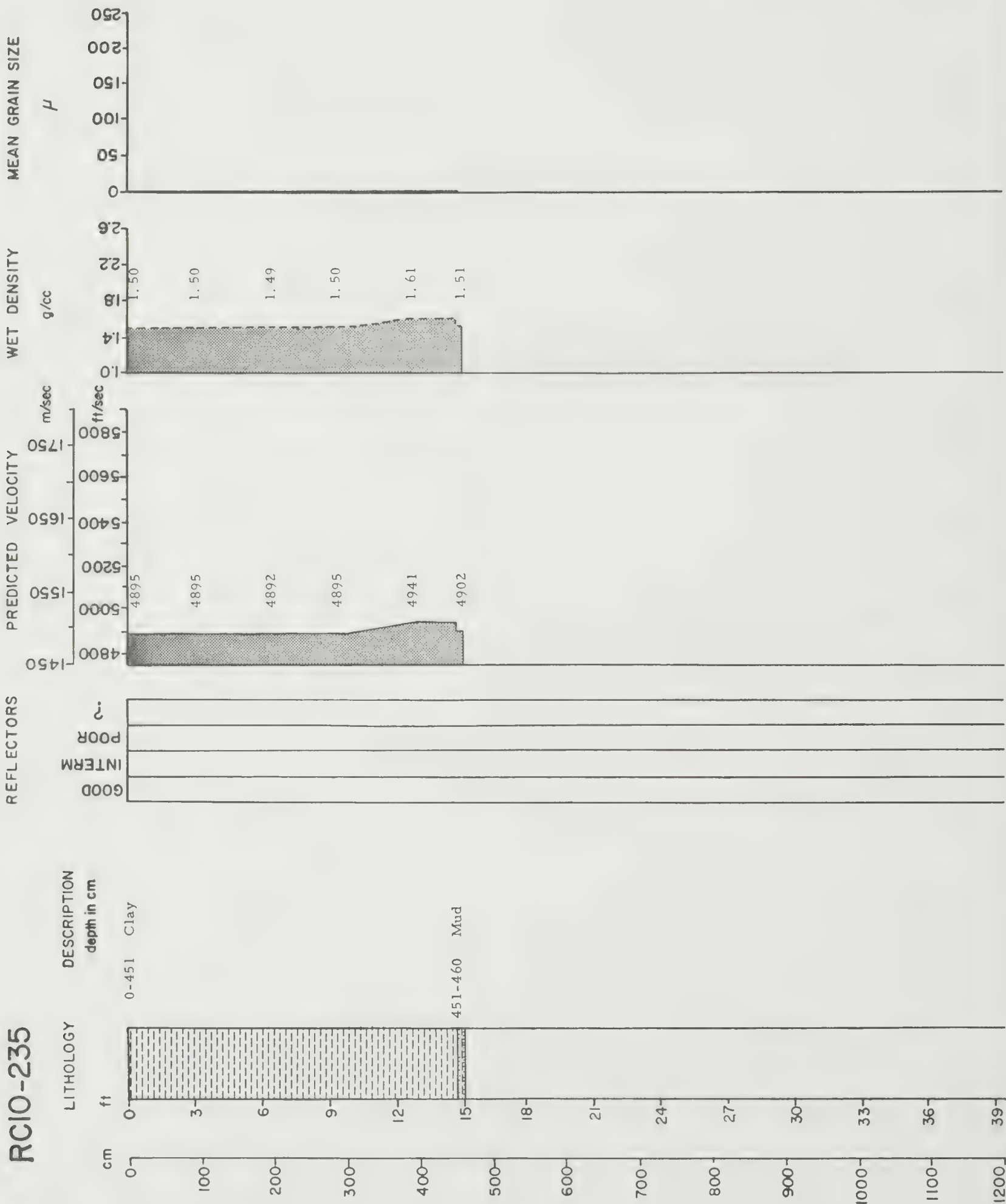
RCIO-232



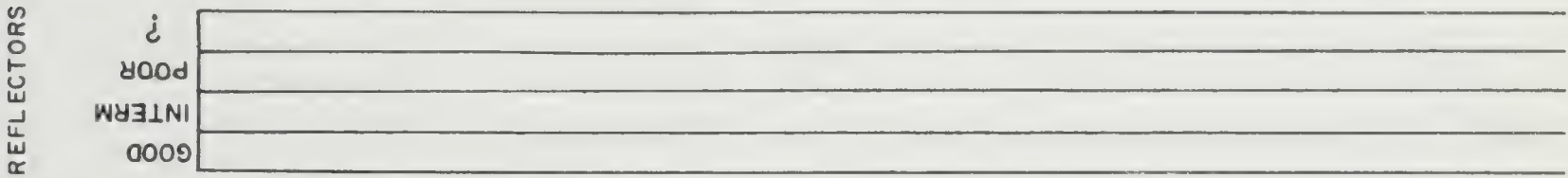
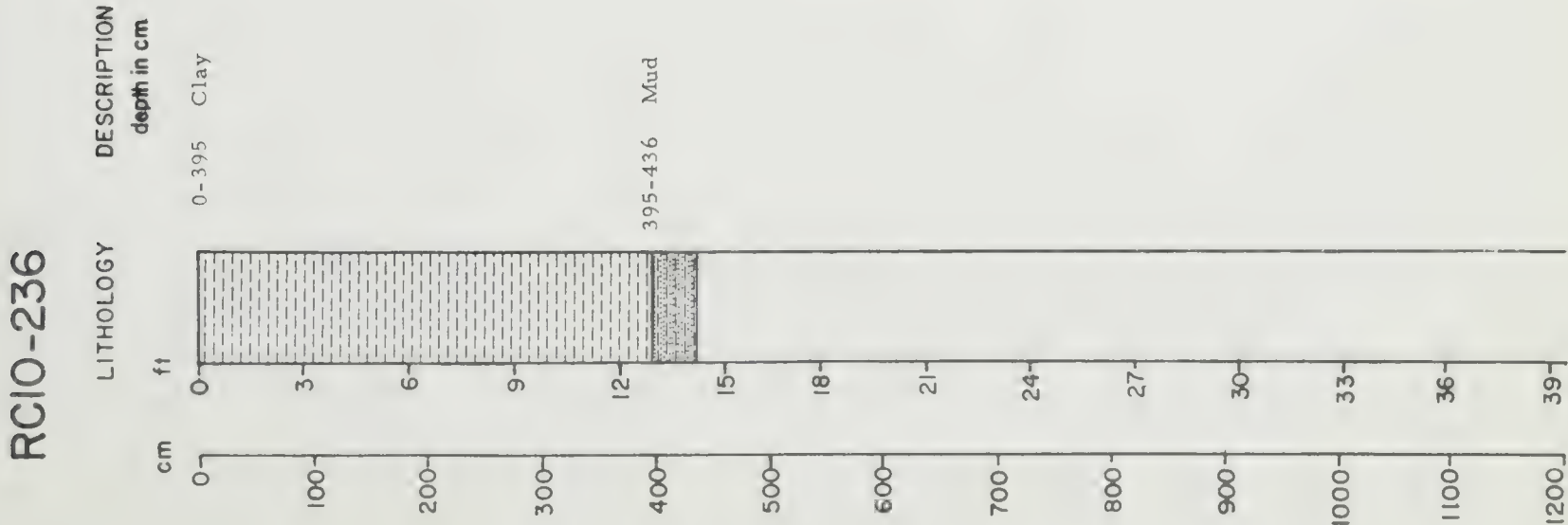


RC10-234

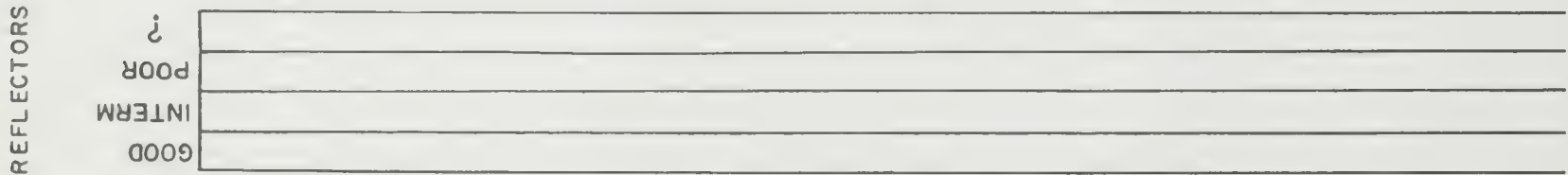
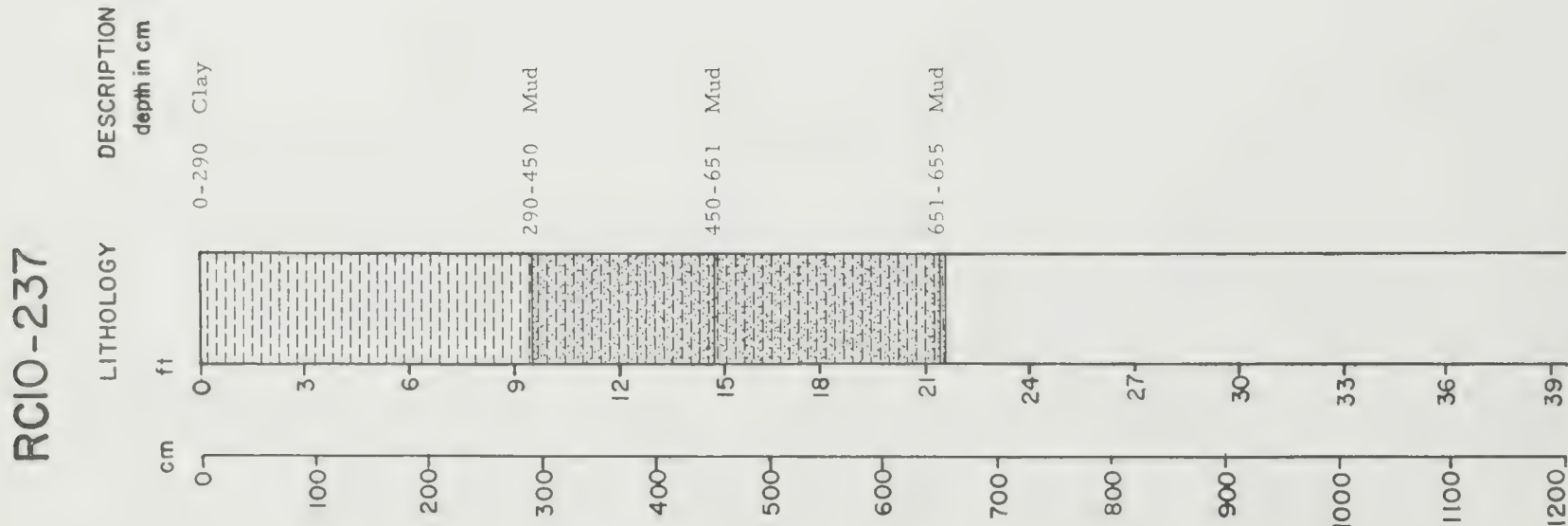




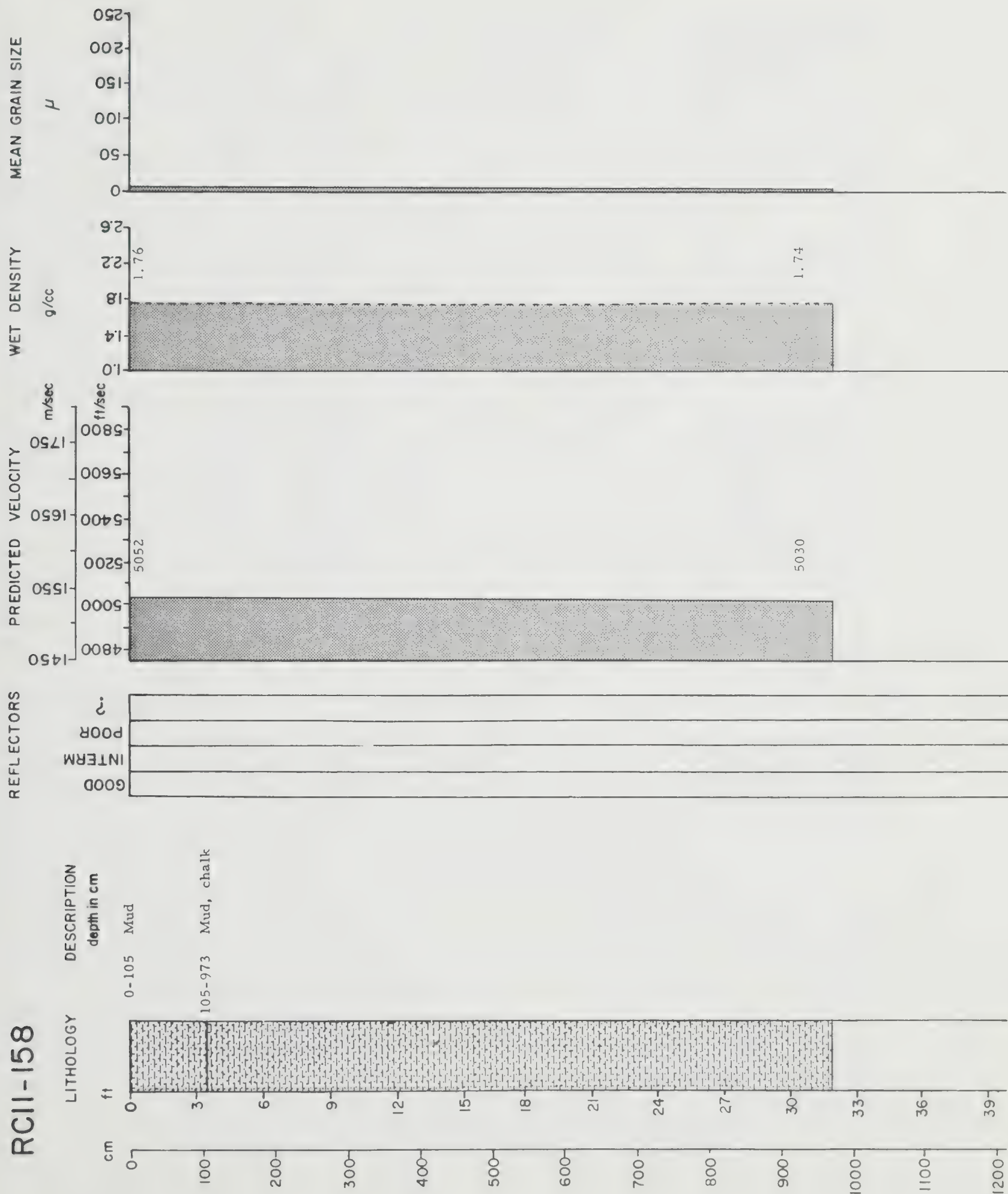
# RCIO-236



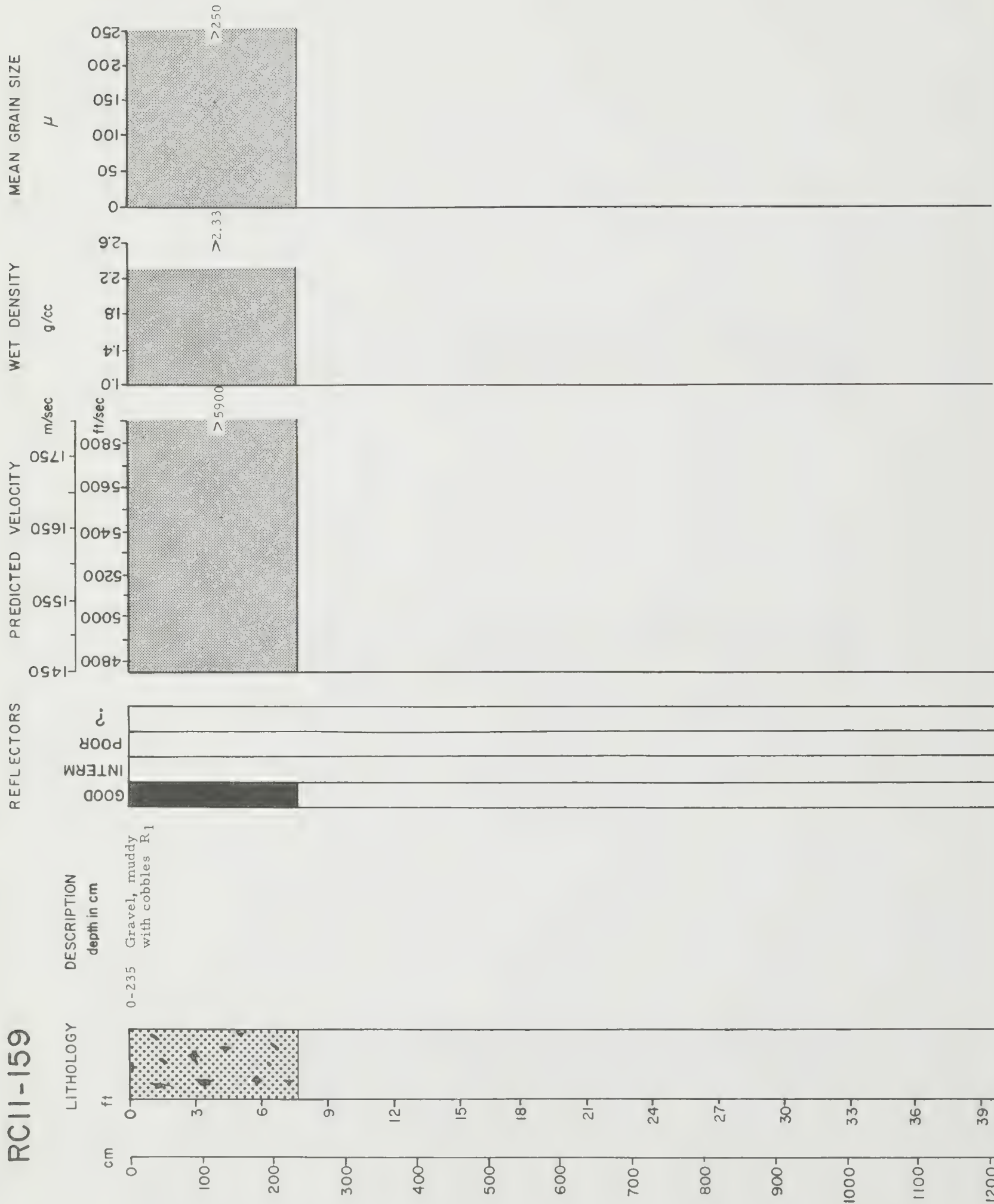
RCIO-237



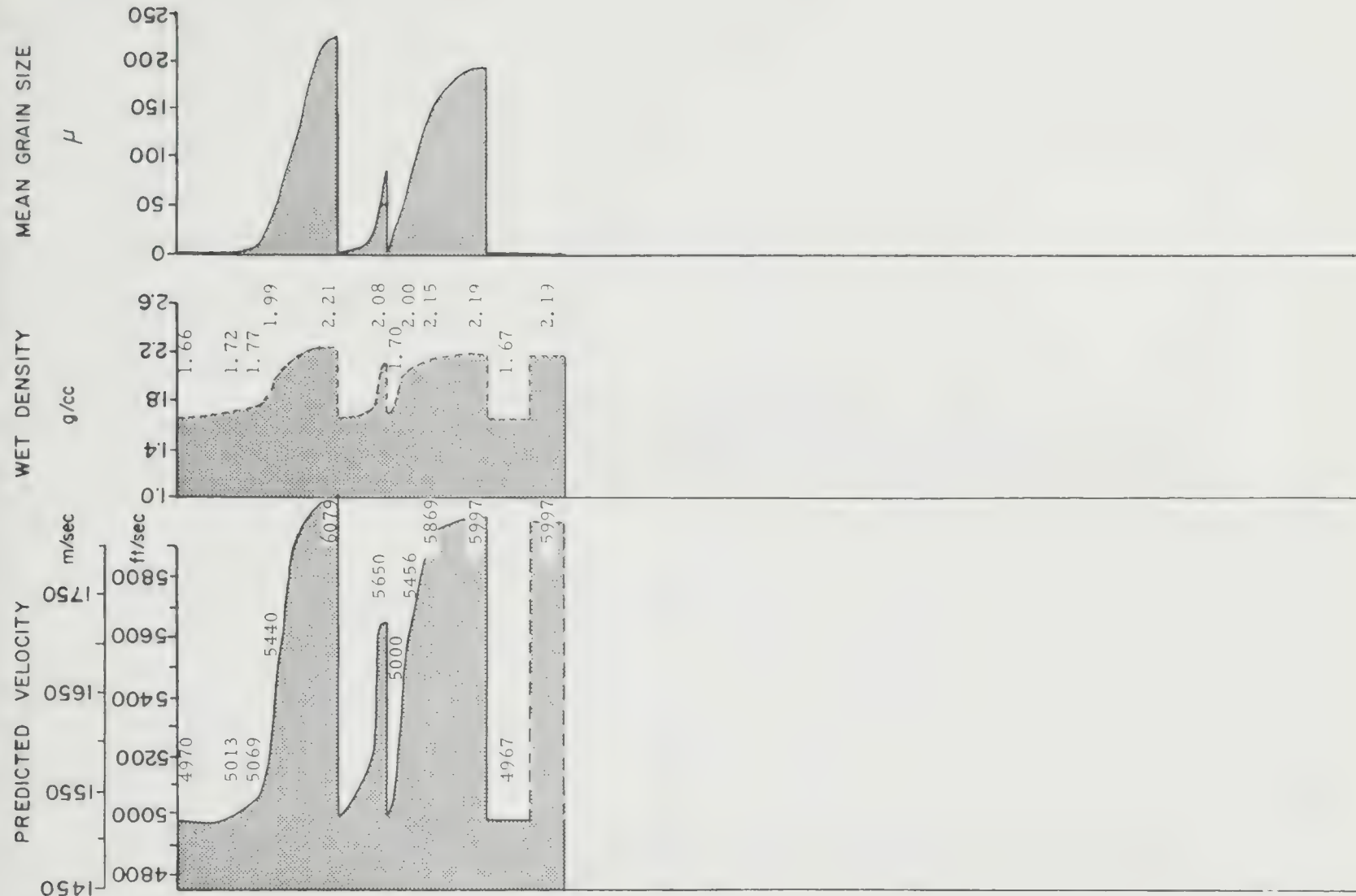
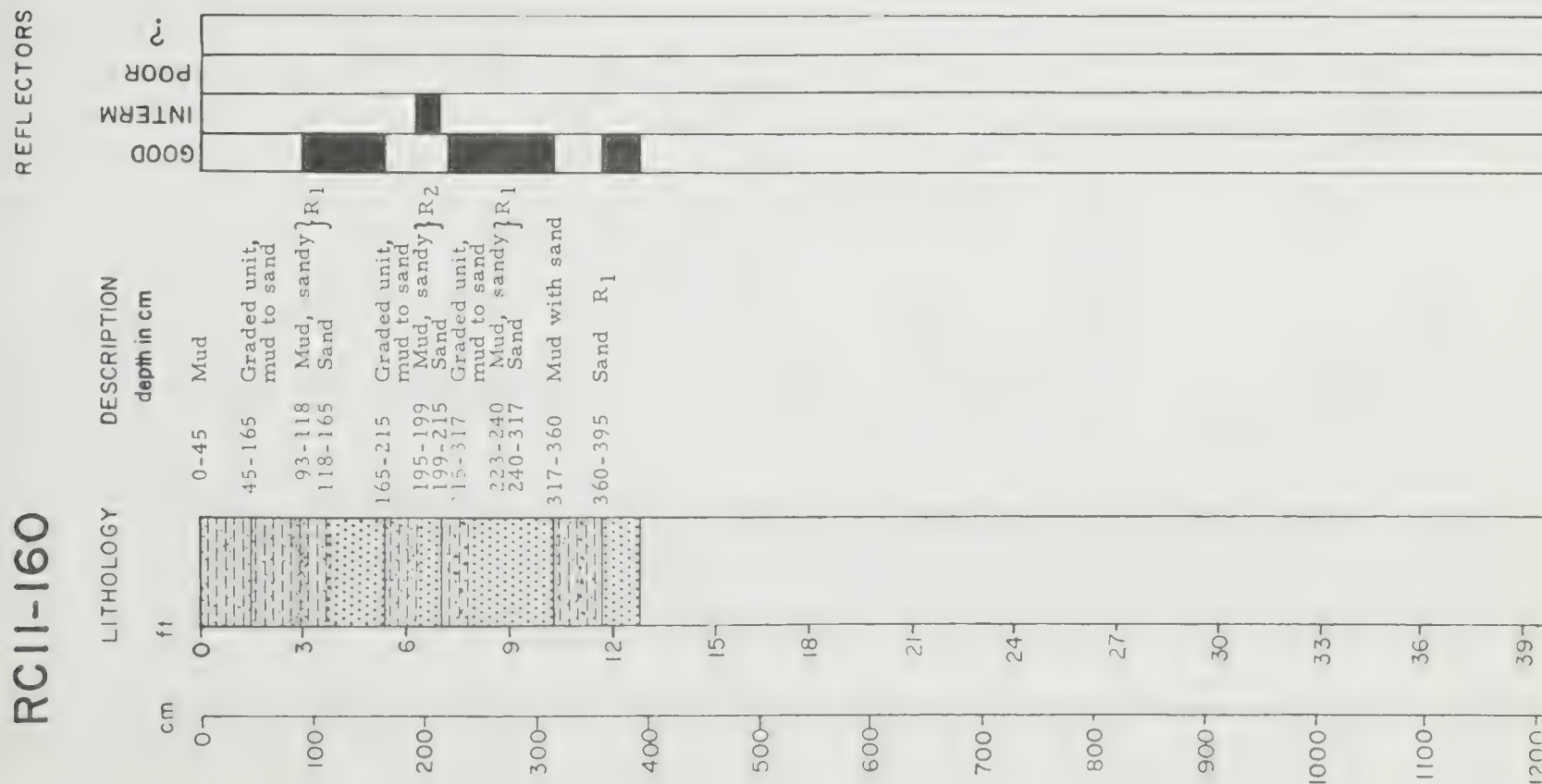




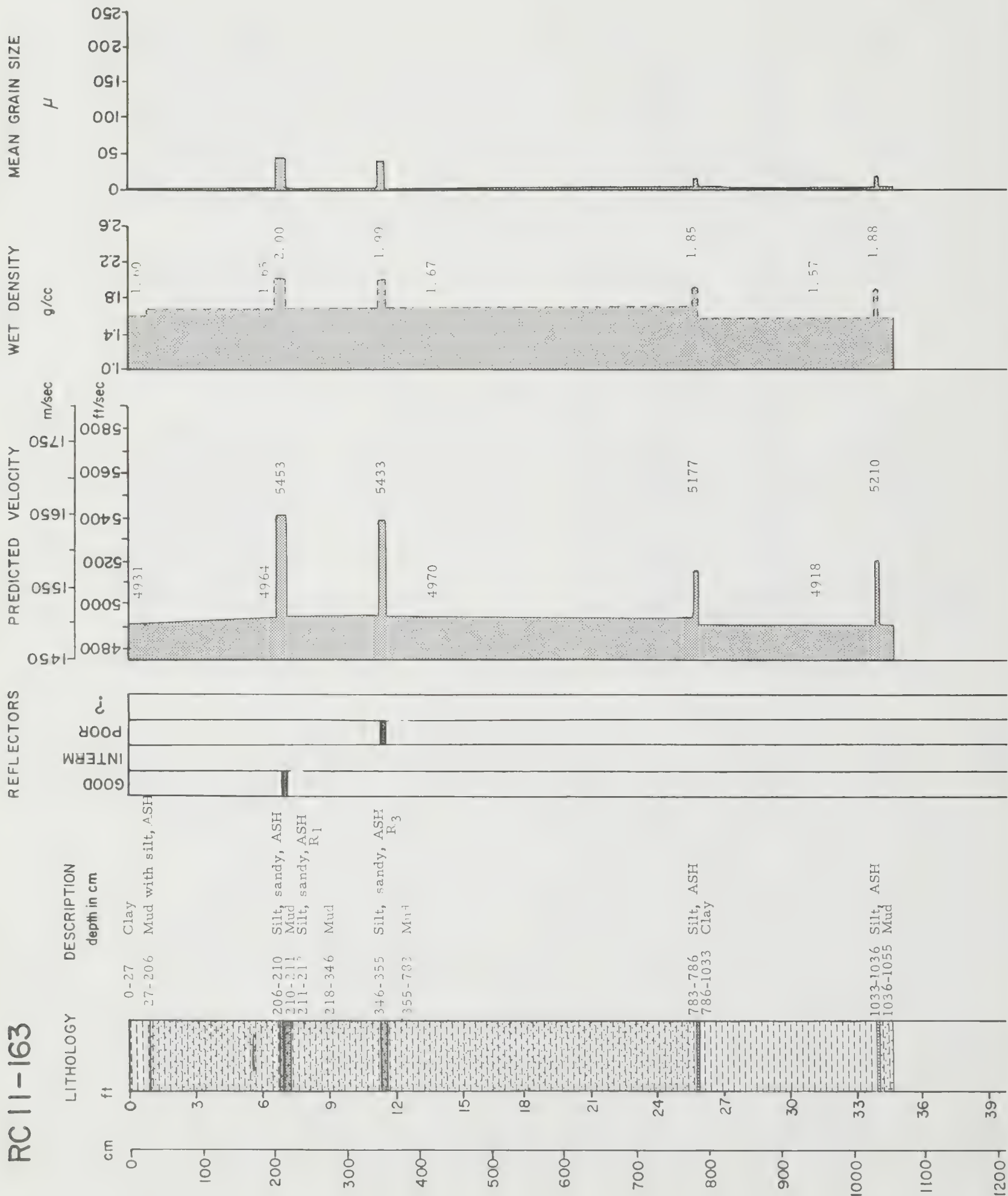
RC11-159



# RC11-160

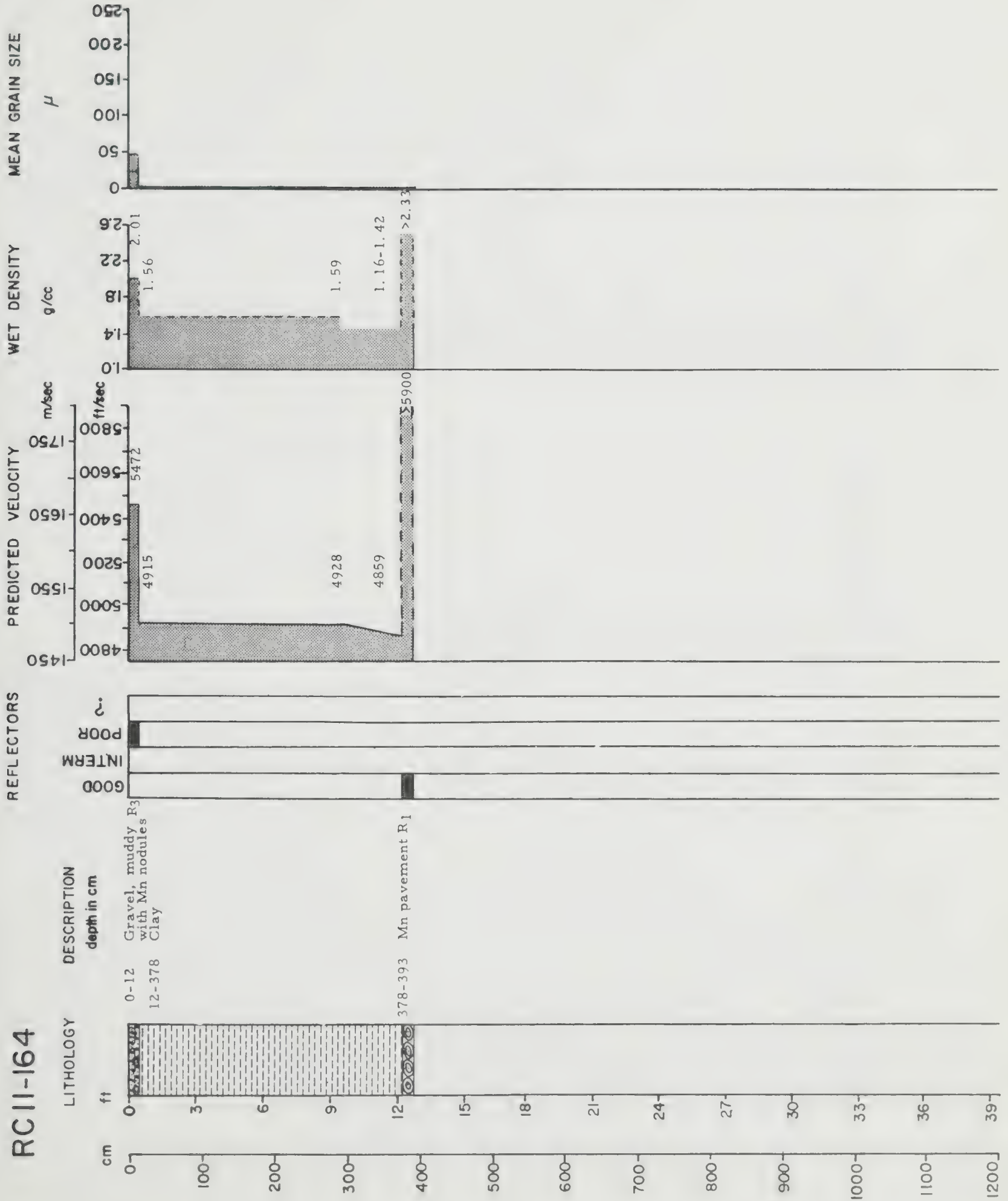


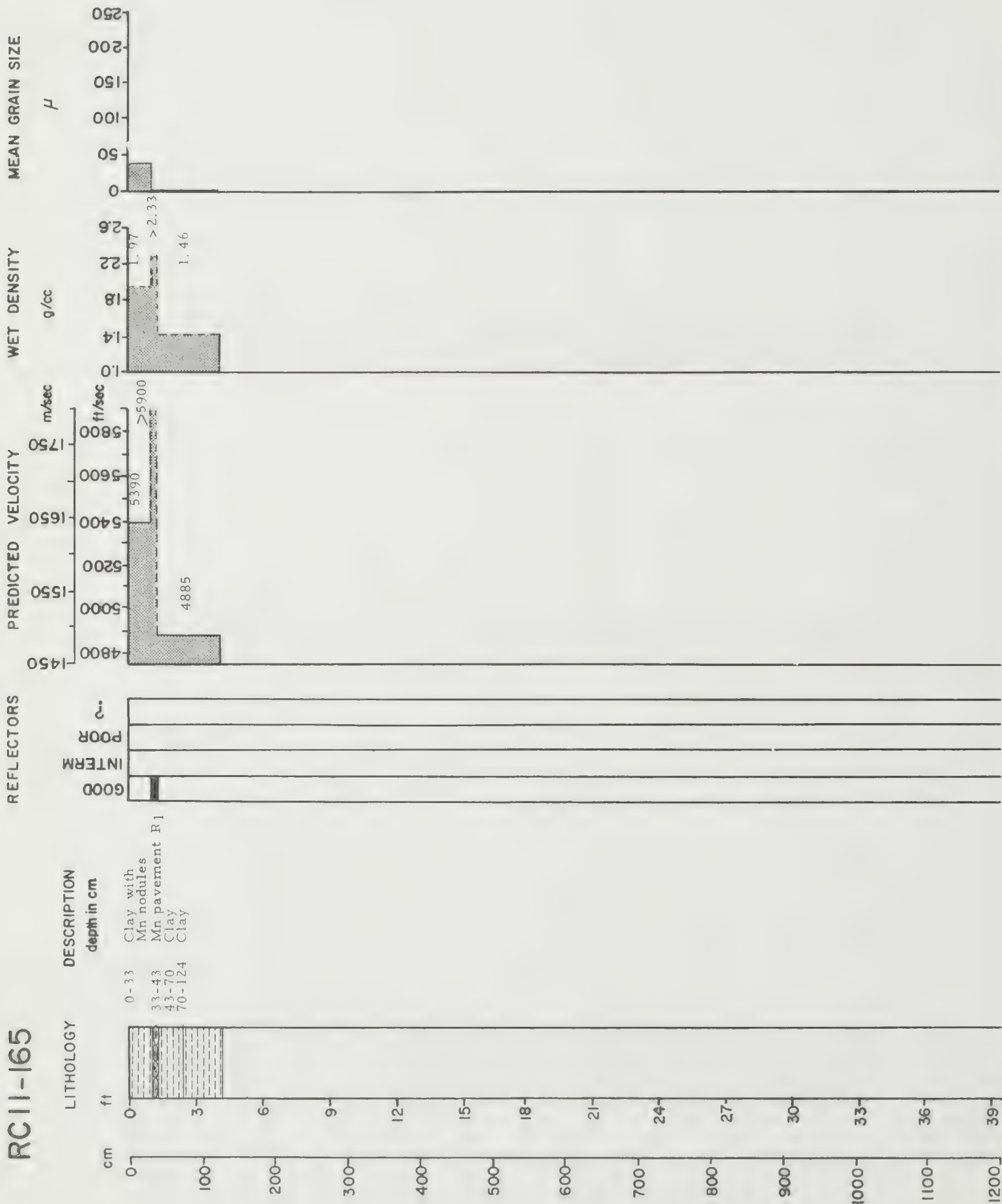
RC 11-163



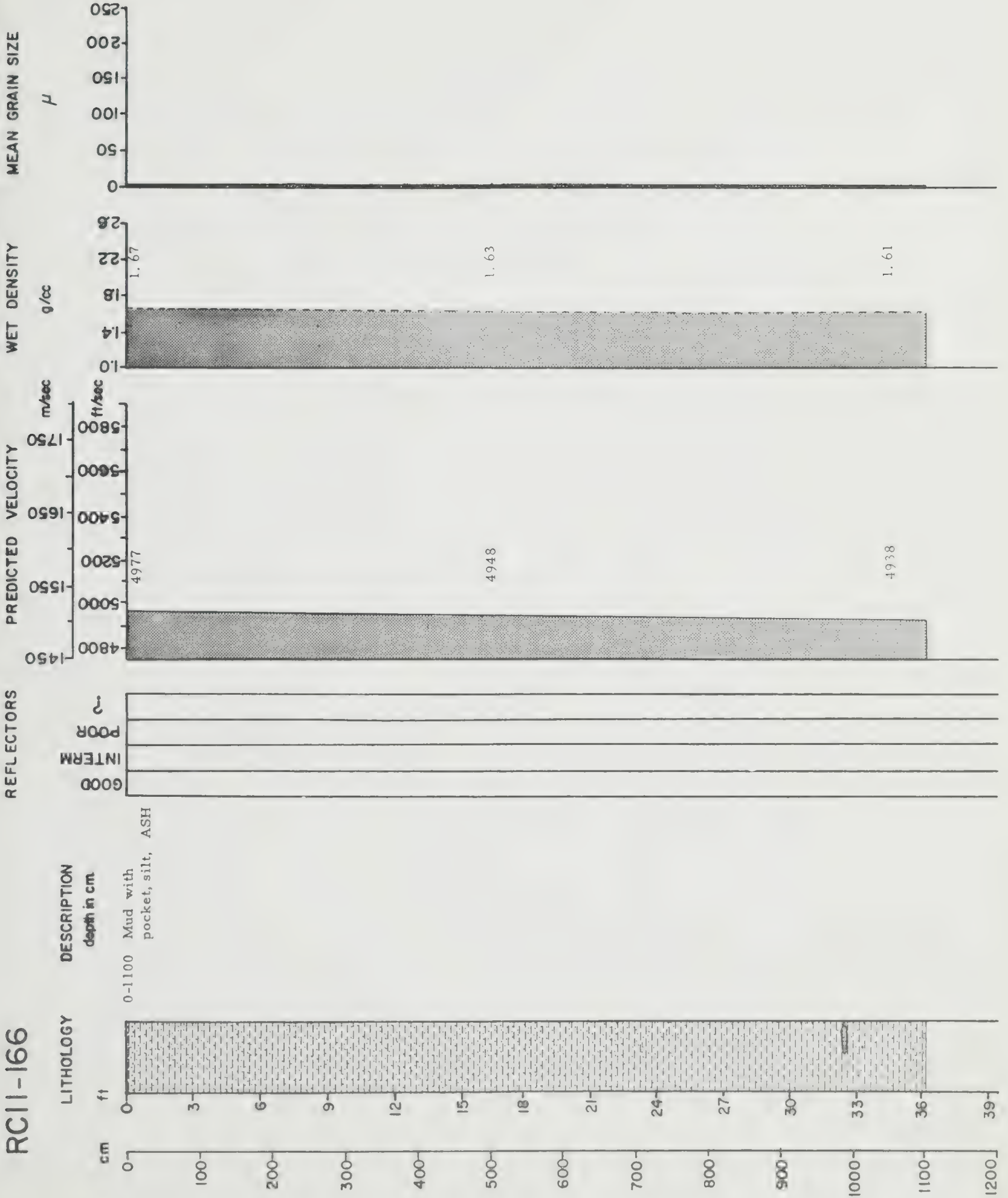


RC11-164

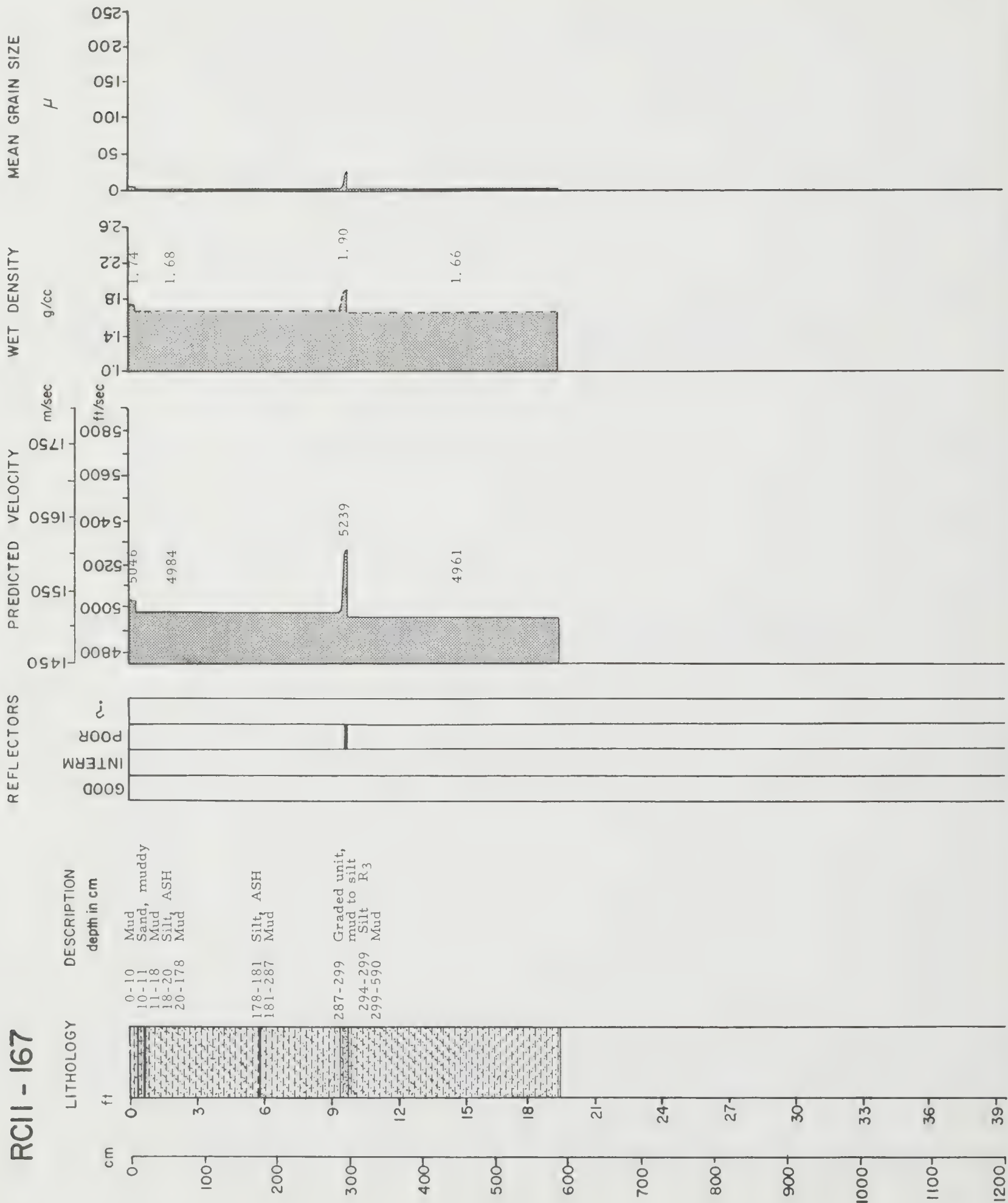




RC11-166



# RCII - 167





RC 11-168

REFLECTORS

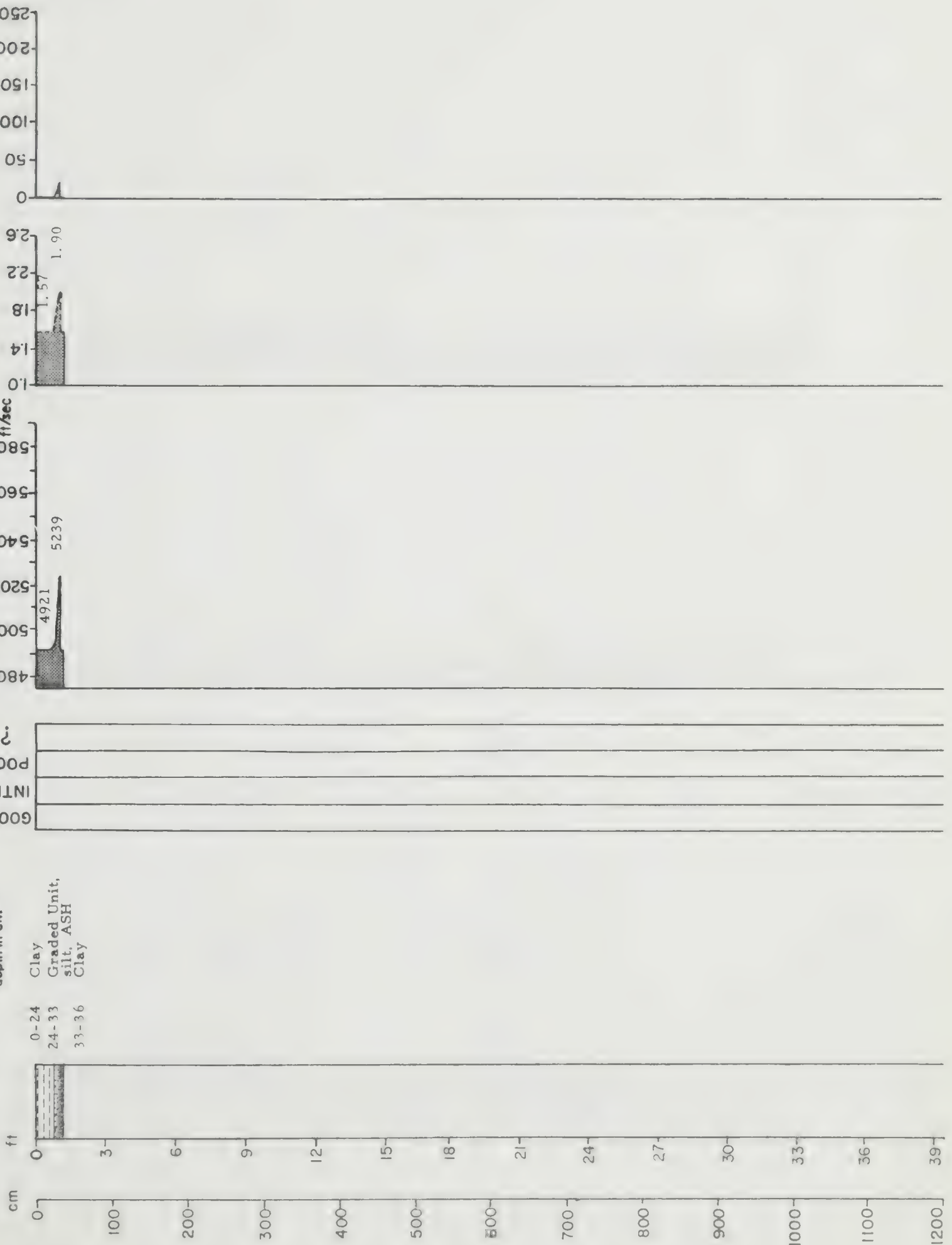
PREDICTED VELOCITY

WET DENSITY

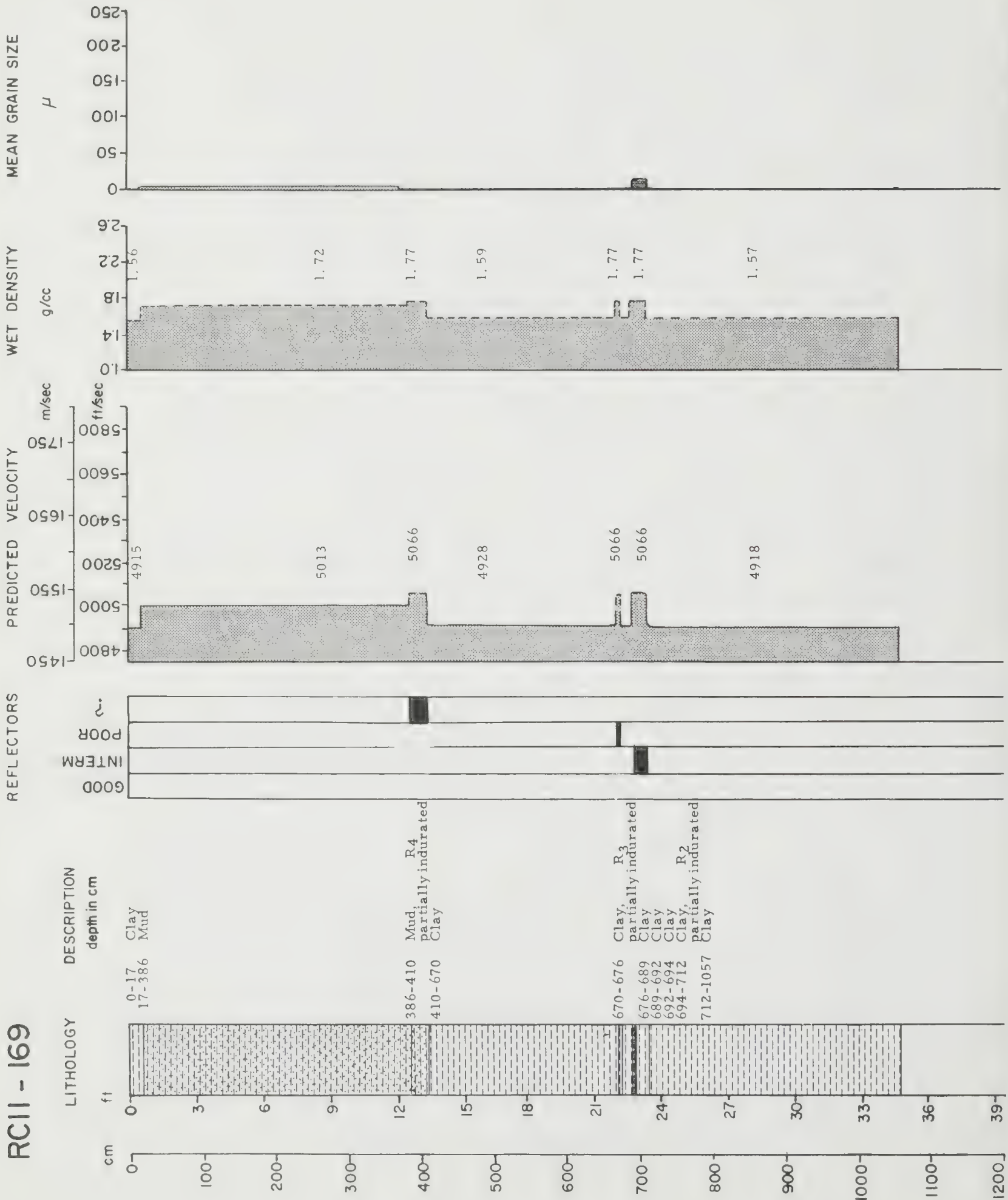
MEAN GRAIN SIZE

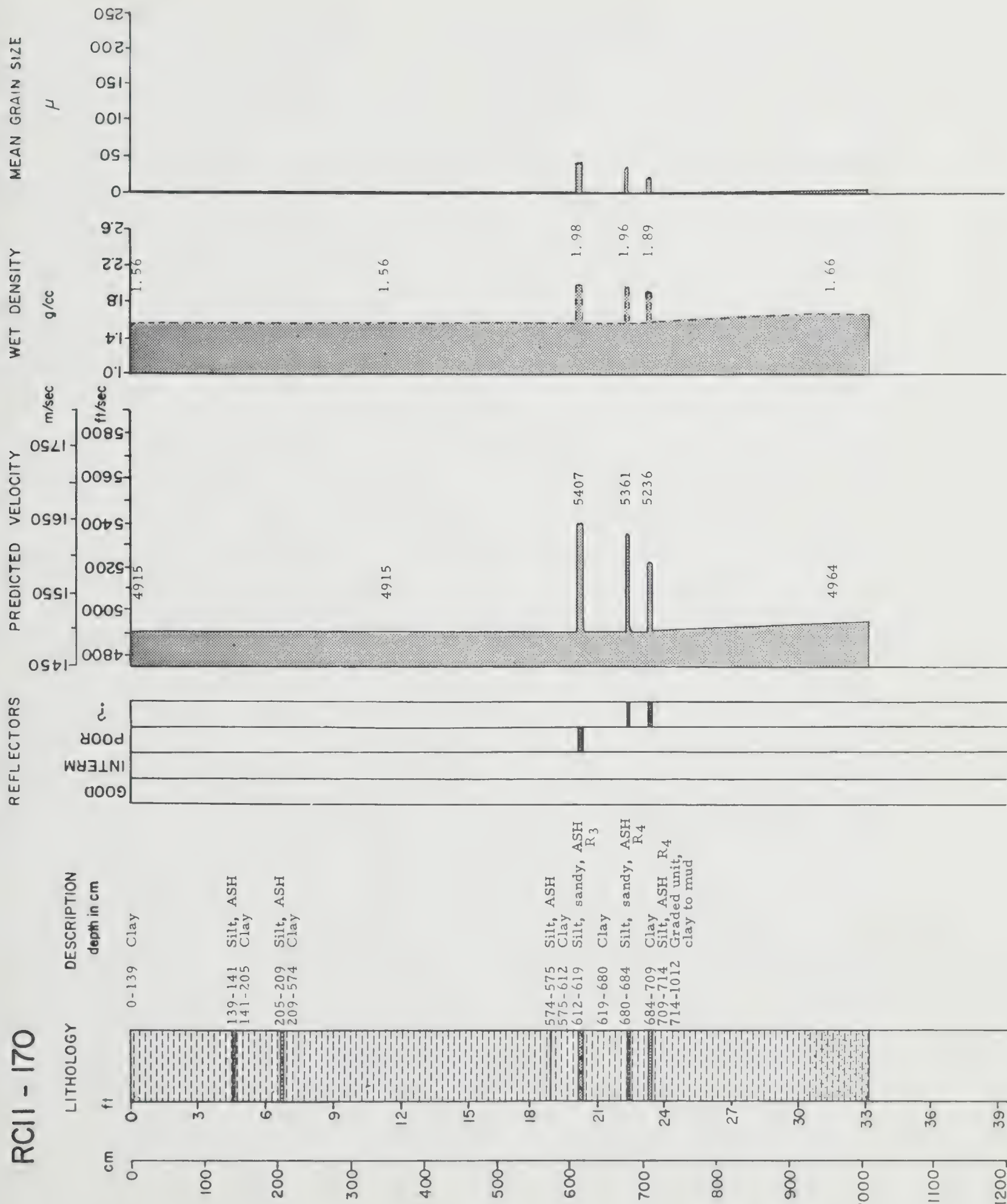
DESCRIPTION  
depth in cm

LITHOLOGY

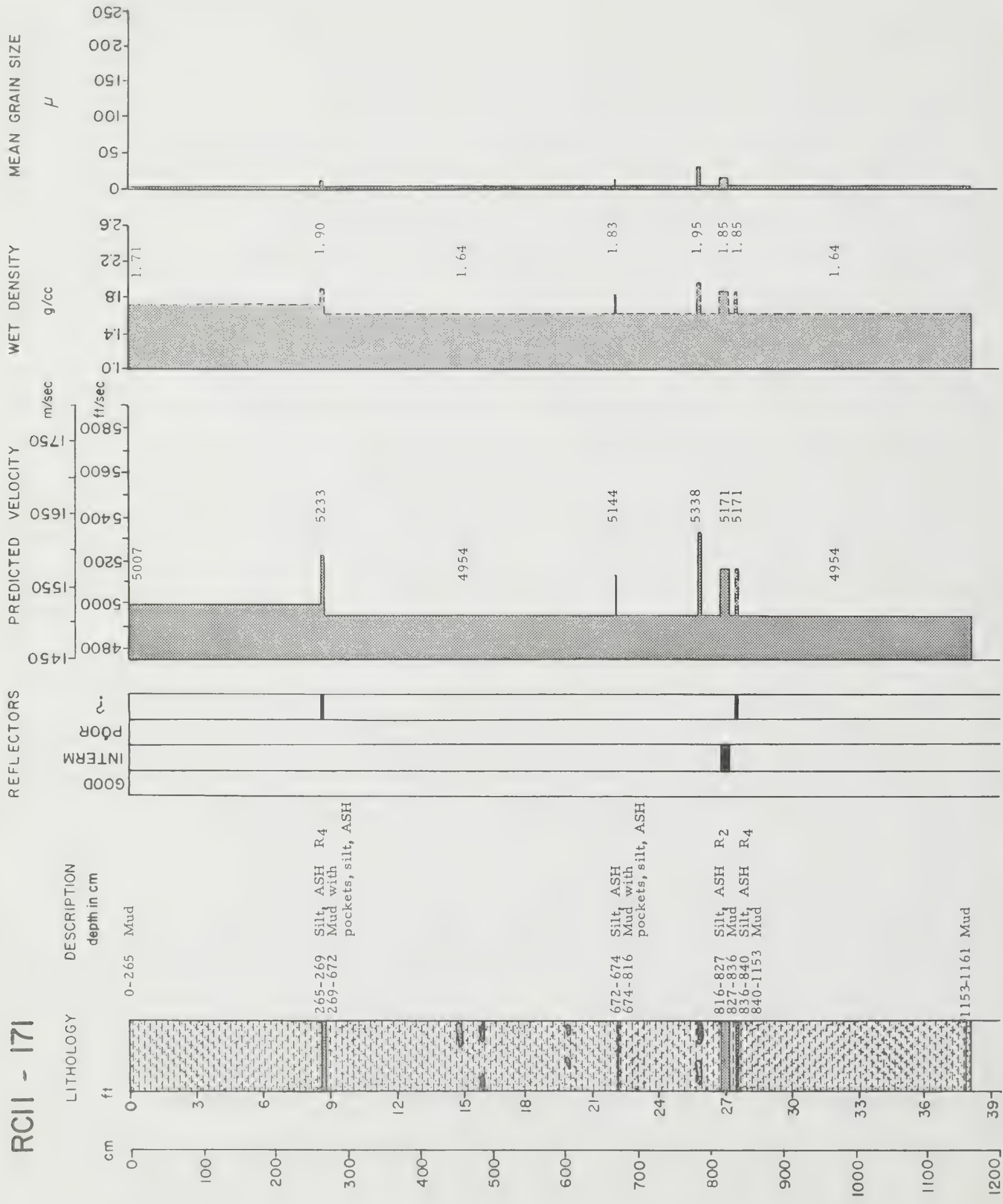


RCII - 169

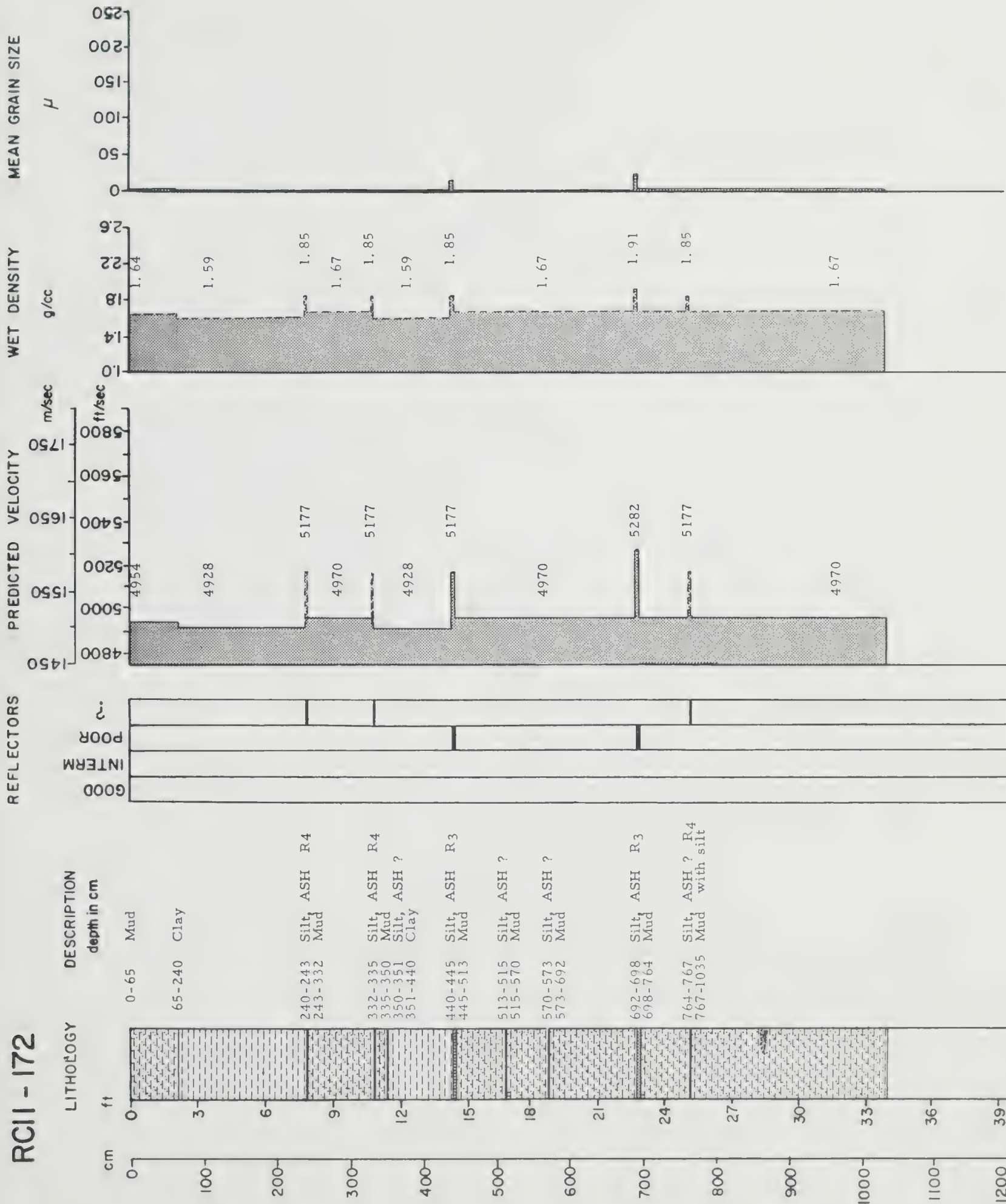




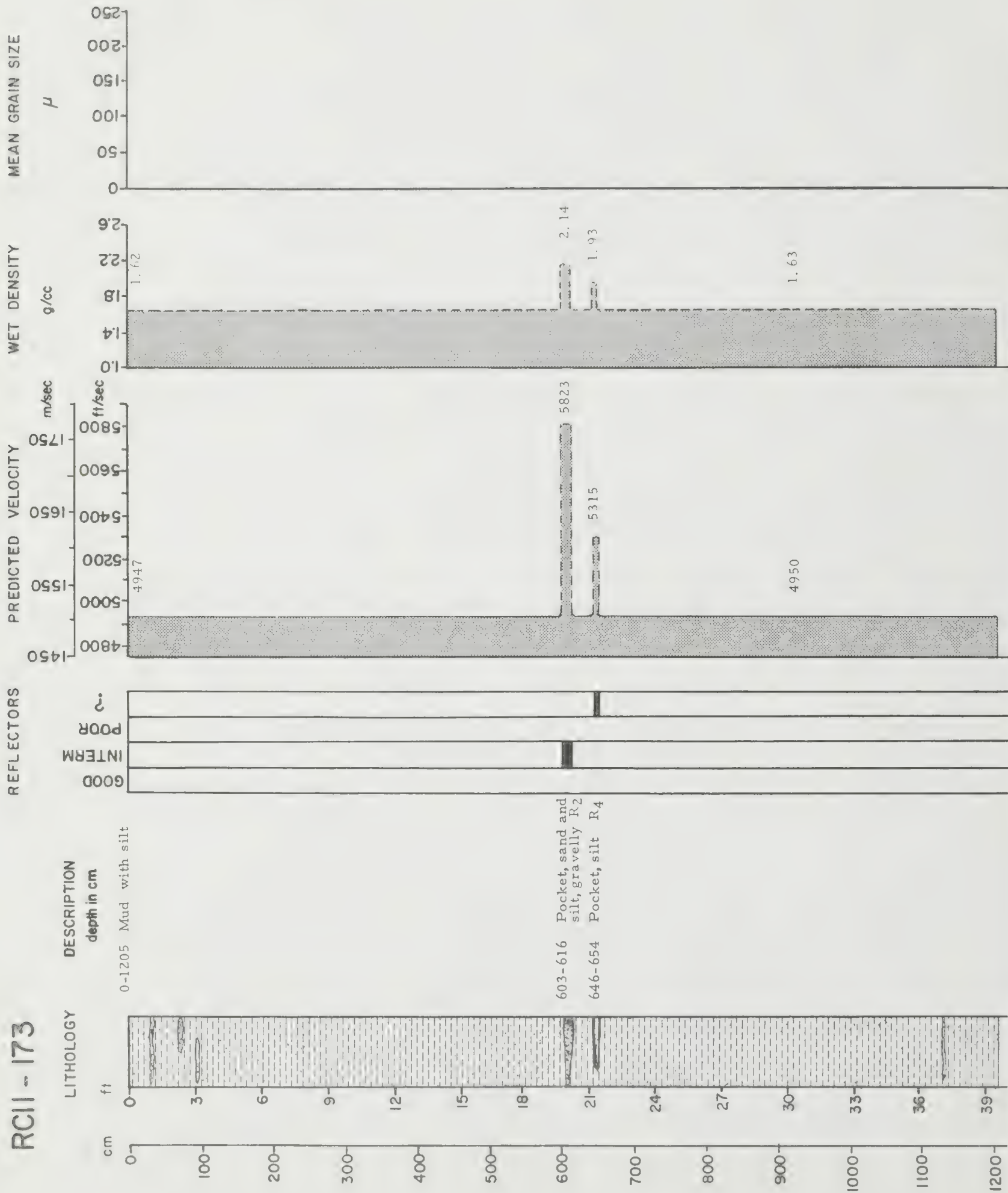
RCII - 171







RCII - 173



RC11 - 174

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

DESCRIPTION

LITHOLOGY

depth in cm

cm

ft

0-356 Gravel, muddy sandy R1

GOOD  
INTERM  
POOR  
?

1450  
1500  
1550  
1600  
1650  
1700  
1750  
m/sec  
ft/sec

1.0  
1.4  
1.8  
2.2  
2.6  
g/cc

$\mu$

0  
50  
100  
150  
200  
250

0  
100  
200  
300  
400  
500  
600  
700  
800  
900  
1000  
1100  
1200

0  
3  
6  
9  
12  
15  
18  
21  
24  
27  
30  
33  
36  
39

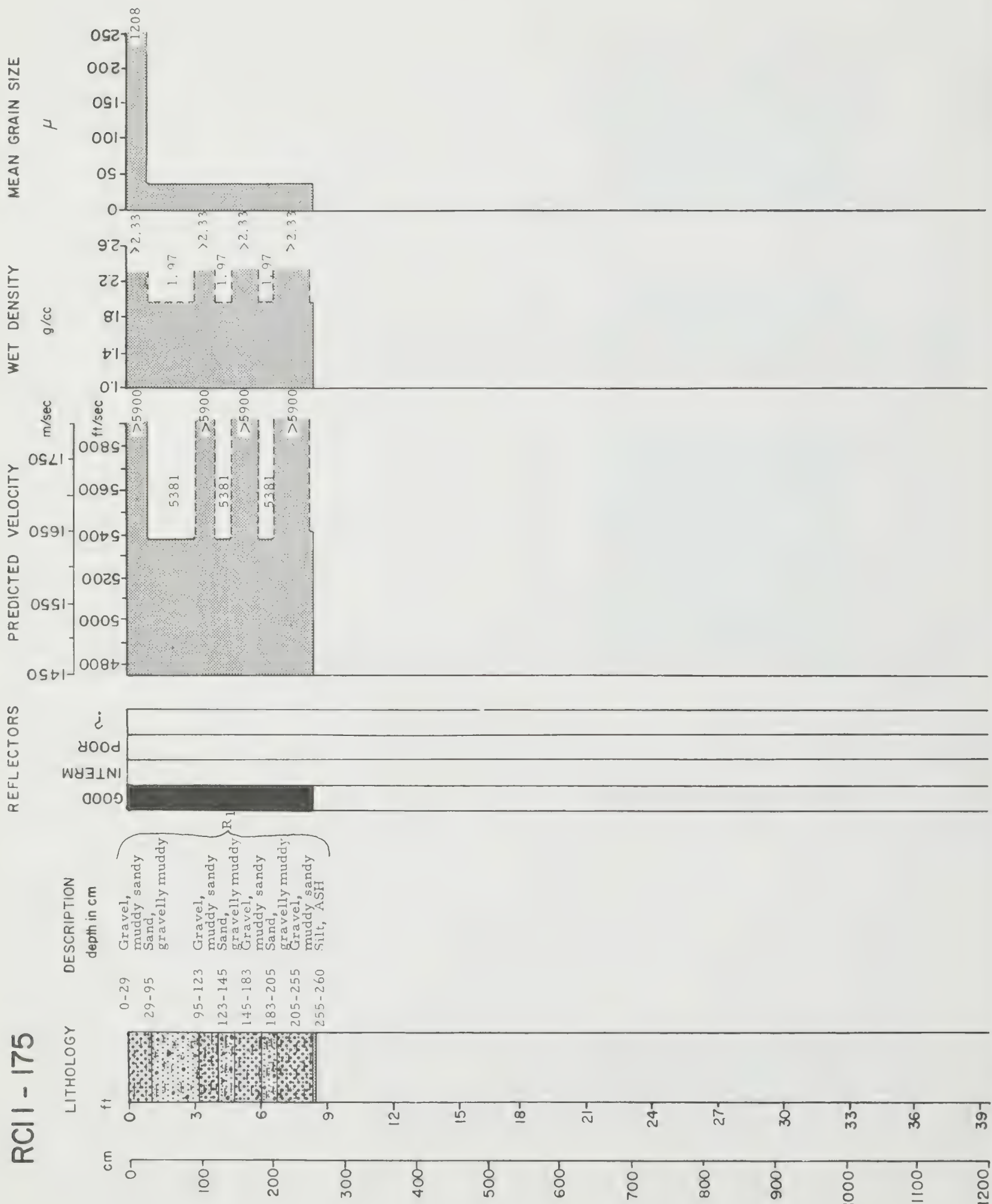
2214

> 2.33

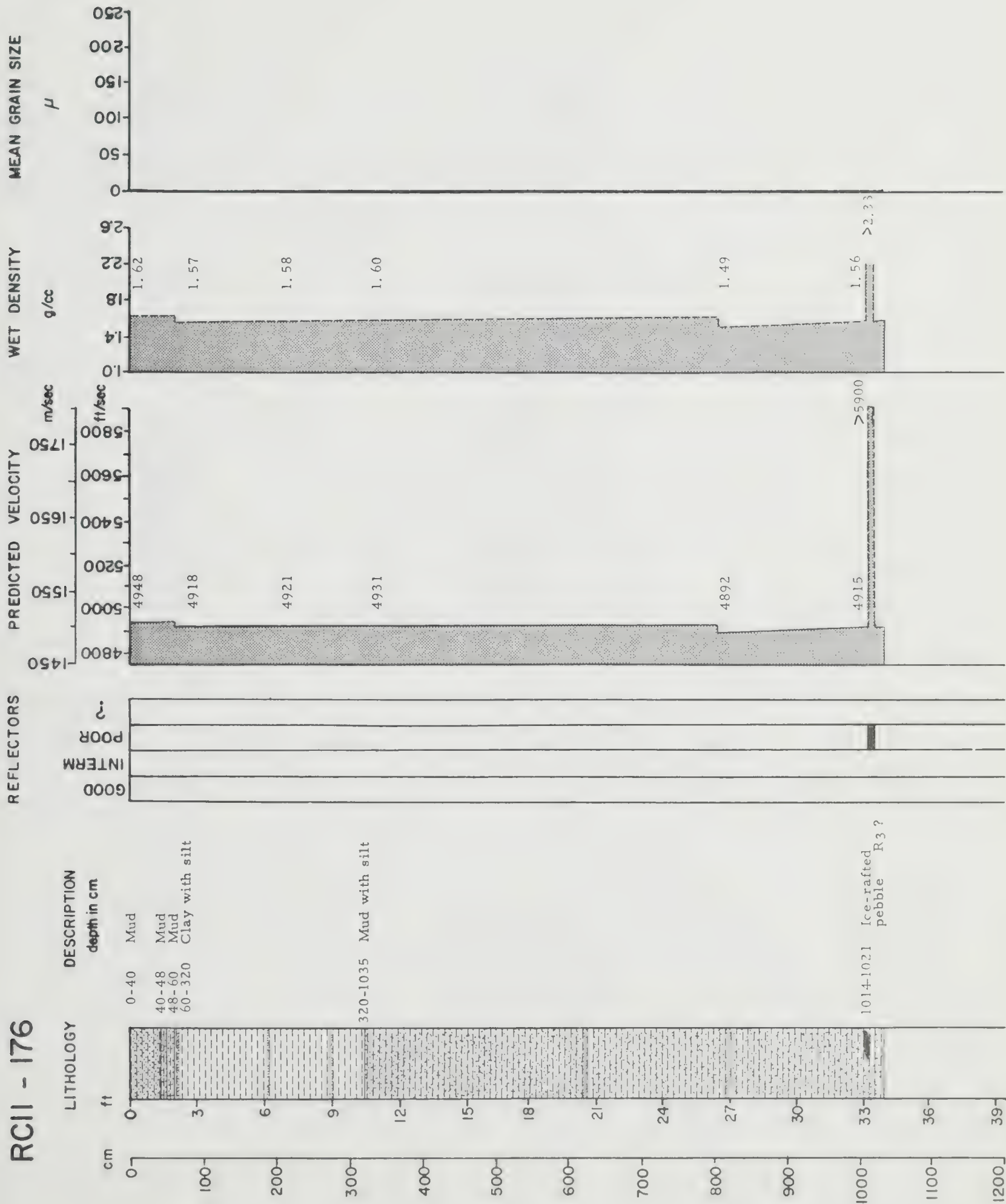
> 5900



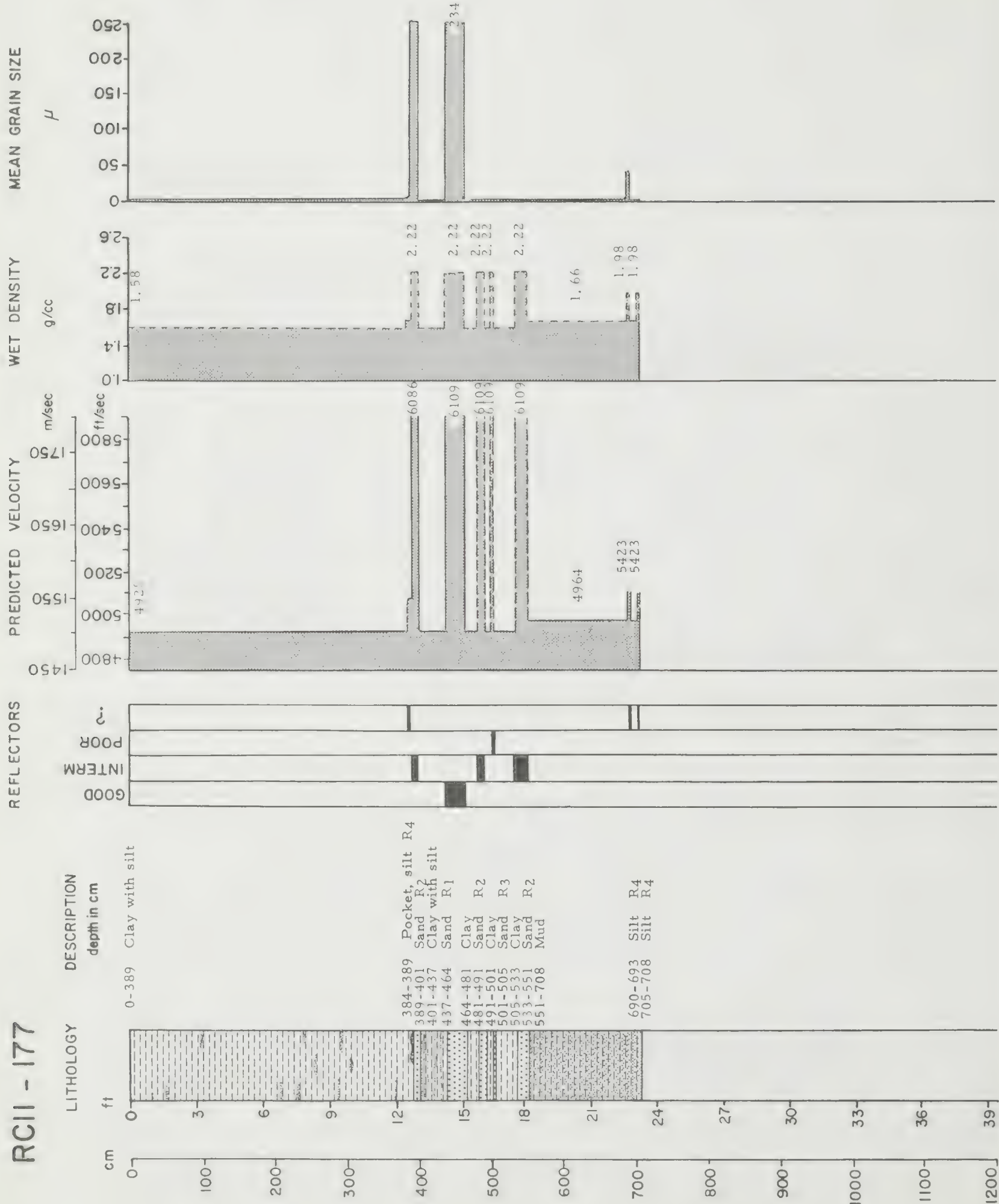
RCII - 175







RCII - 177



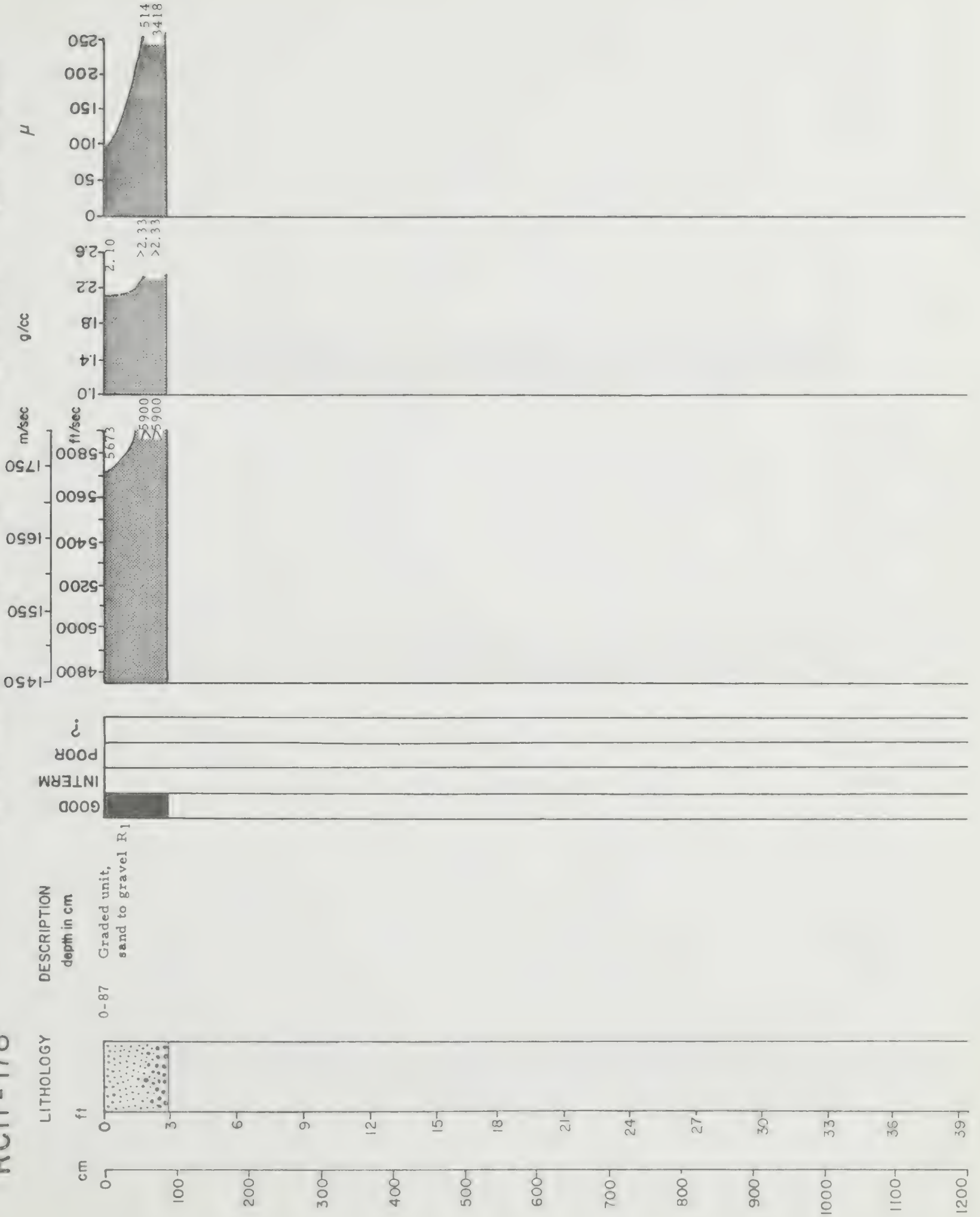
RC11-178

REFLECTORS

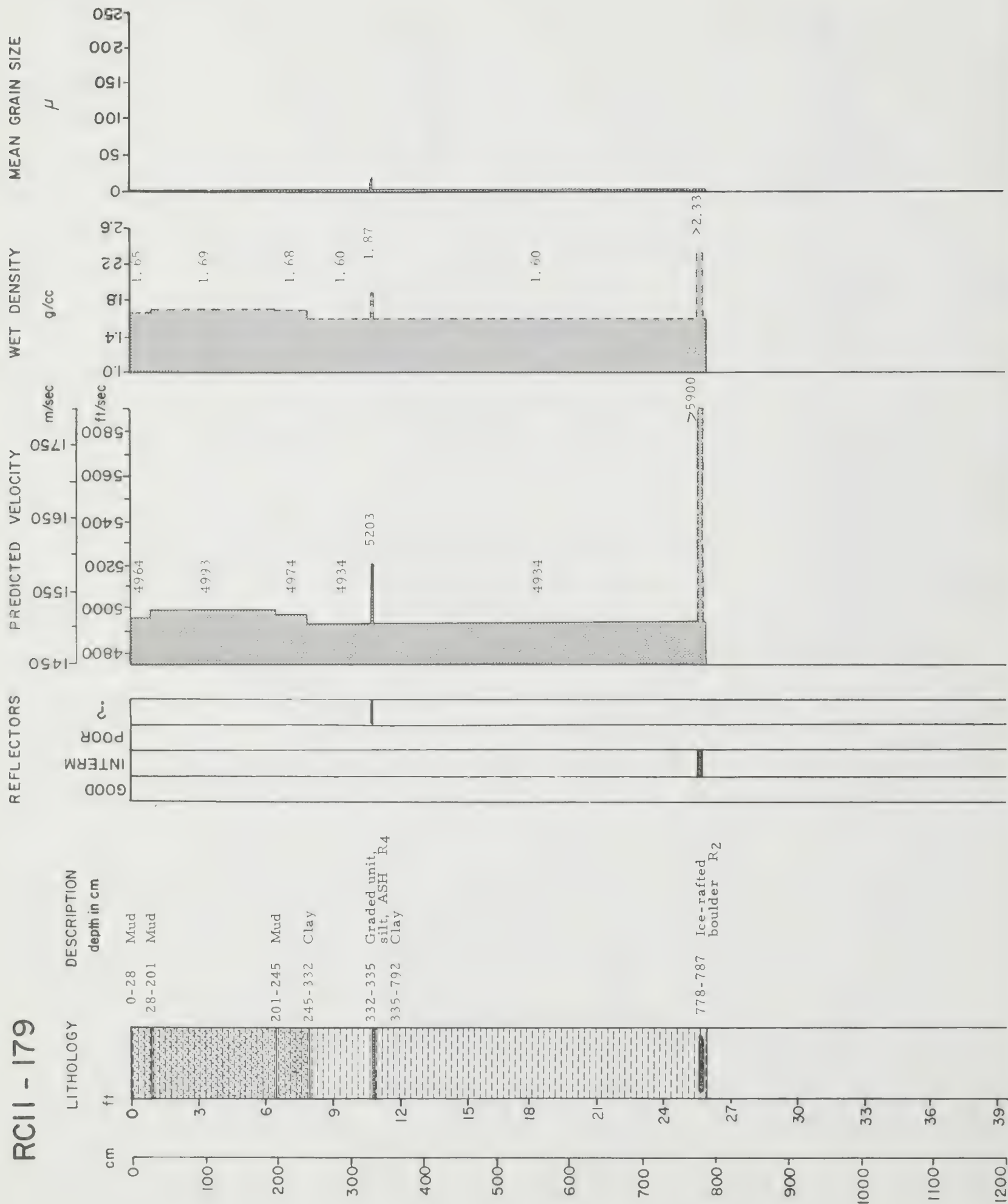
PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

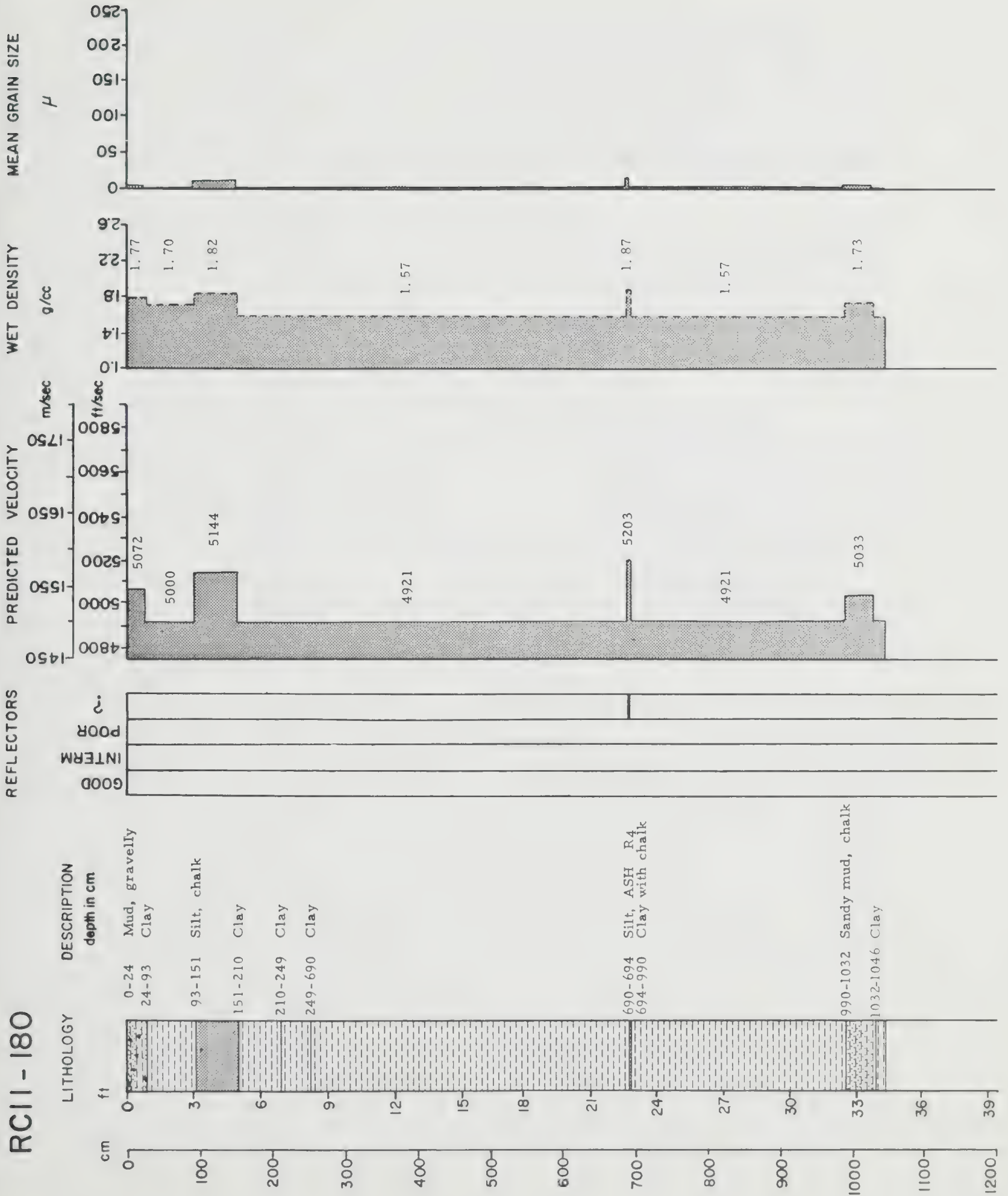


# RC11 - 179

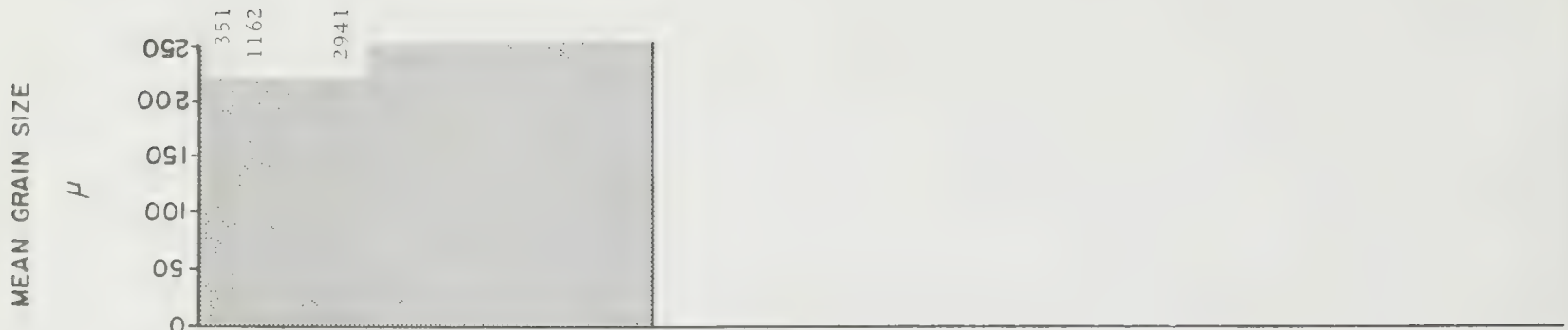
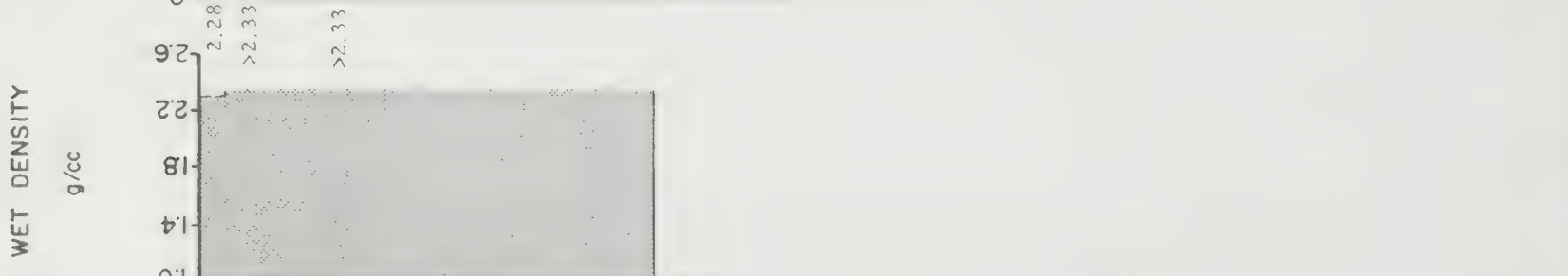
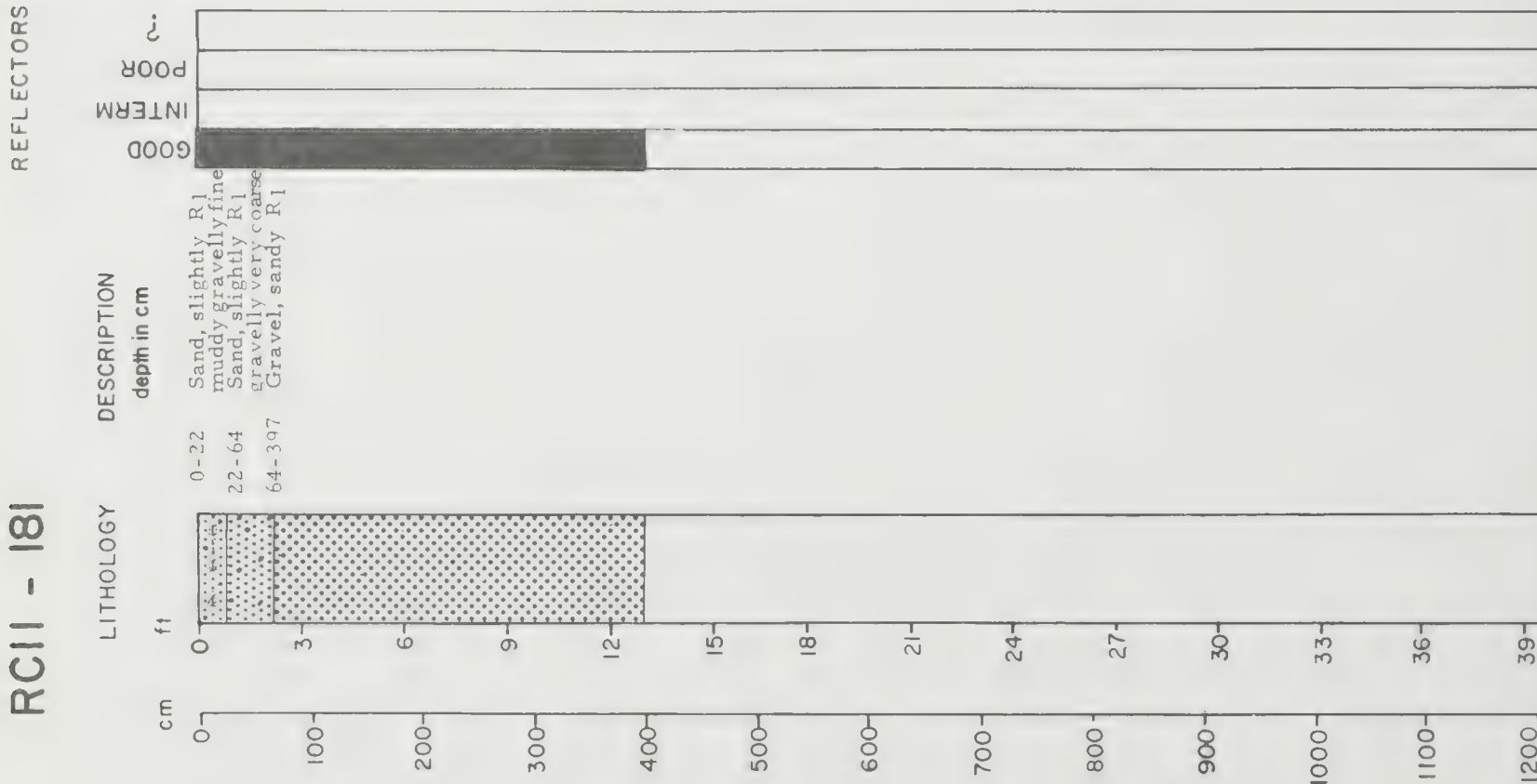


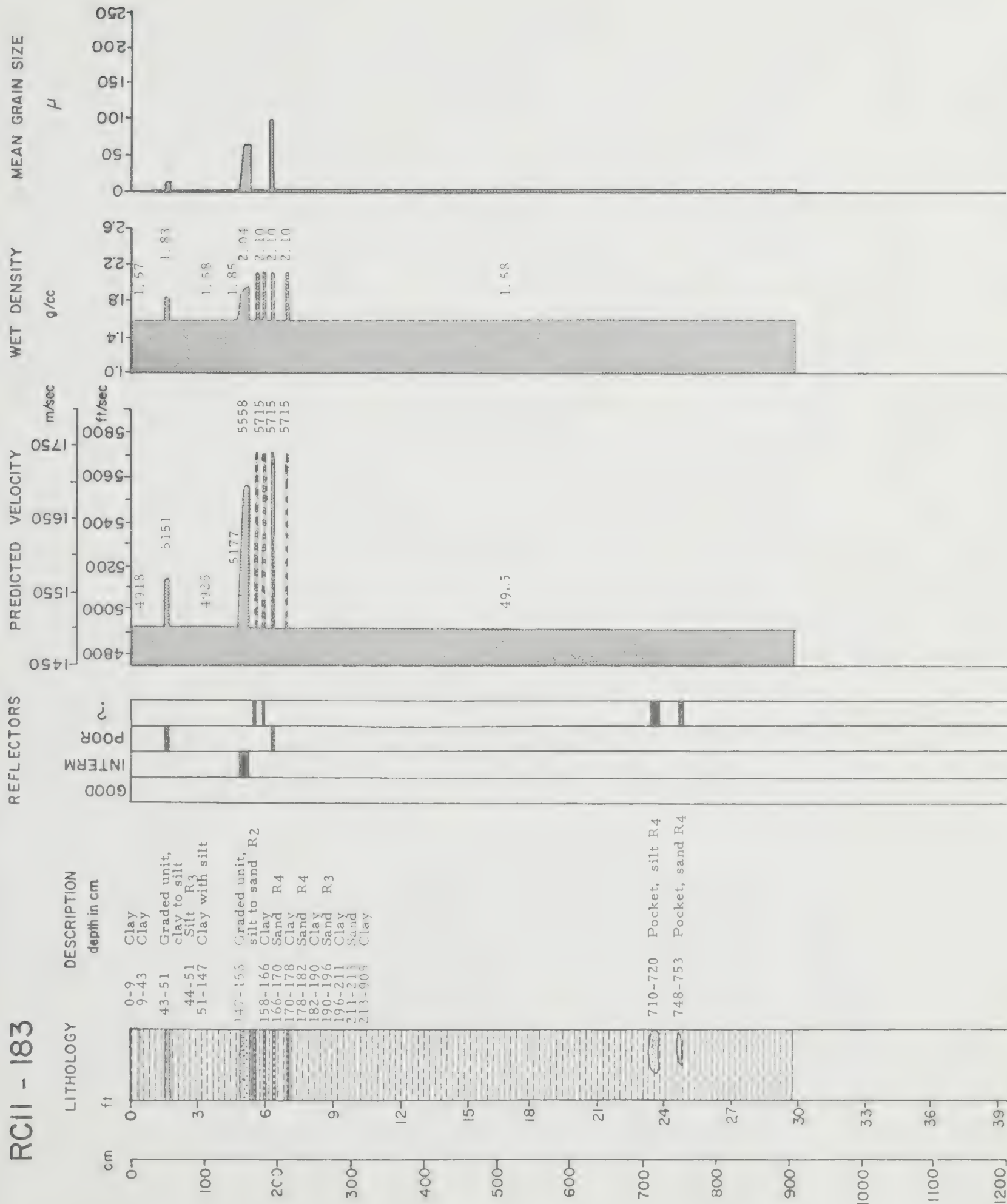


# RC11-180

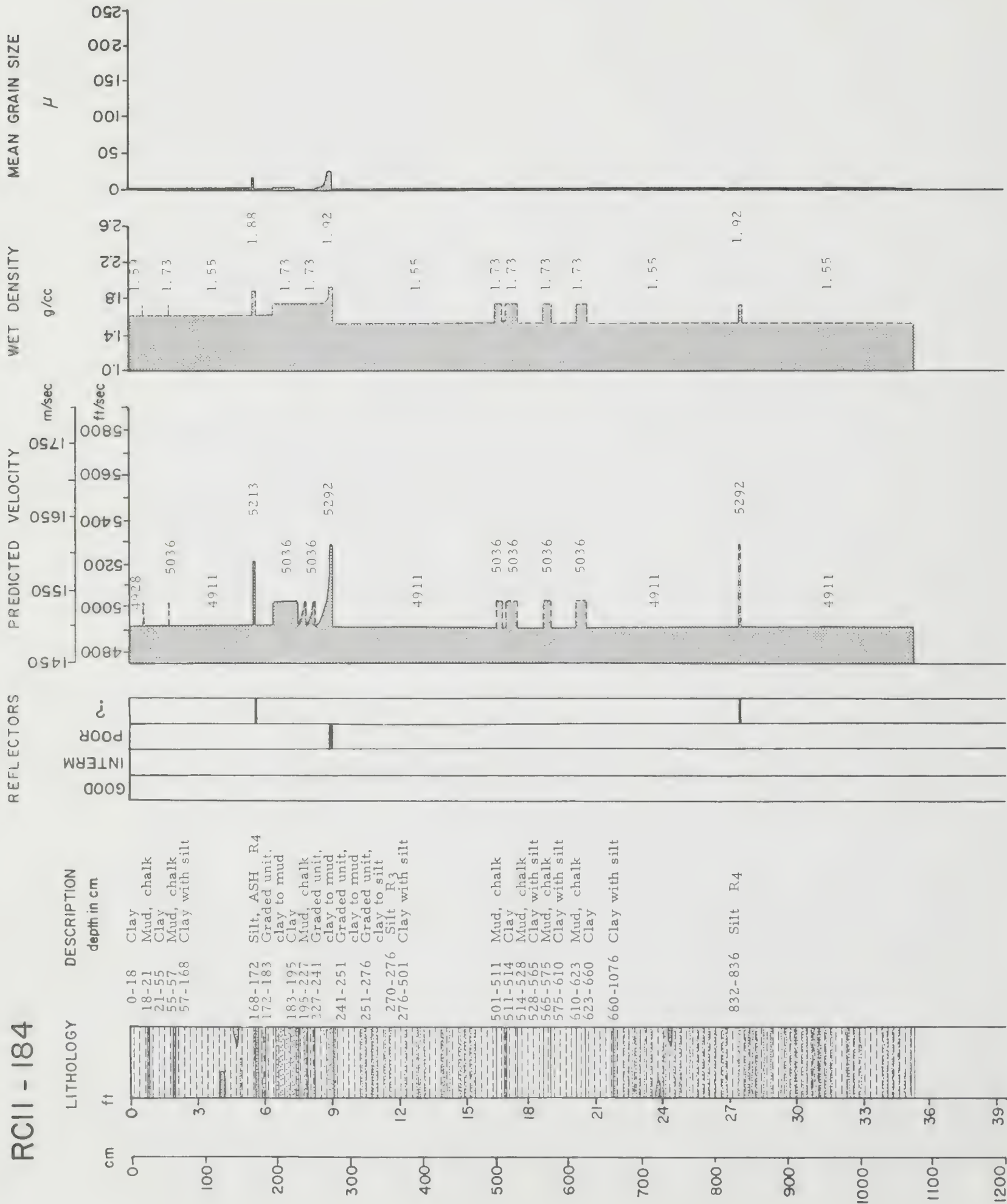


RC11 - 181



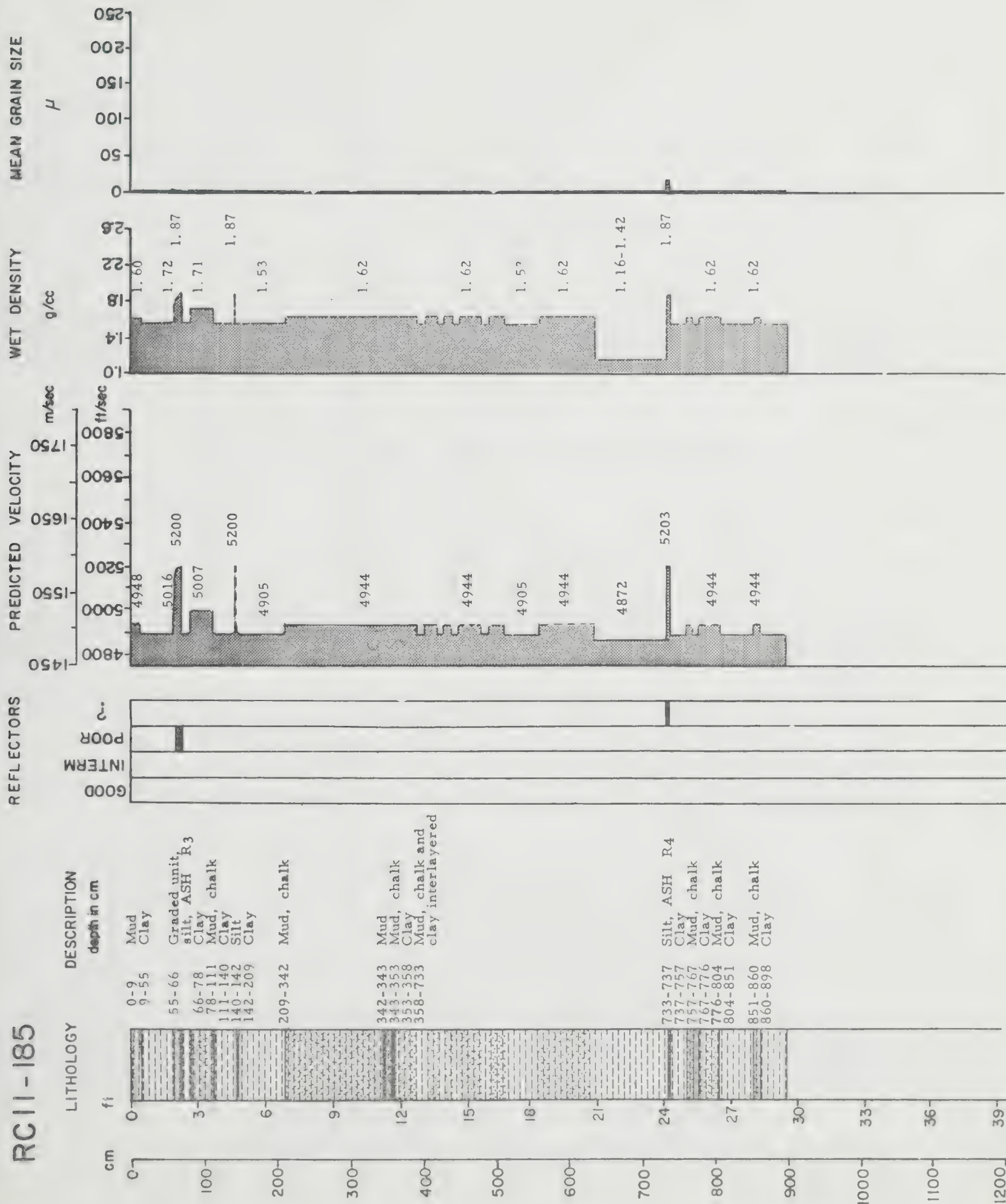


RC11 - 184

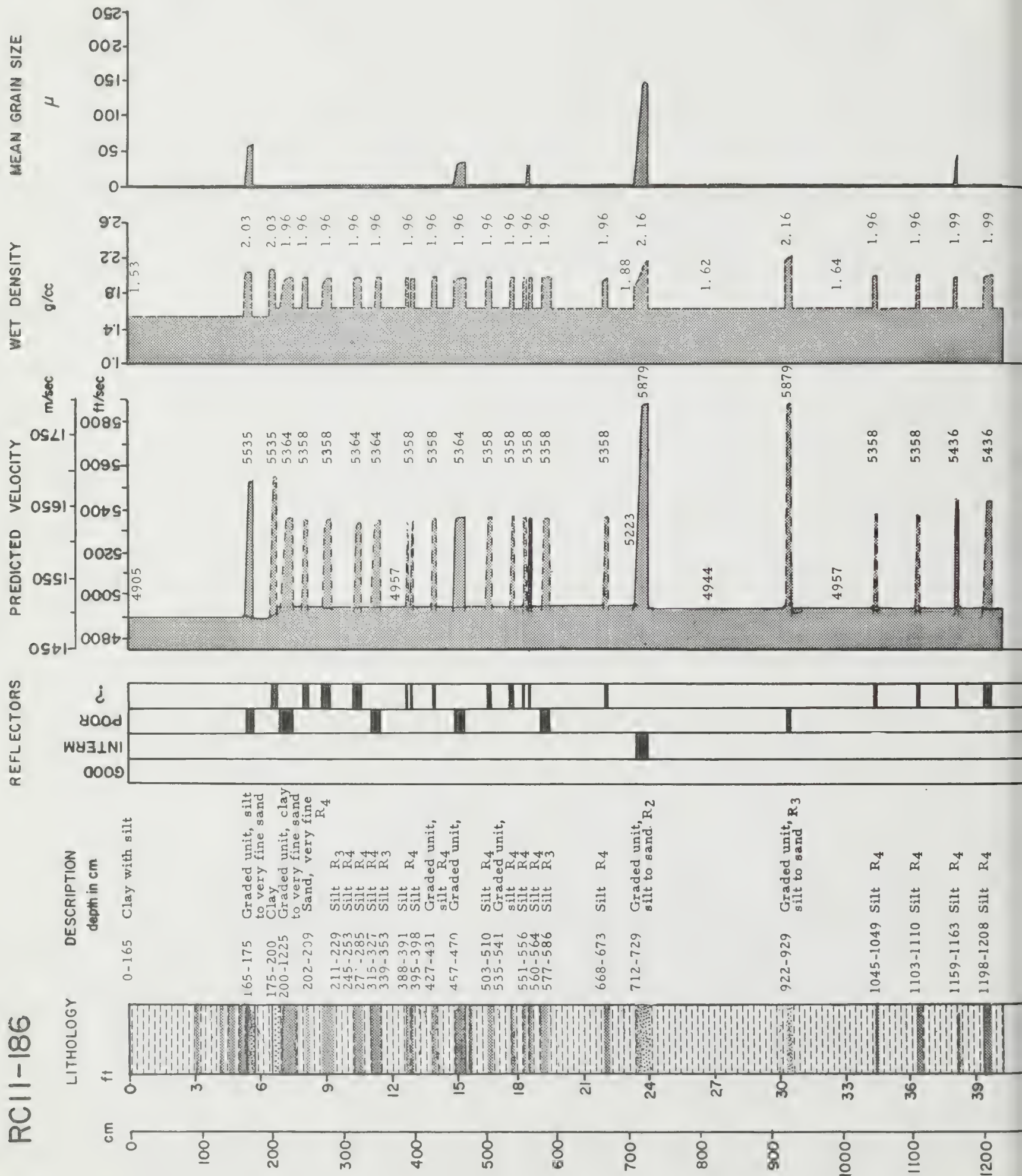


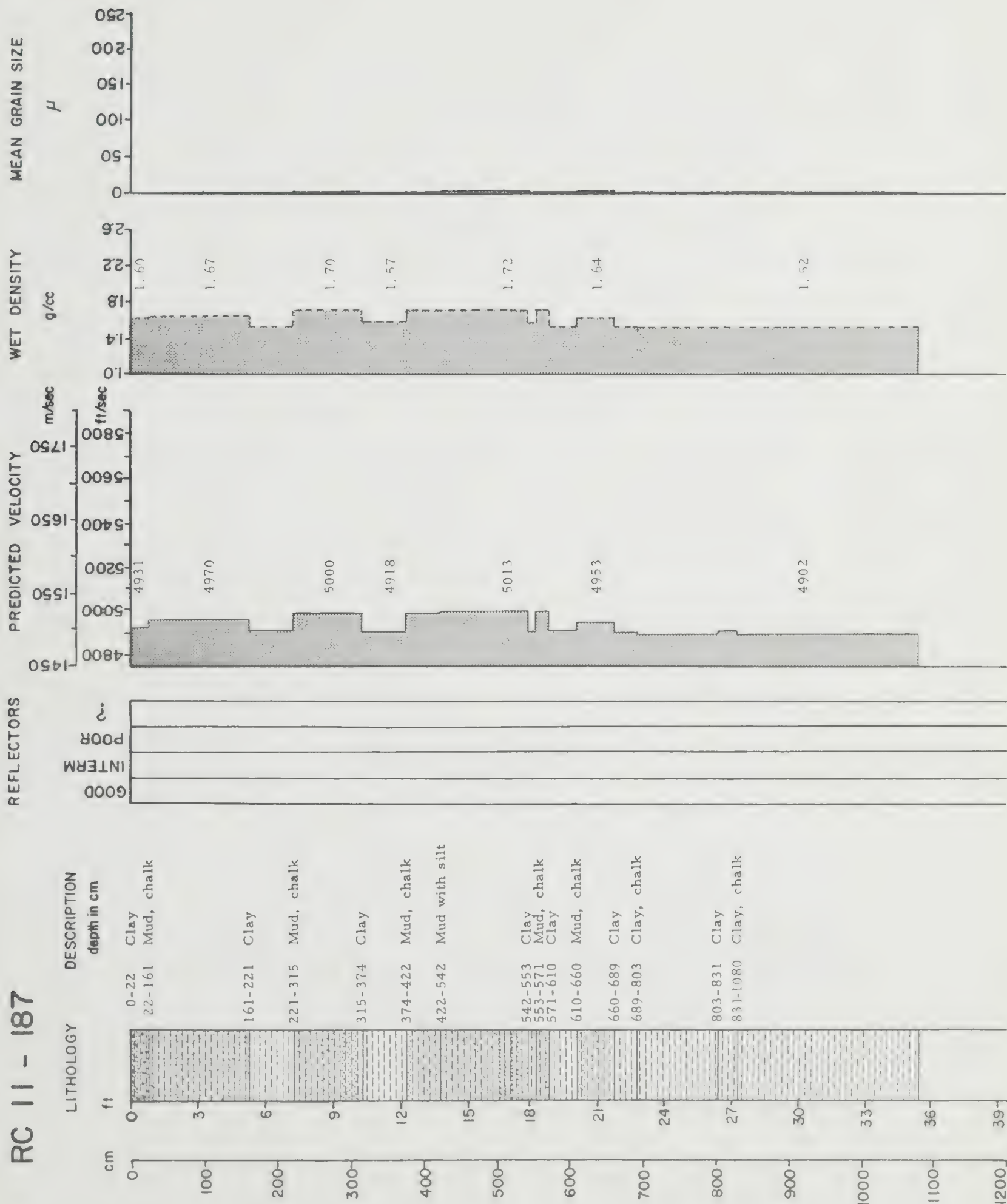


RC11-185



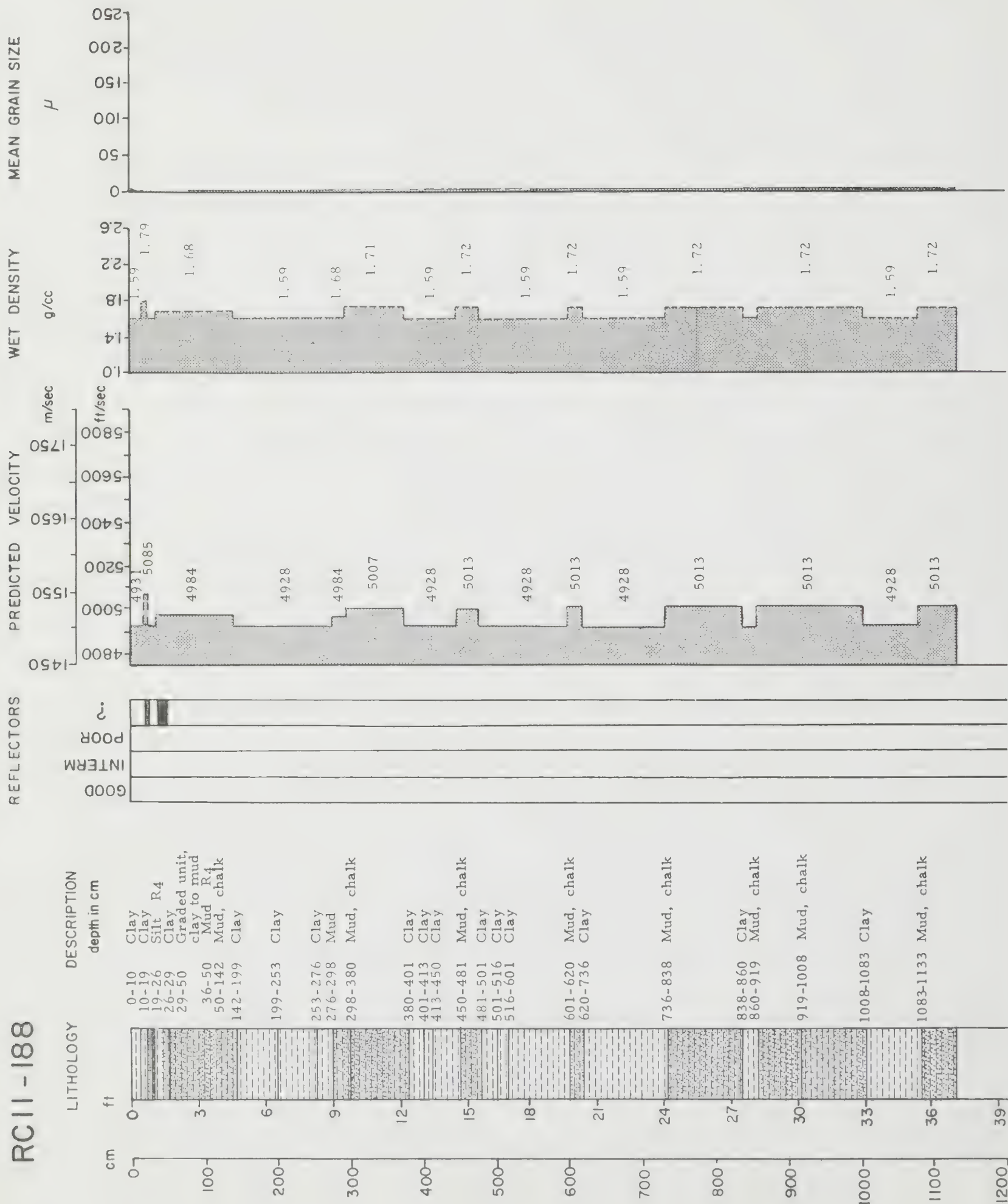
# RC11-186





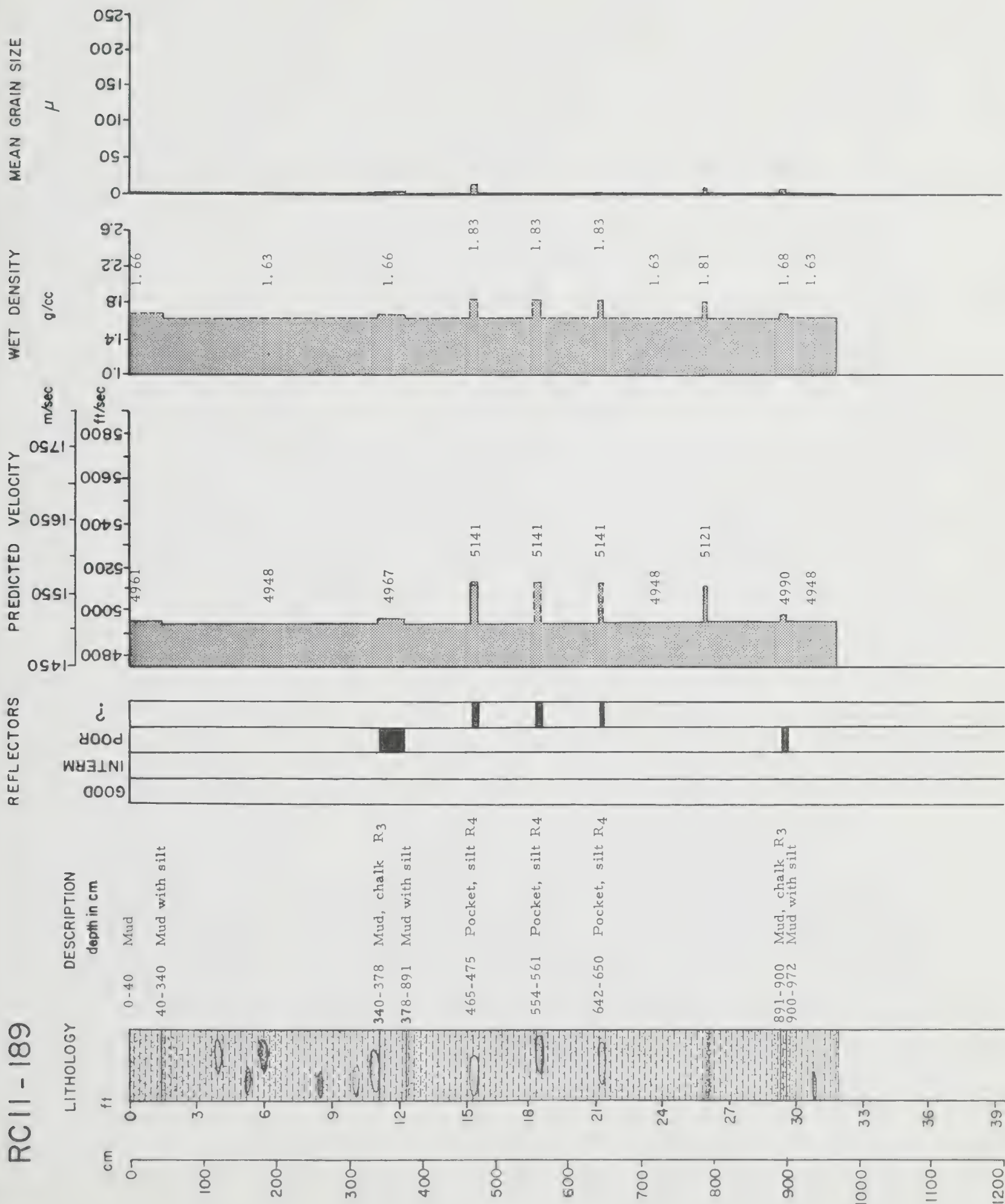


RC11-188





RC11-189



# RC11-190

## REFLECTORS

## PREDICTED VELOCITY

## WET DENSITY

## MEAN GRAIN SIZE

## DESCRIPTION

## LITHOLOGY

depth in cm

cm

ft

0-32 Graded unit, clay to silt  
 32-93 Graded unit, clay to silt  
 72-93 Graded unit, silt R2  
 93-132 Graded unit, clay to silt  
 109-132 Graded unit, silt R2  
 132-165 Graded unit, clay to silt  
 149-165 Graded unit, silt R2  
 165-200 Graded unit, clay to silt  
 184-200 Graded unit, silt R2  
 200-248 Graded unit, clay to silt  
 229-248 Graded unit, silt R2  
 248-281 Graded unit, clay to silt  
 271-281 Graded unit, silt R2  
 281-392 Clay  
 392-405 Graded unit, clay to silt  
 405-454 Silt R4  
 454-493 Graded unit, clay to silt  
 481-493 Silt R3  
 493-514 Graded unit, clay  
 514-535 Graded unit, clay  
 535-578 Graded unit, clay to silt  
 559-578 Silt R3  
 578-586 Clay  
 586-620 Graded unit, clay to silt  
 609-620 Silt R2  
 620-641 Clay  
 641-656 Graded unit, clay to silt  
 649-656 Silt R3  
 656-696 Clay  
 696-865 Clay  
 865-881 Graded unit, clay to mud  
 881-903 Graded unit, clay to silt  
 900-903 Silt R4  
 903-914 Graded unit, clay to silt  
 910-914 Silt R4  
 914-958 Graded unit, clay  
 958-982 Graded unit, clay to silt  
 972-982 Silt R3  
 982-985 Clay

GOOD  
 INTERM  
 POOR  
 ?

4800  
 4900  
 5000  
 5100  
 5200  
 5300  
 5400  
 5500  
 5600  
 5700  
 5800  
 5900  
 6000  
 6100  
 6200  
 6300  
 6400  
 6500  
 6600  
 6700  
 6800  
 6900  
 7000  
 7100  
 7200  
 7300  
 7400  
 7500  
 7600  
 7700  
 7800  
 7900  
 8000  
 8100  
 8200  
 8300  
 8400  
 8500  
 8600  
 8700  
 8800  
 8900  
 9000  
 9100  
 9200  
 9300  
 9400  
 9500  
 9600  
 9700  
 9800  
 9900  
 10000  
 10100  
 10200  
 10300  
 10400  
 10500  
 10600  
 10700  
 10800  
 10900  
 11000  
 11100  
 11200  
 11300  
 11400  
 11500  
 11600  
 11700  
 11800  
 11900  
 12000

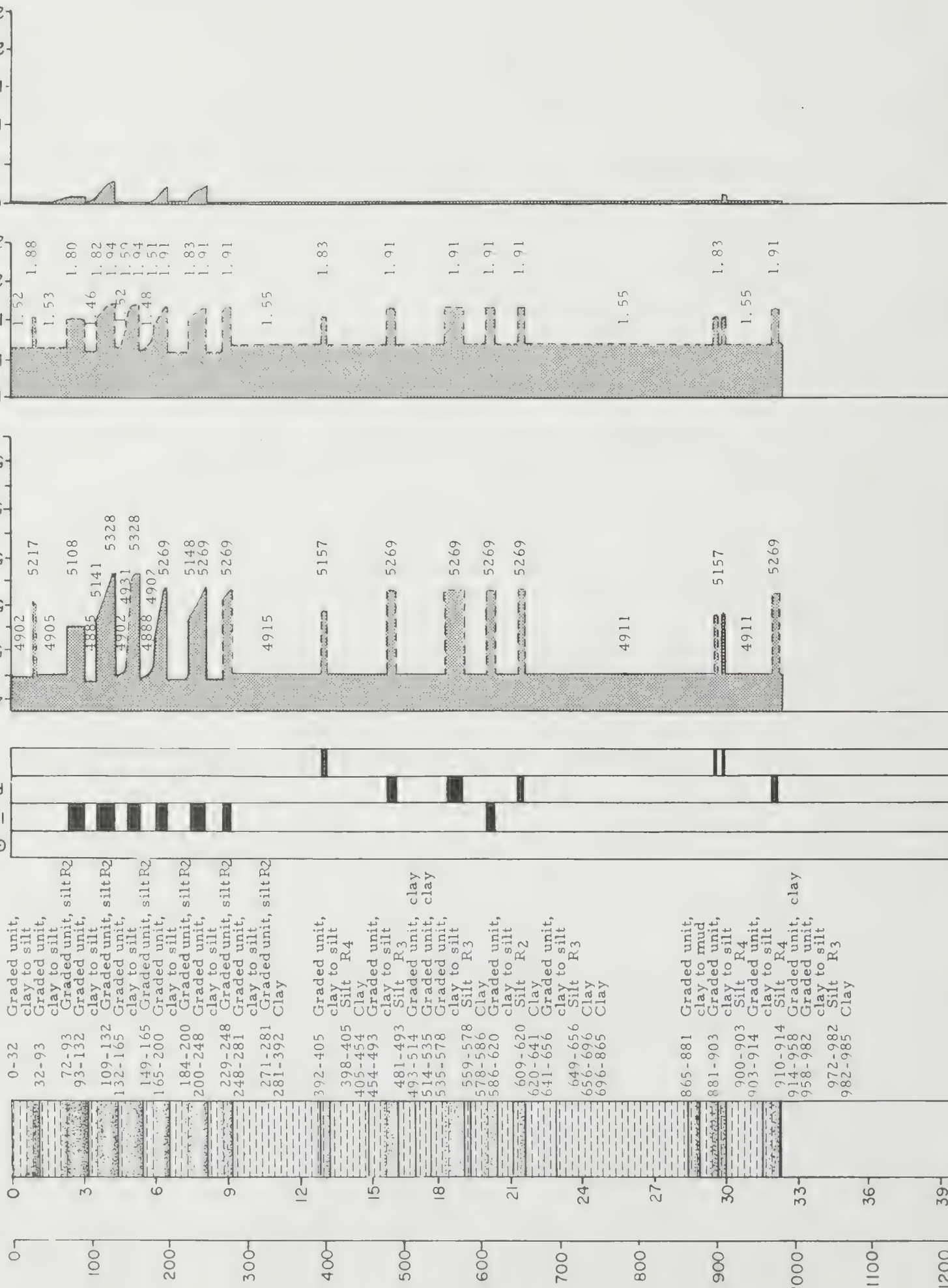
m/sec

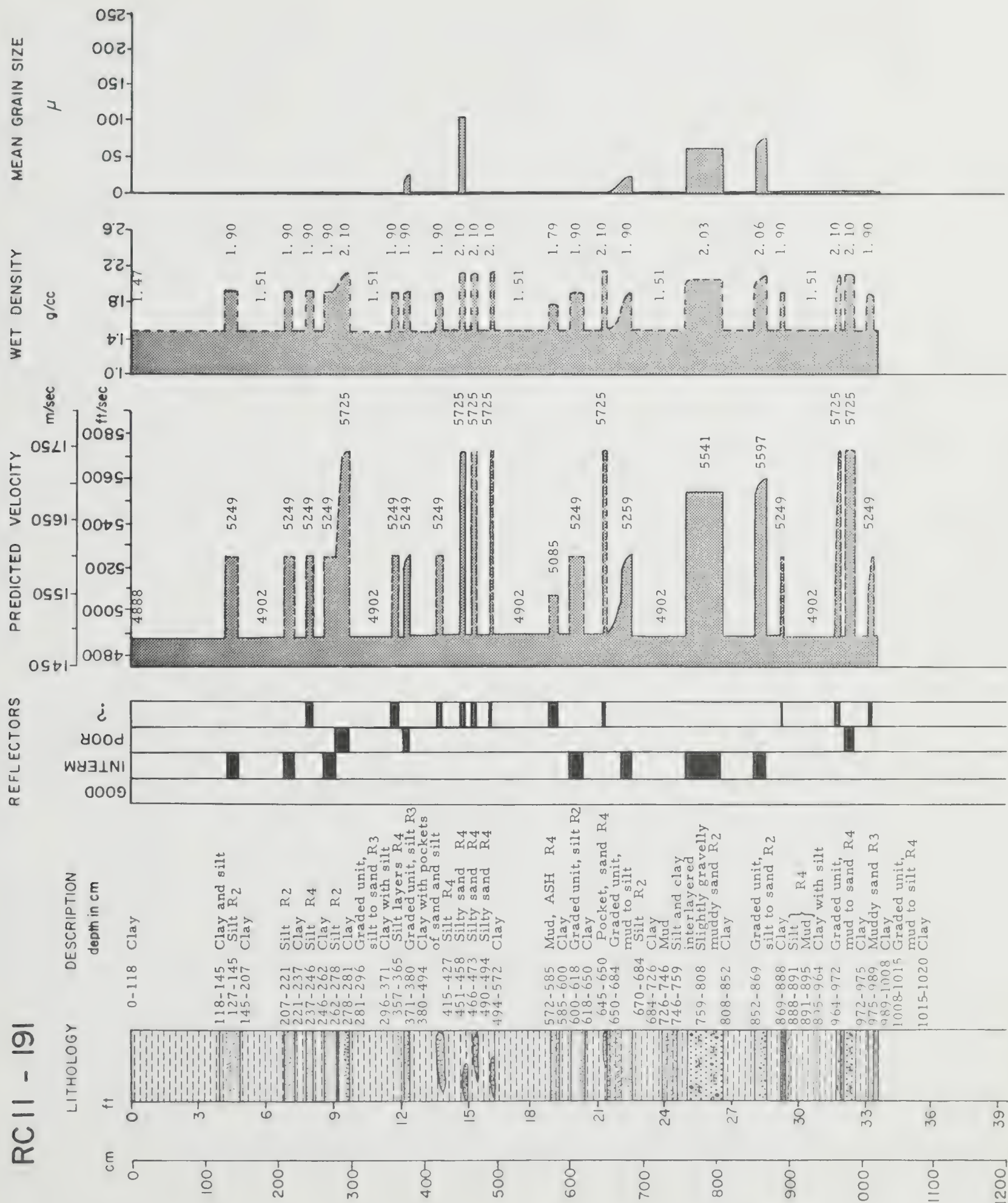
ft/sec

1.0  
 1.2  
 1.4  
 1.6  
 1.8  
 2.0  
 2.2  
 2.4  
 2.6

μ

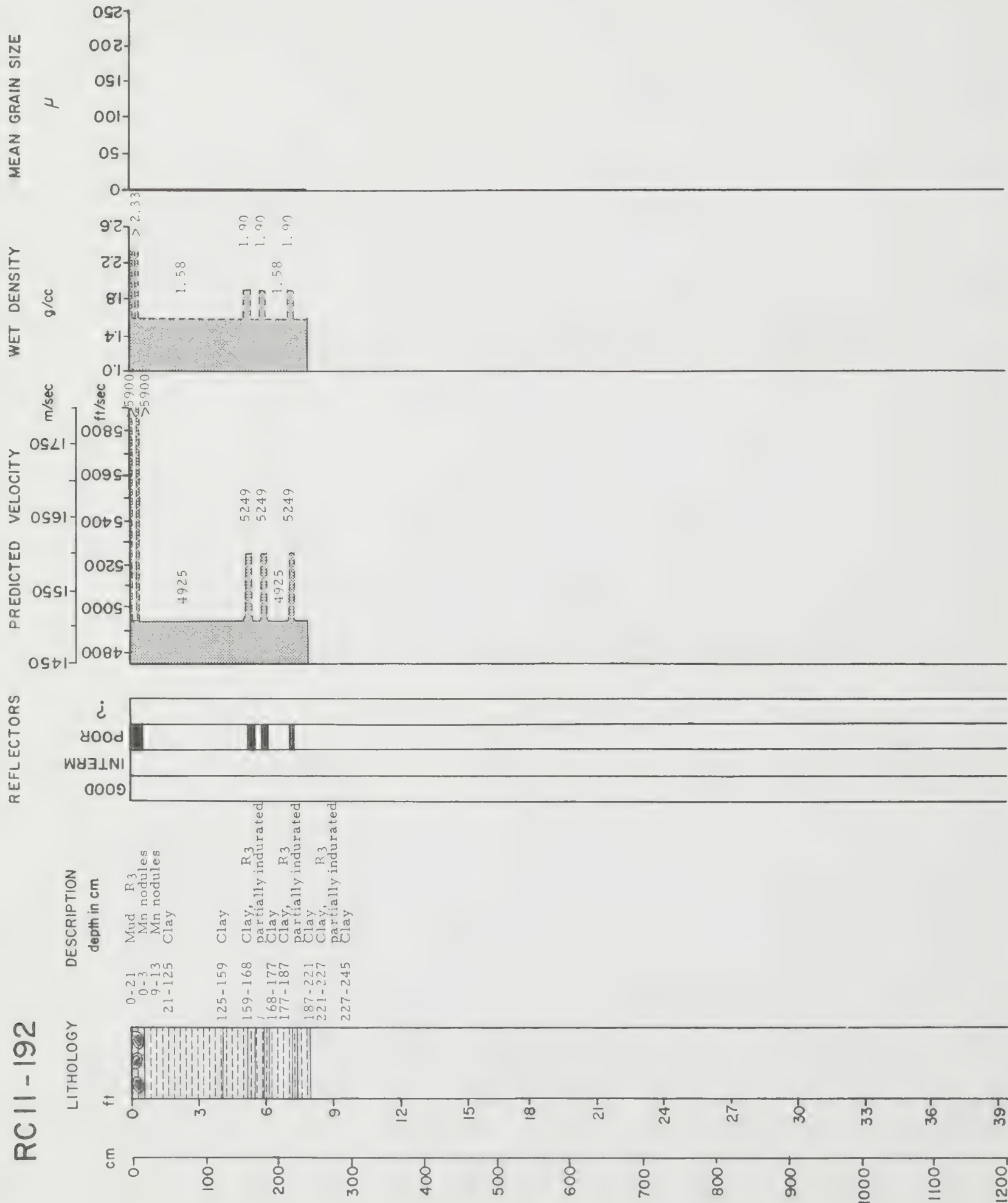
0  
 50  
 100  
 150  
 200  
 250





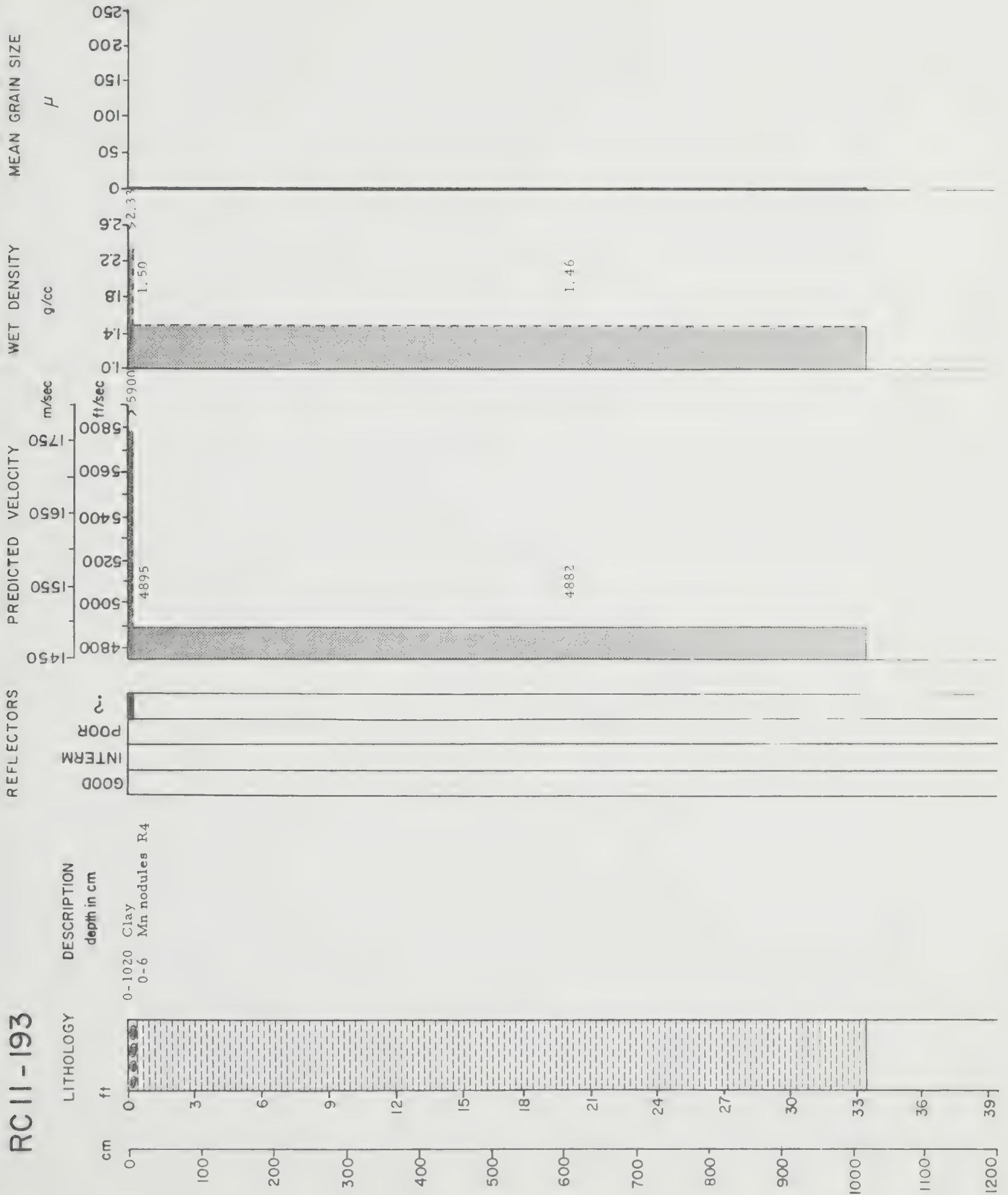


RC 11-192

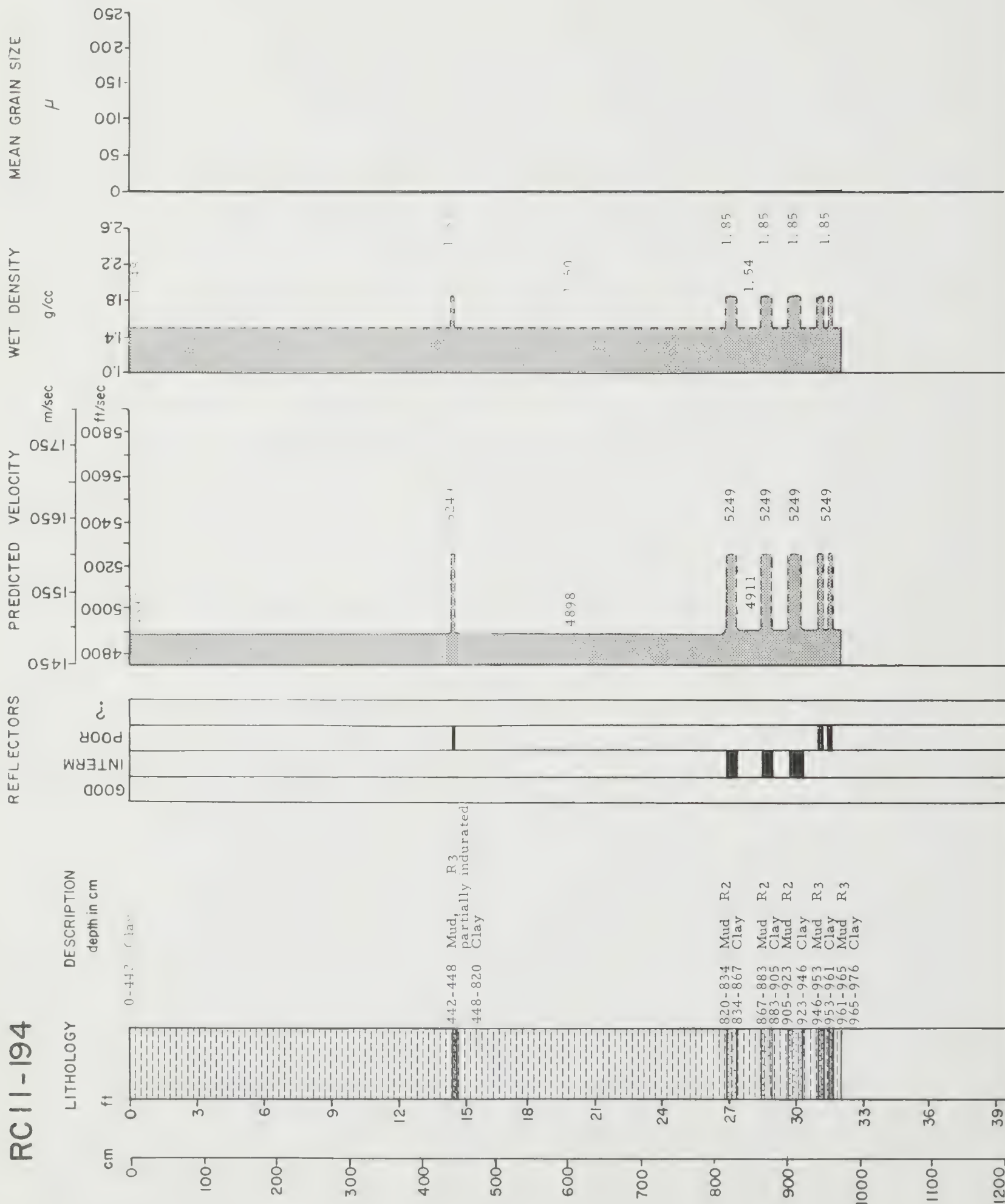




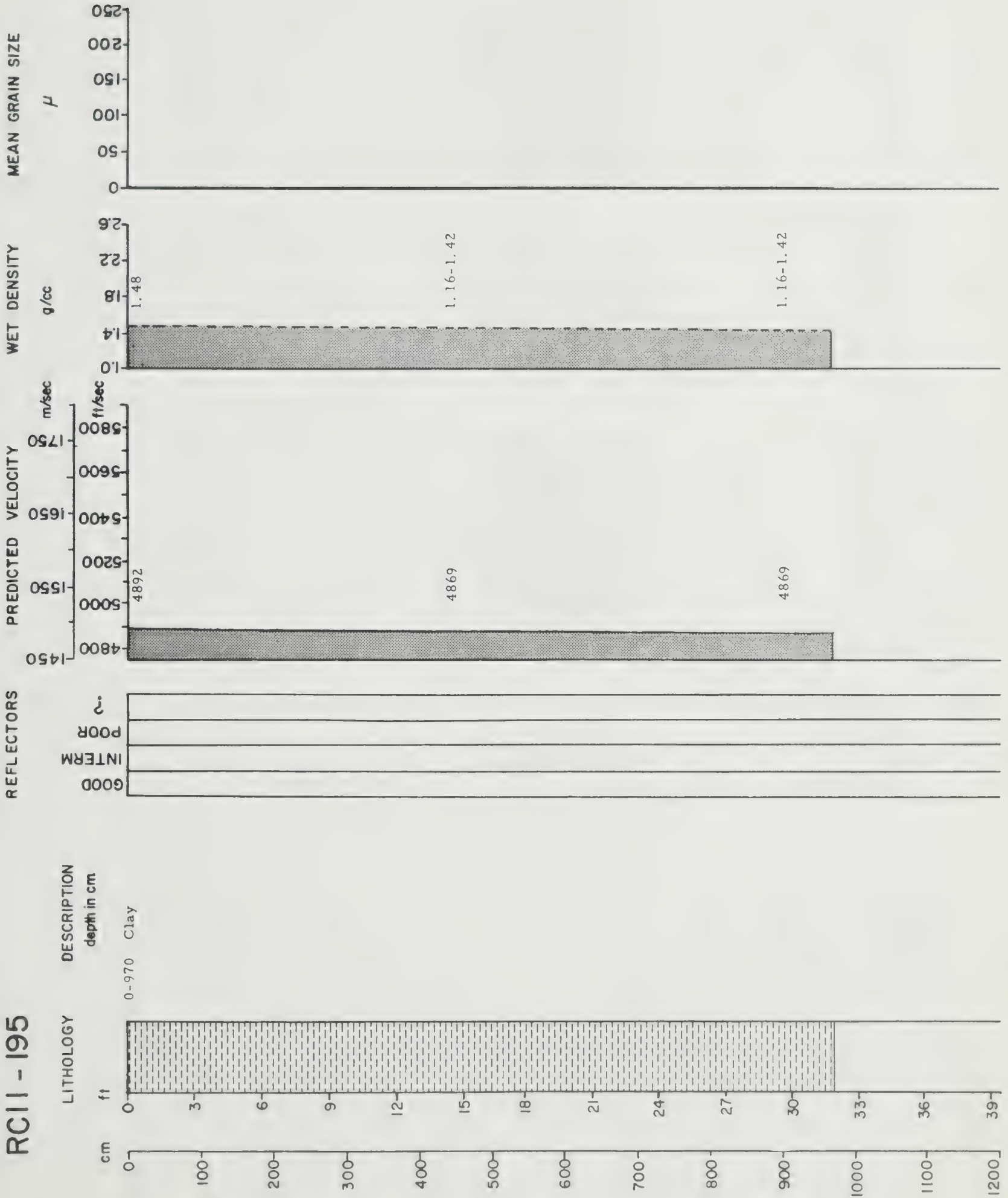
# RC11-193



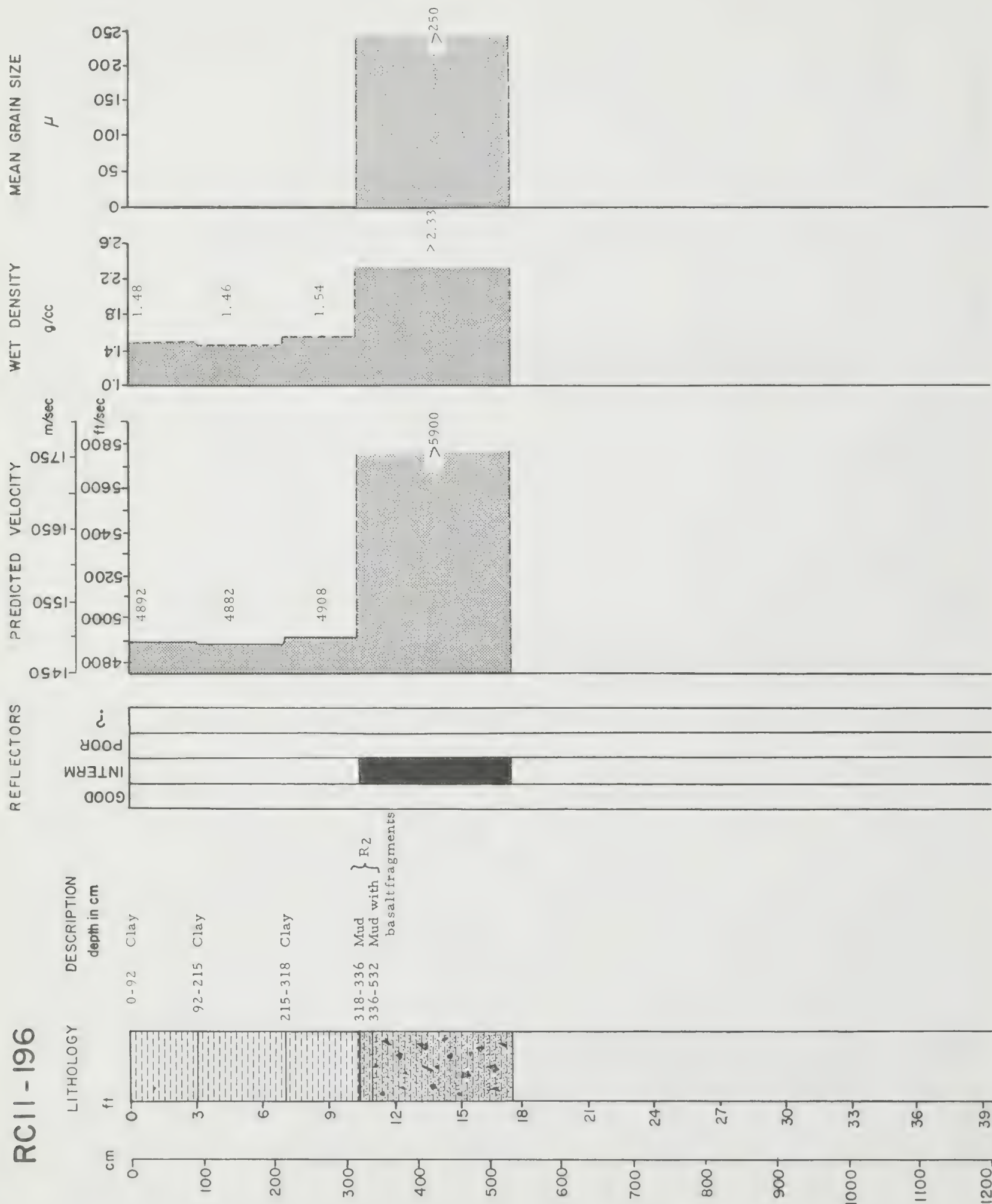
# RC11-194



# RC11 - 195

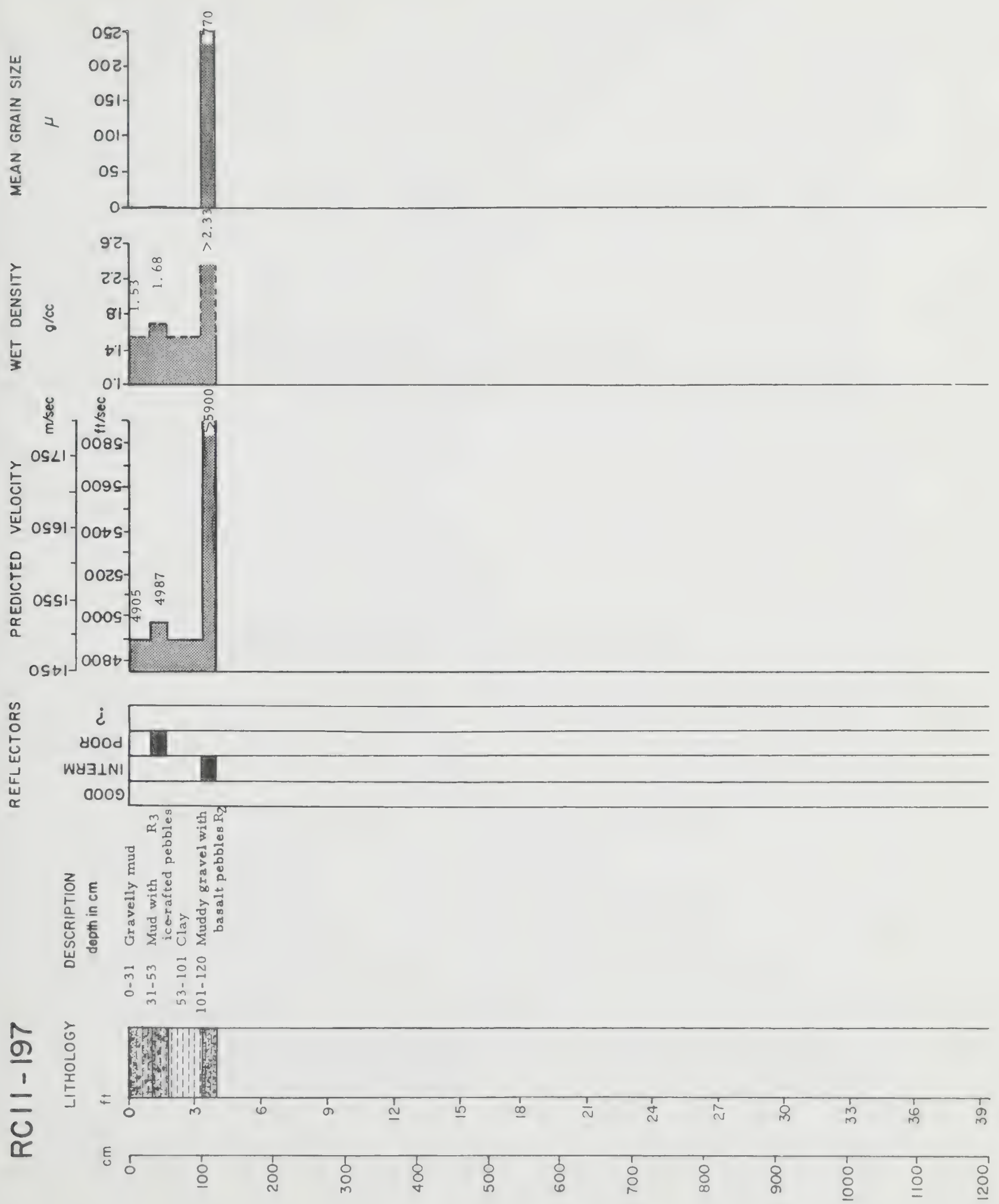


RC11-196

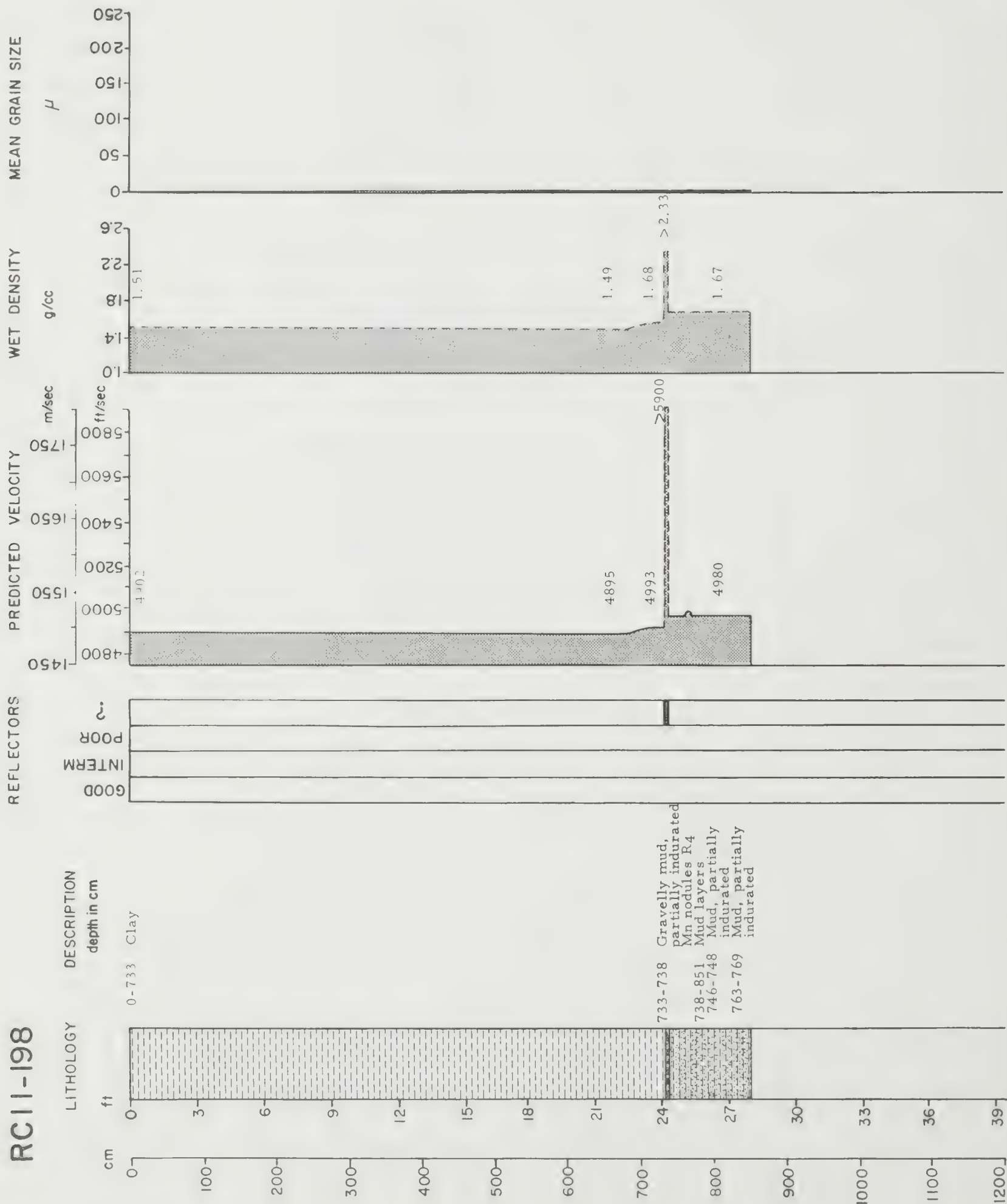


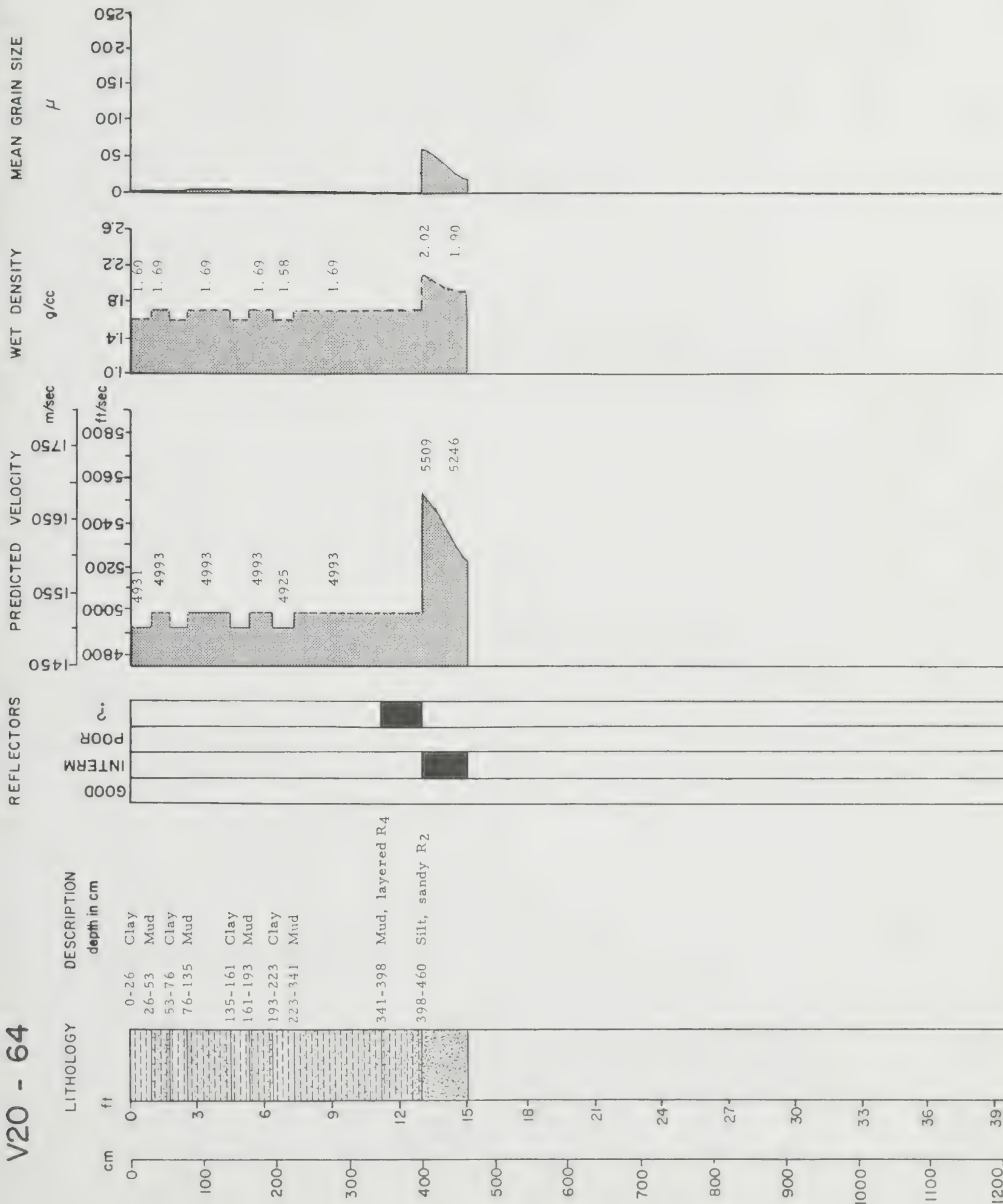


RC11-197

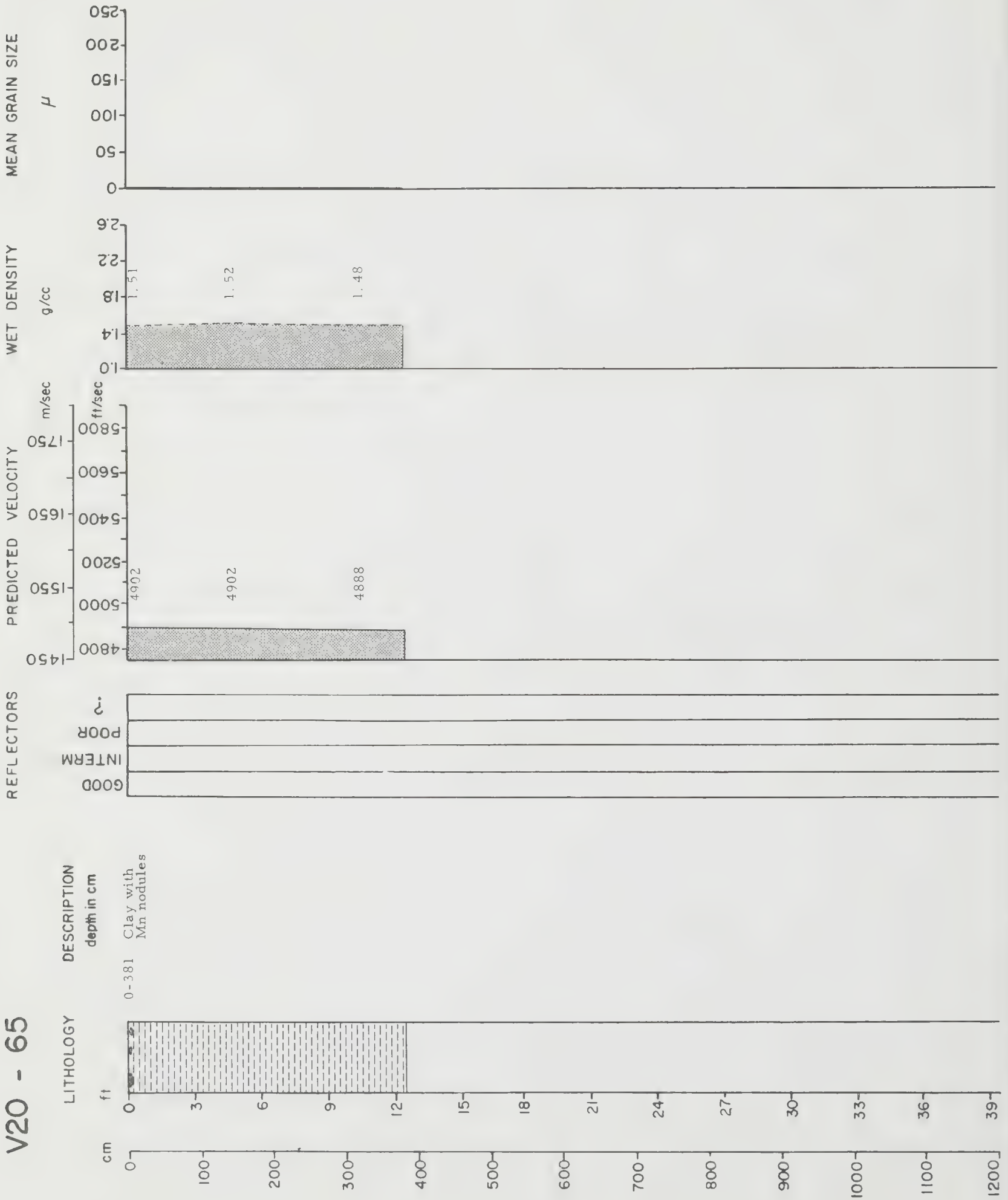


# RC11-198



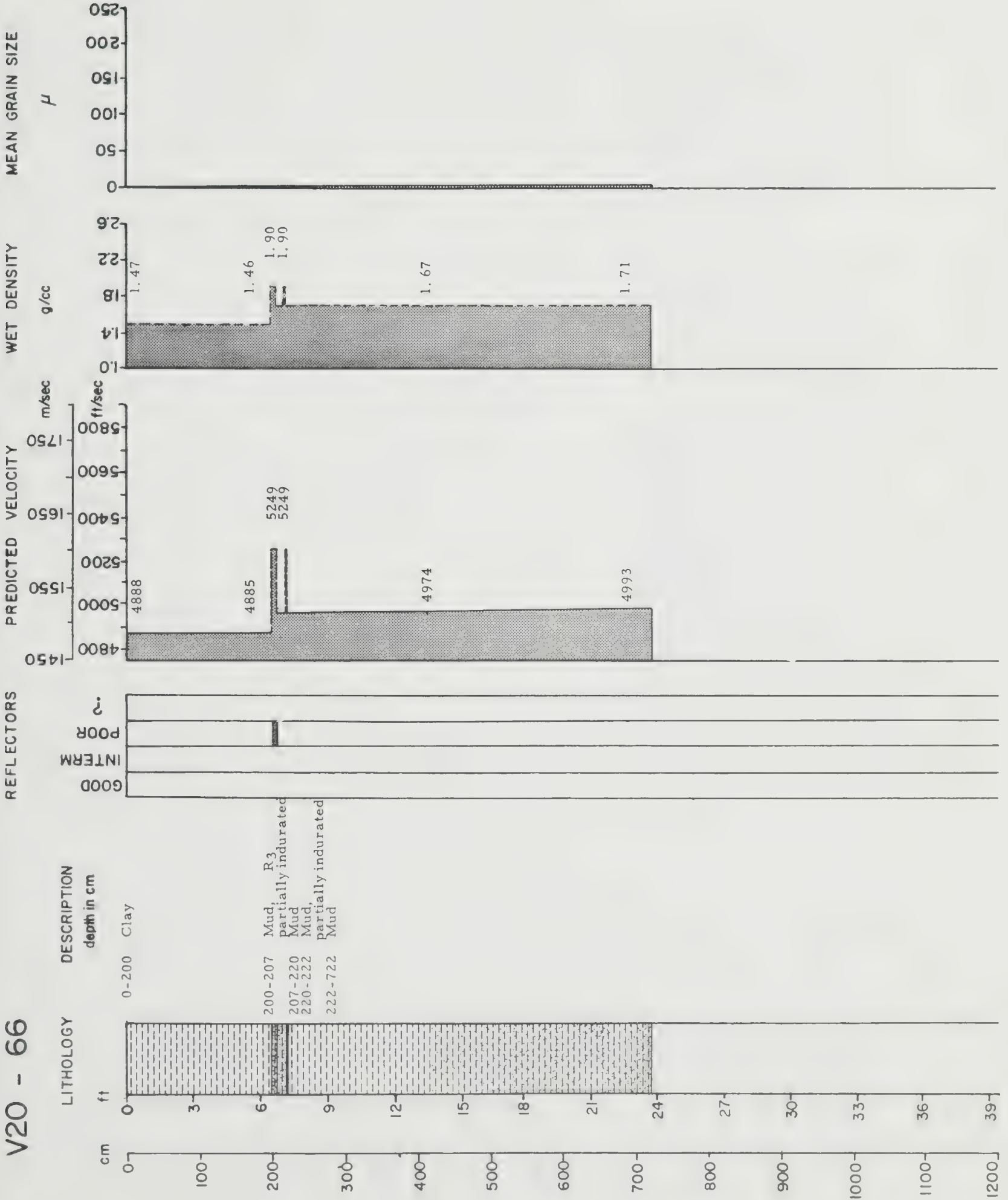


# V20 - 65

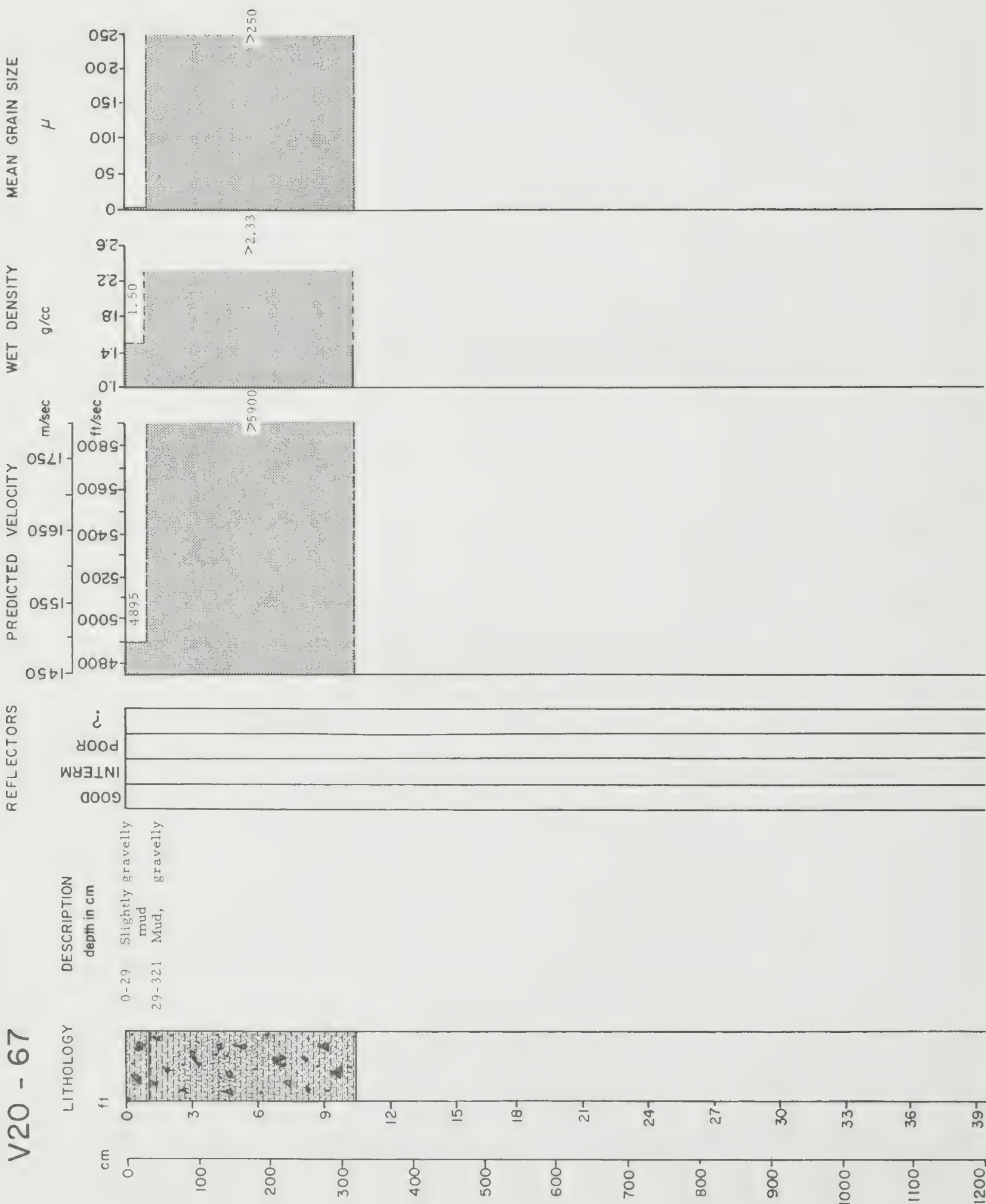




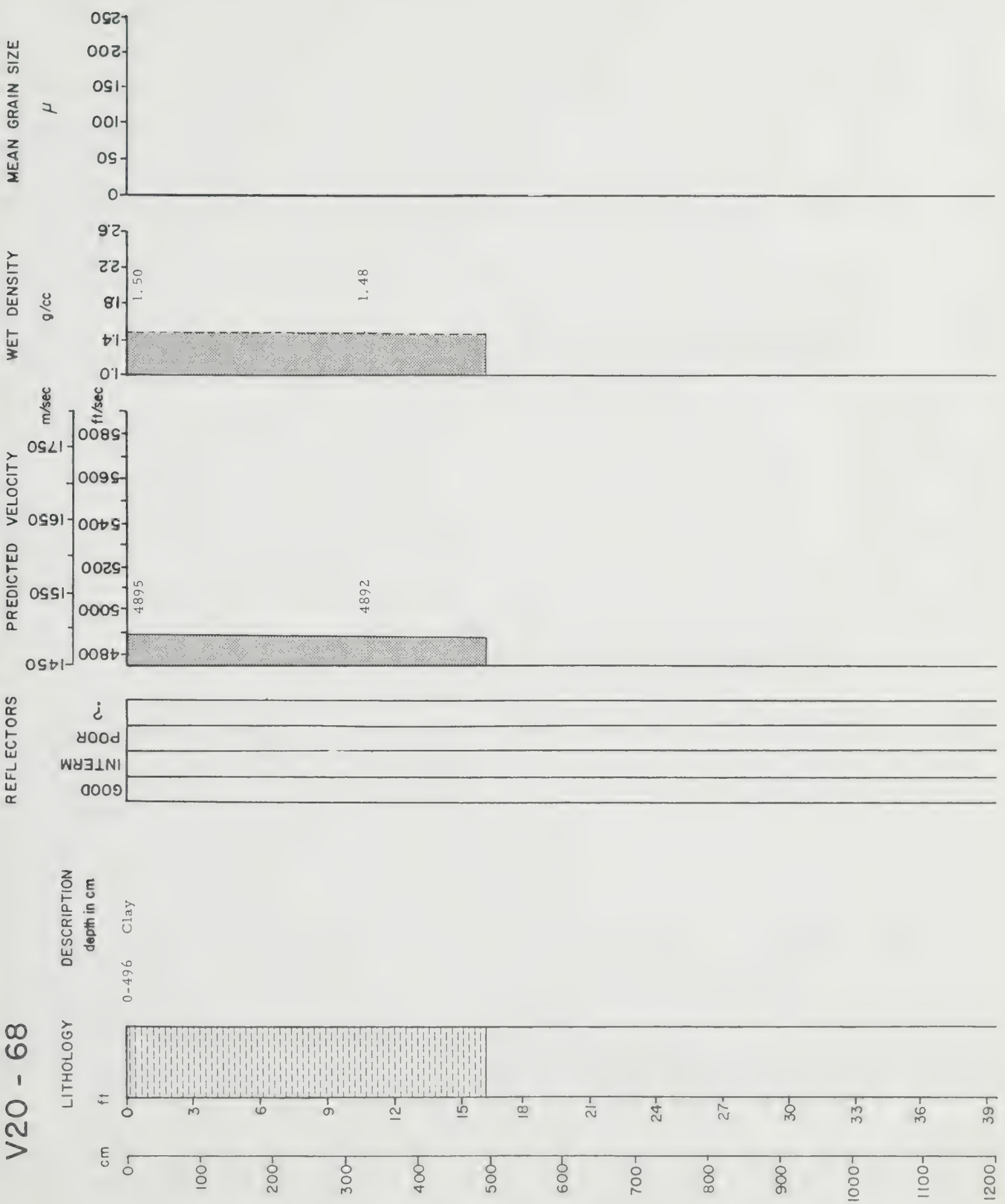
V20 - 66



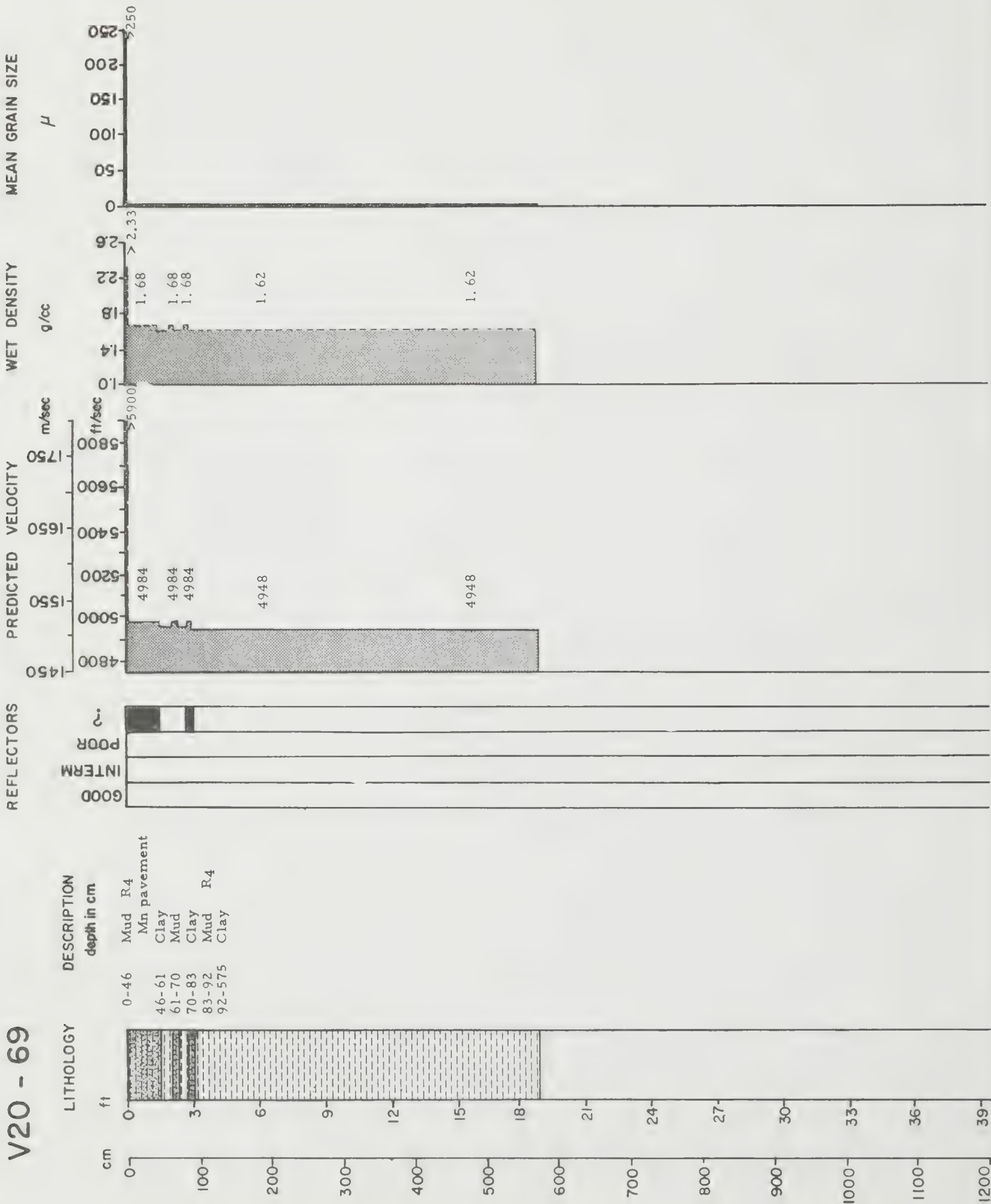
V20 - 67



# V20 - 68

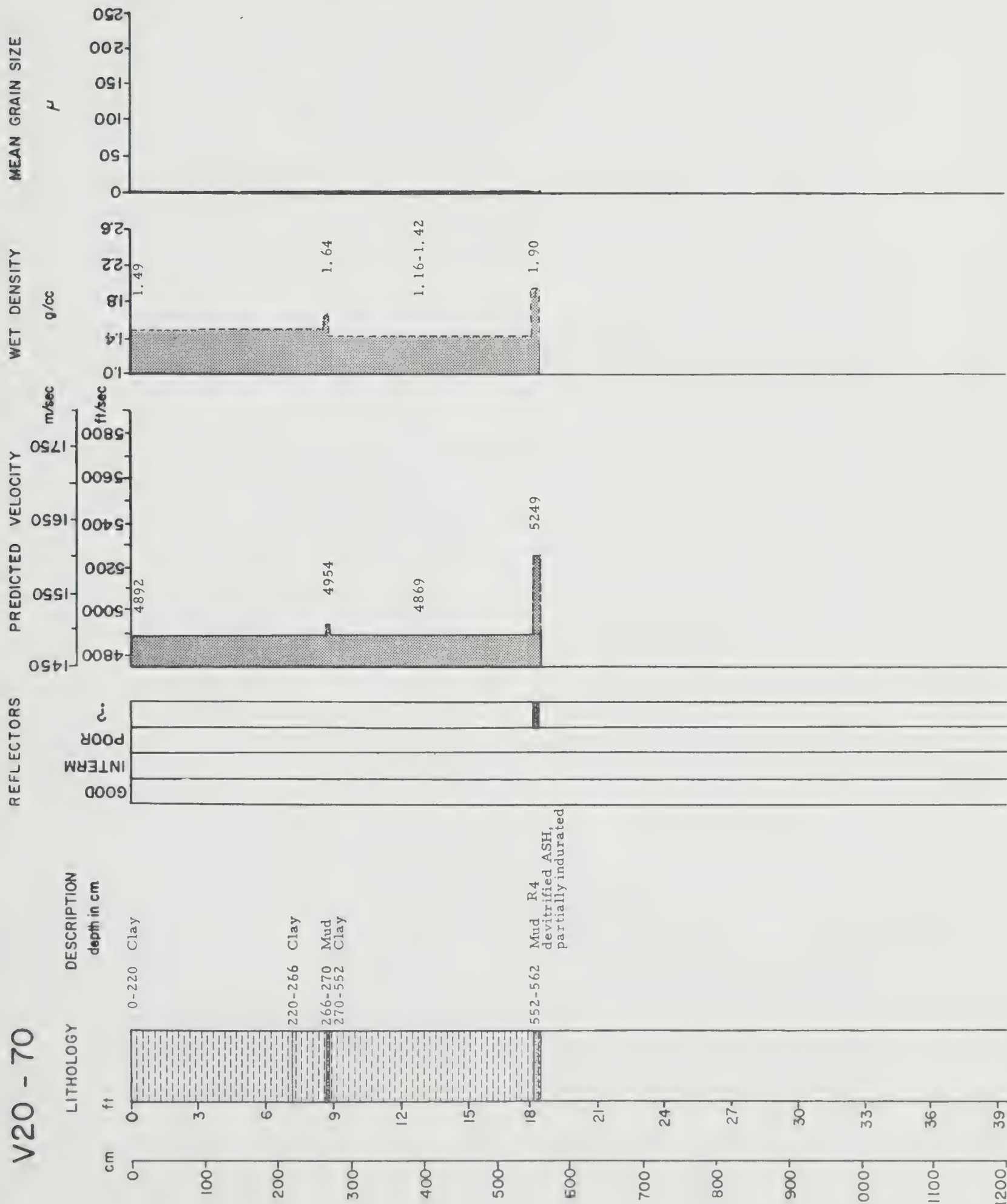


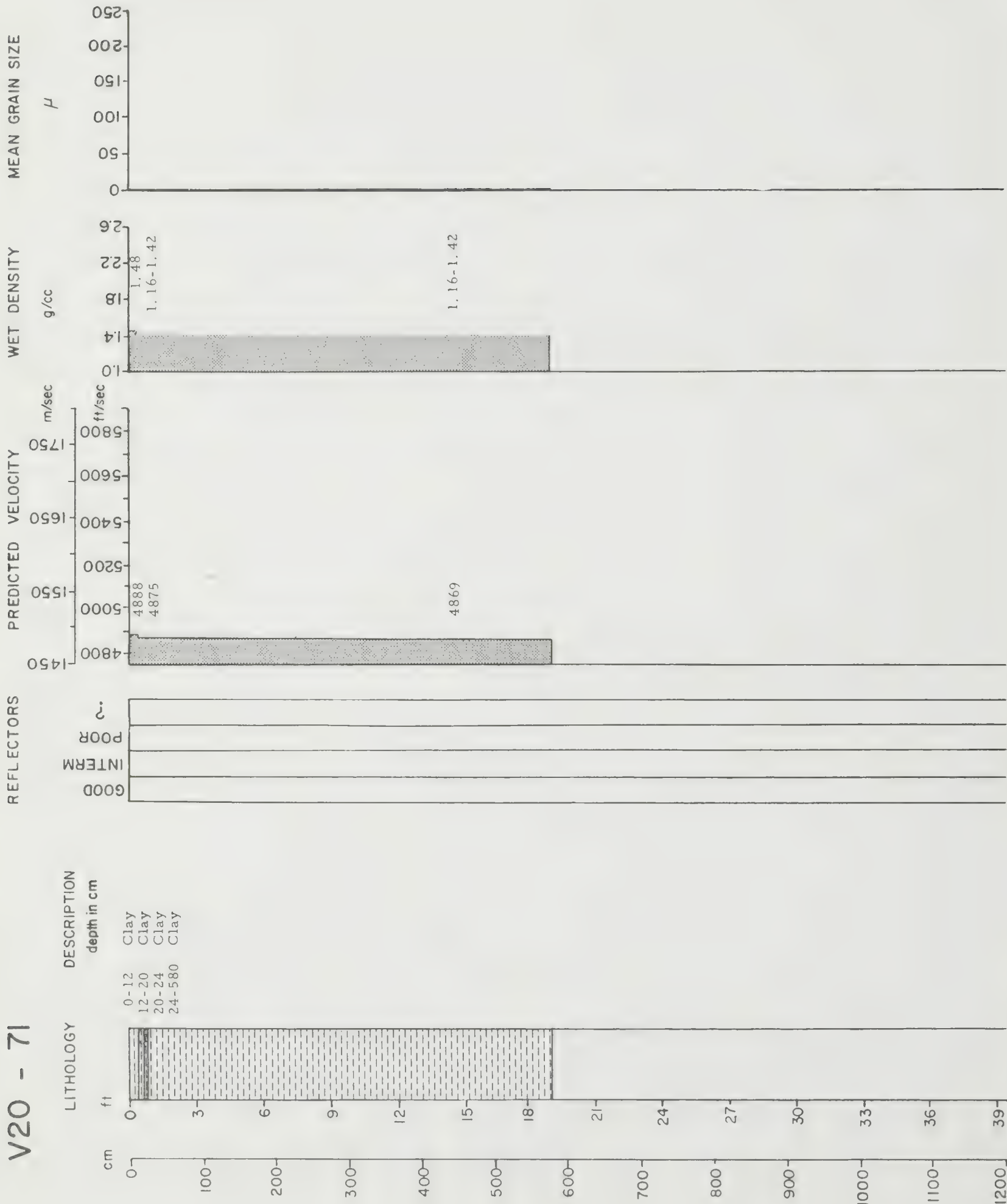
# V20 - 69

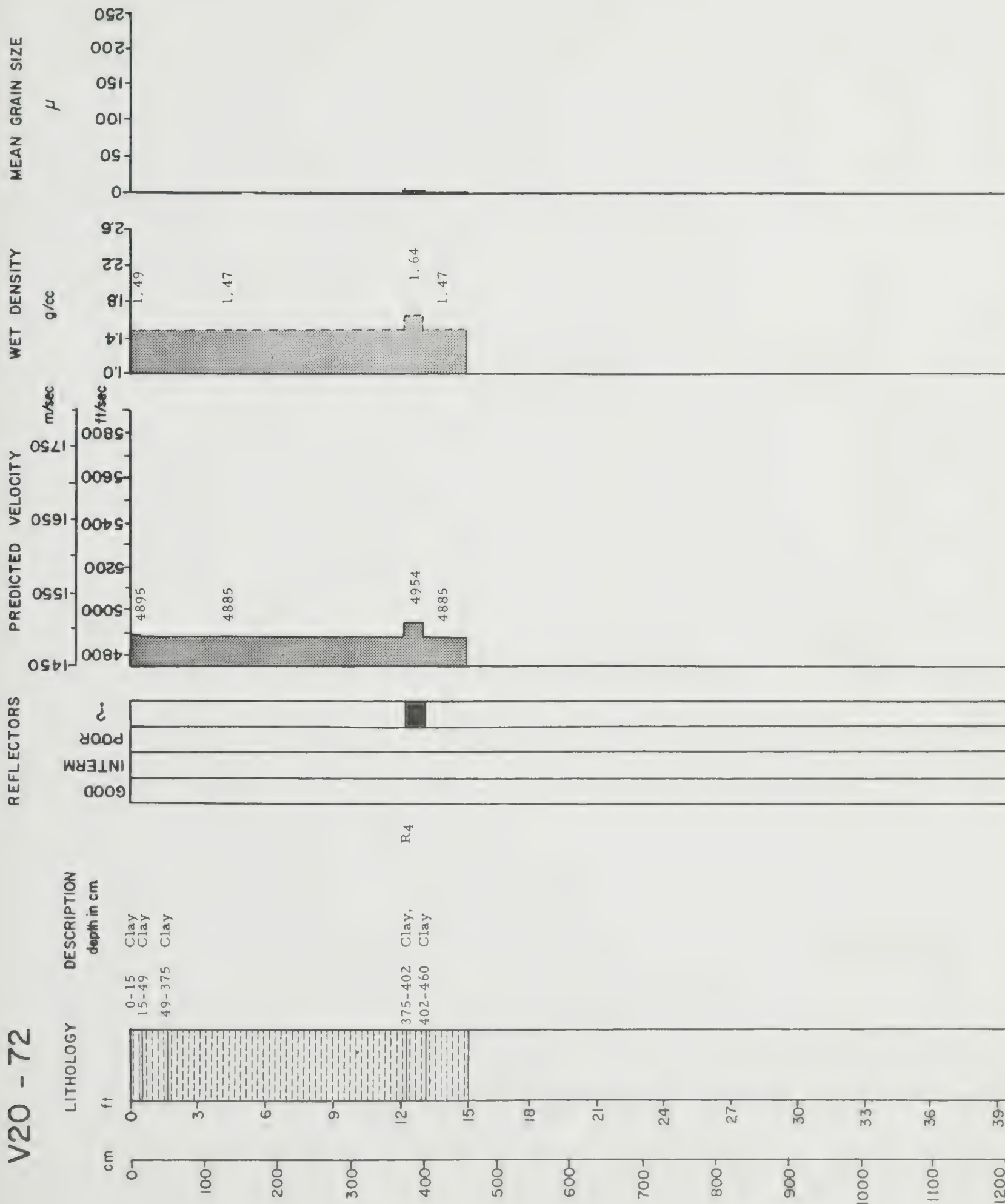




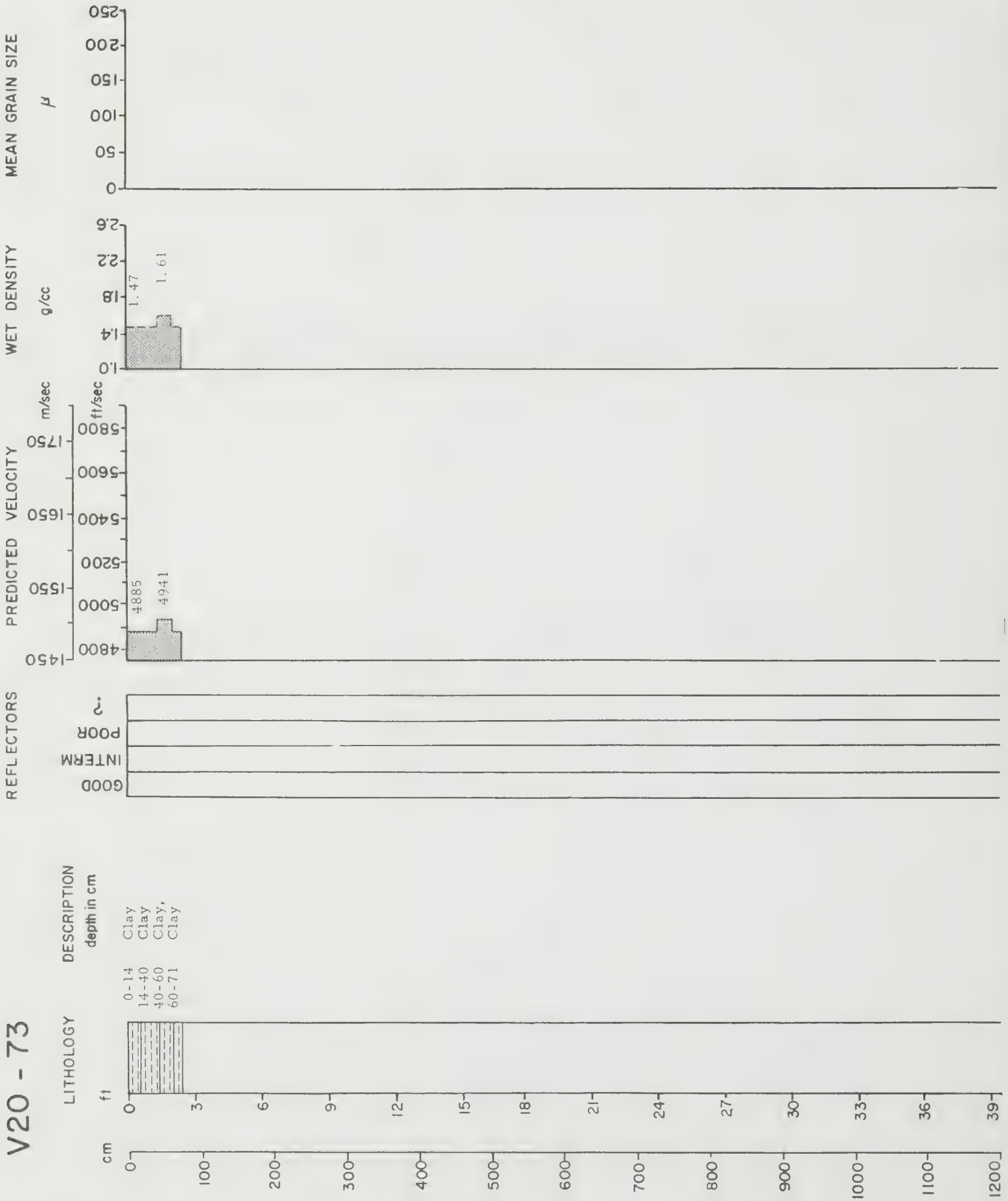
# V20 - 70





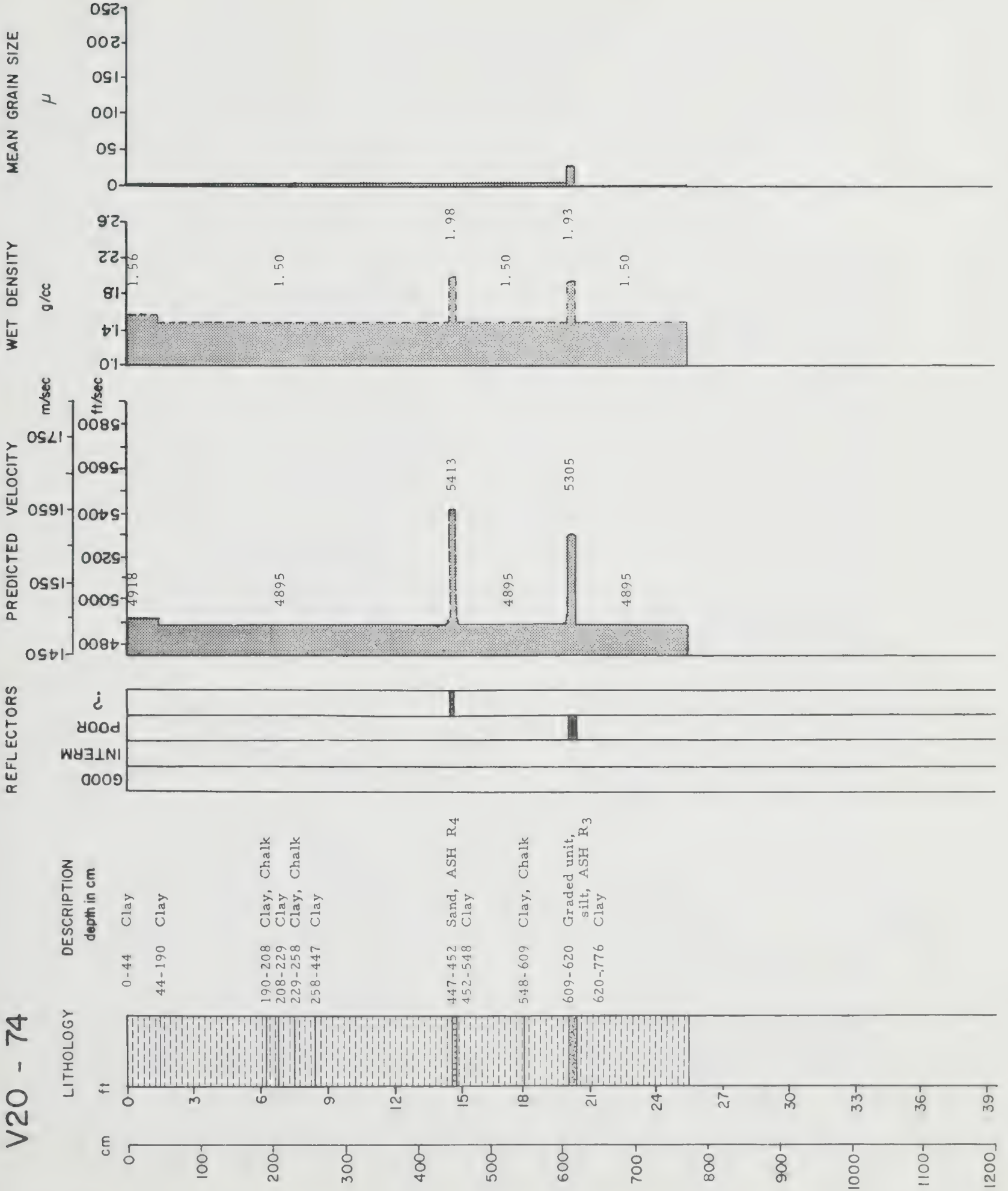


V20 - 73

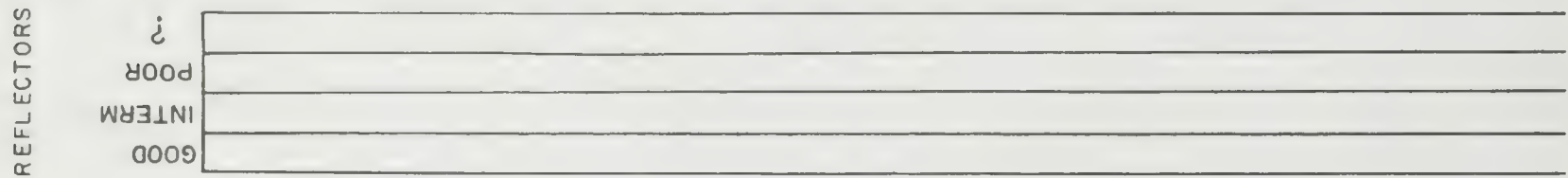
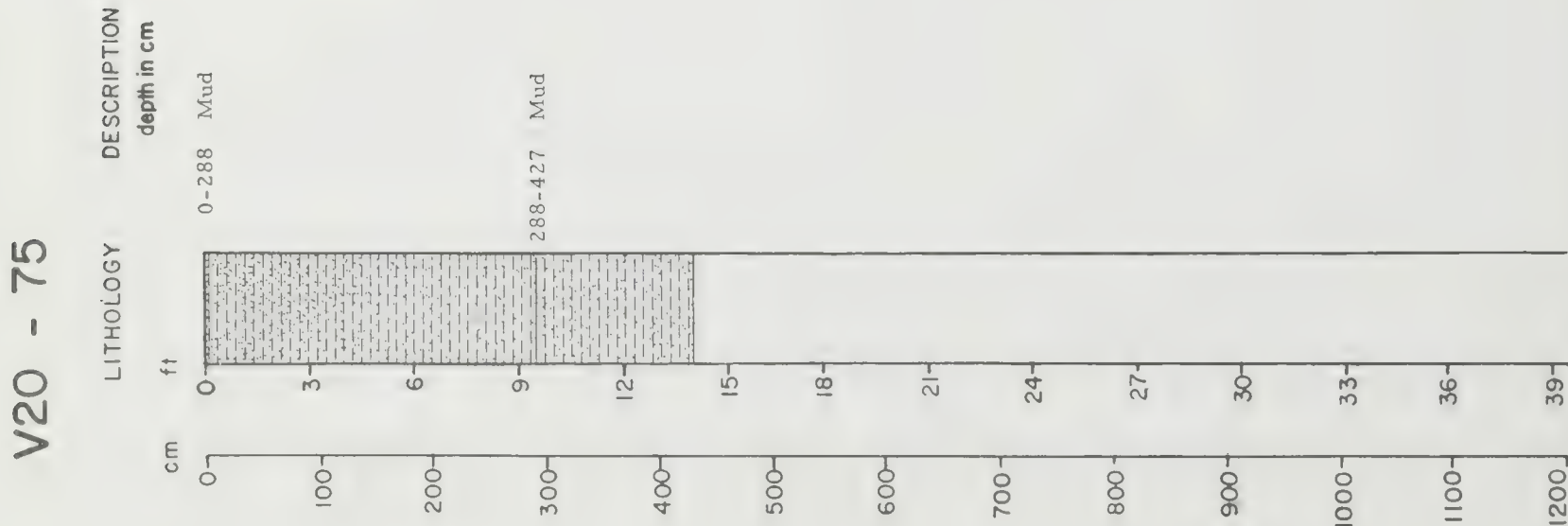


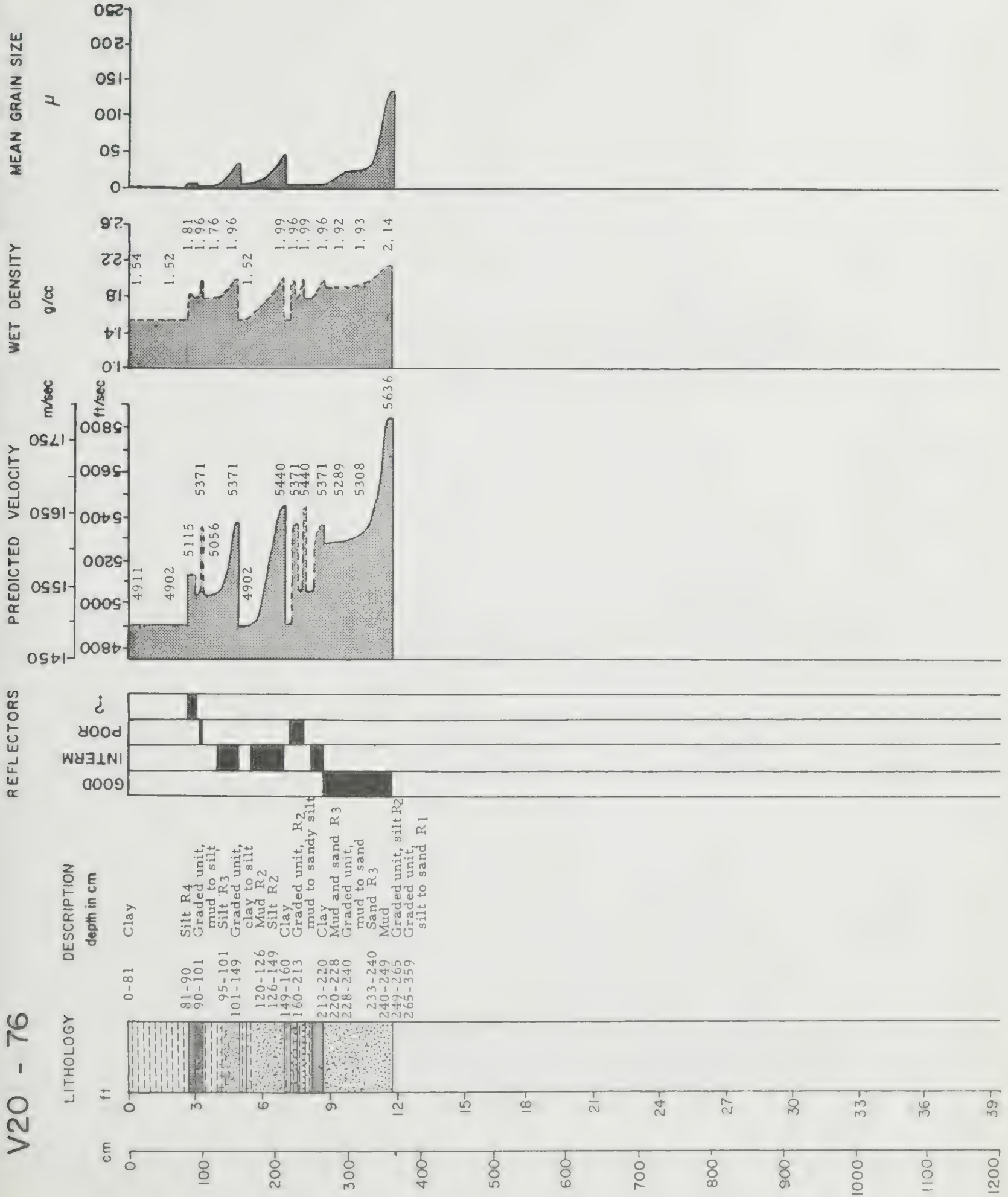


V20 - 74

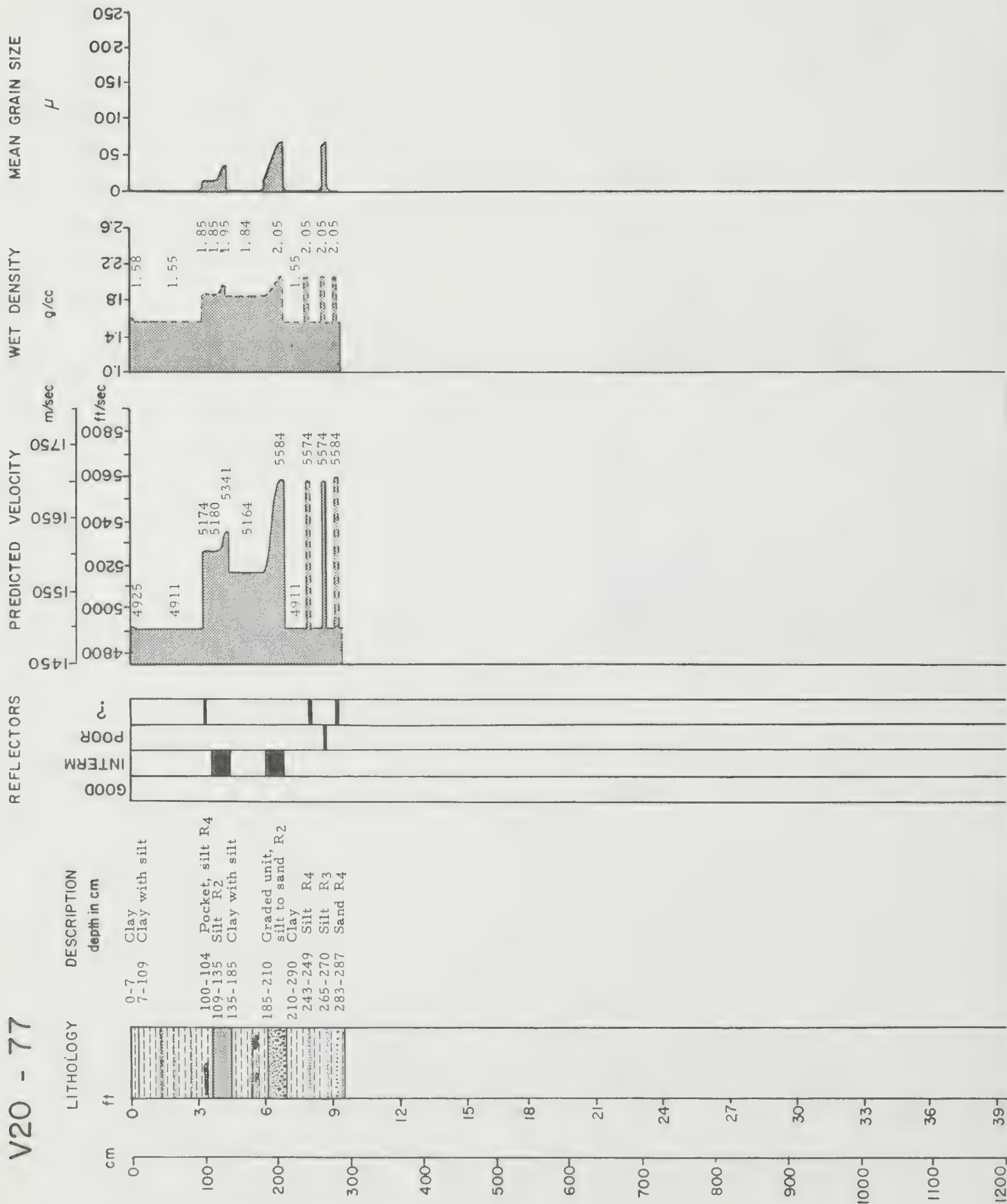


# V20 - 75



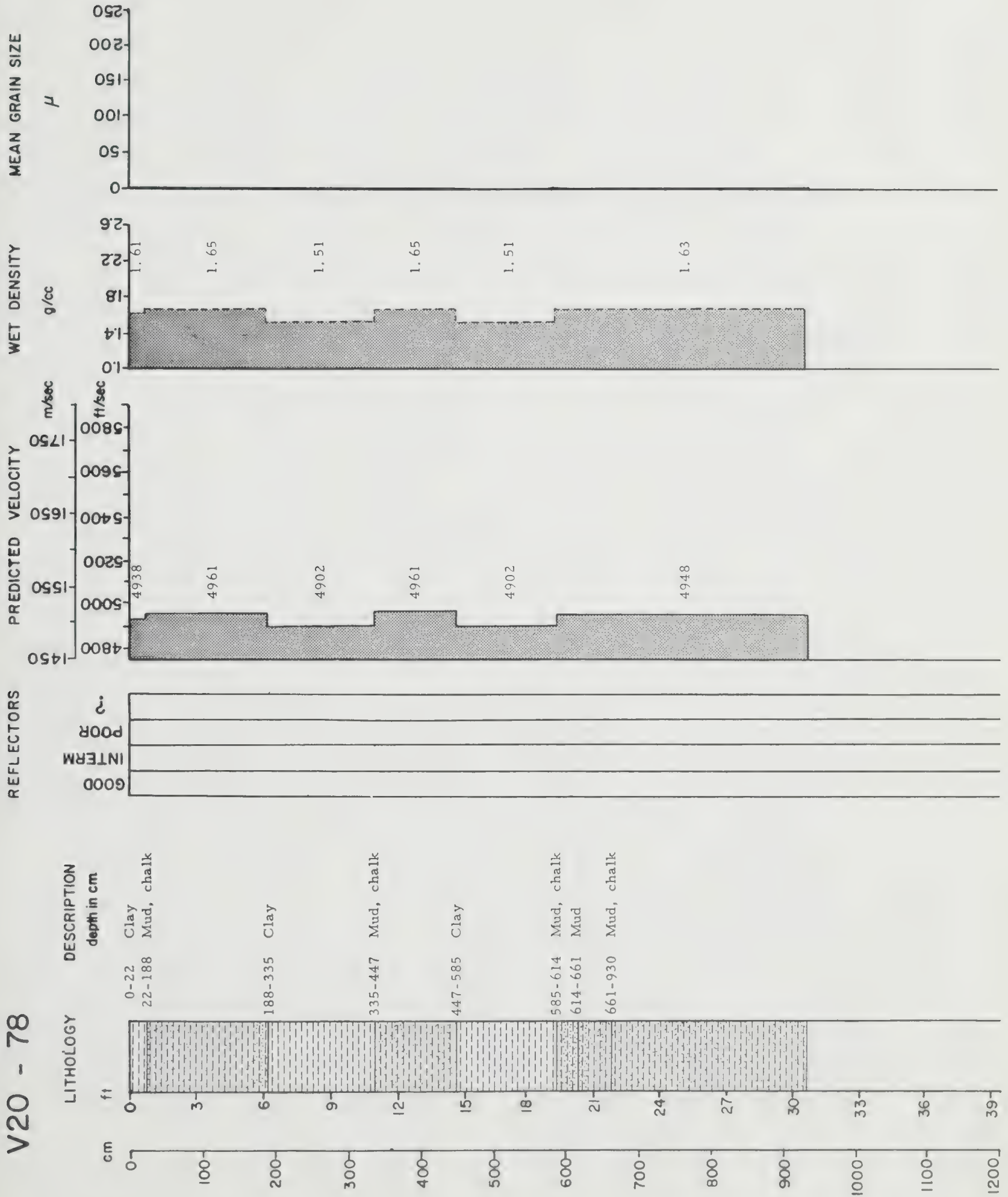


V20 - 77

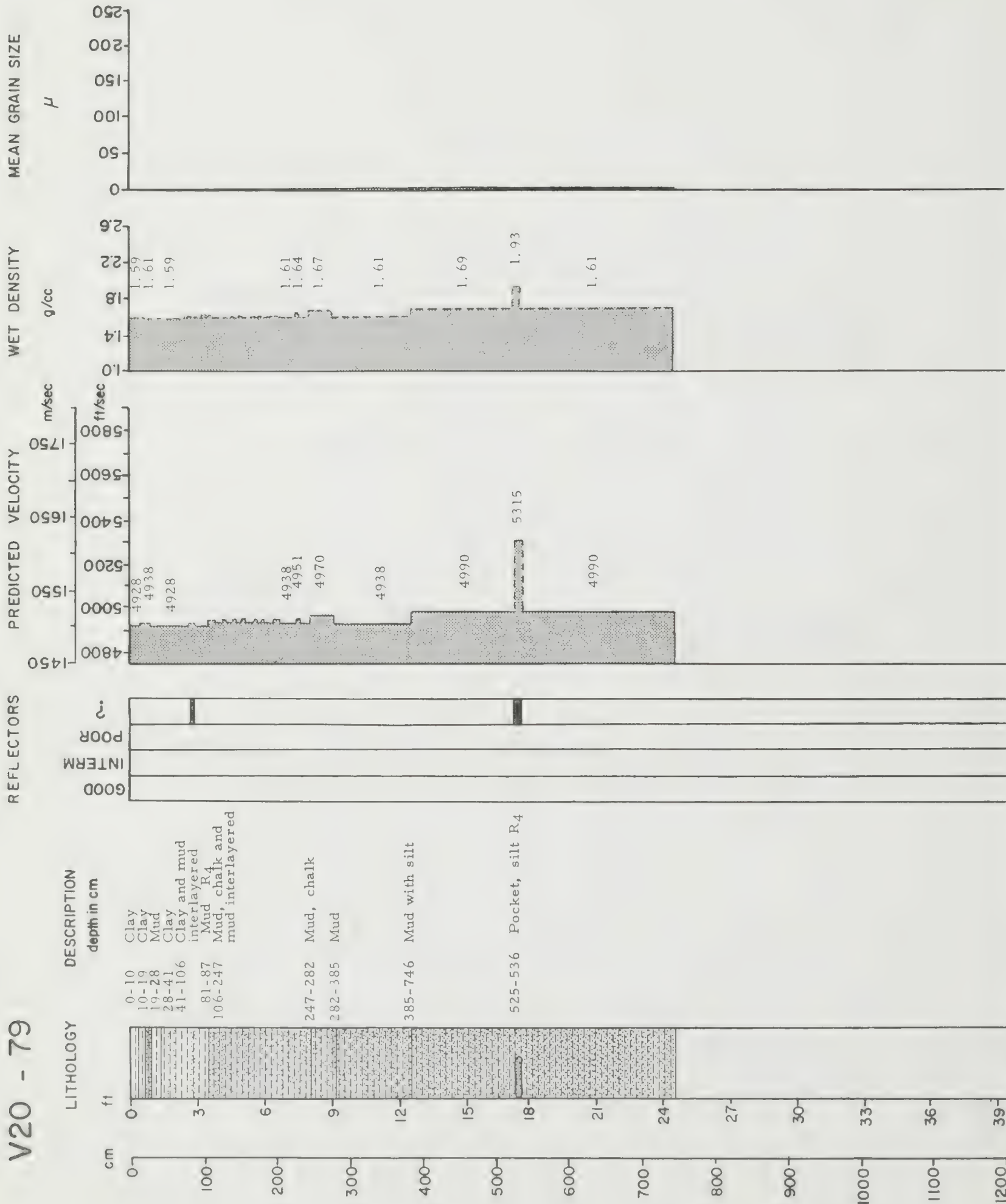




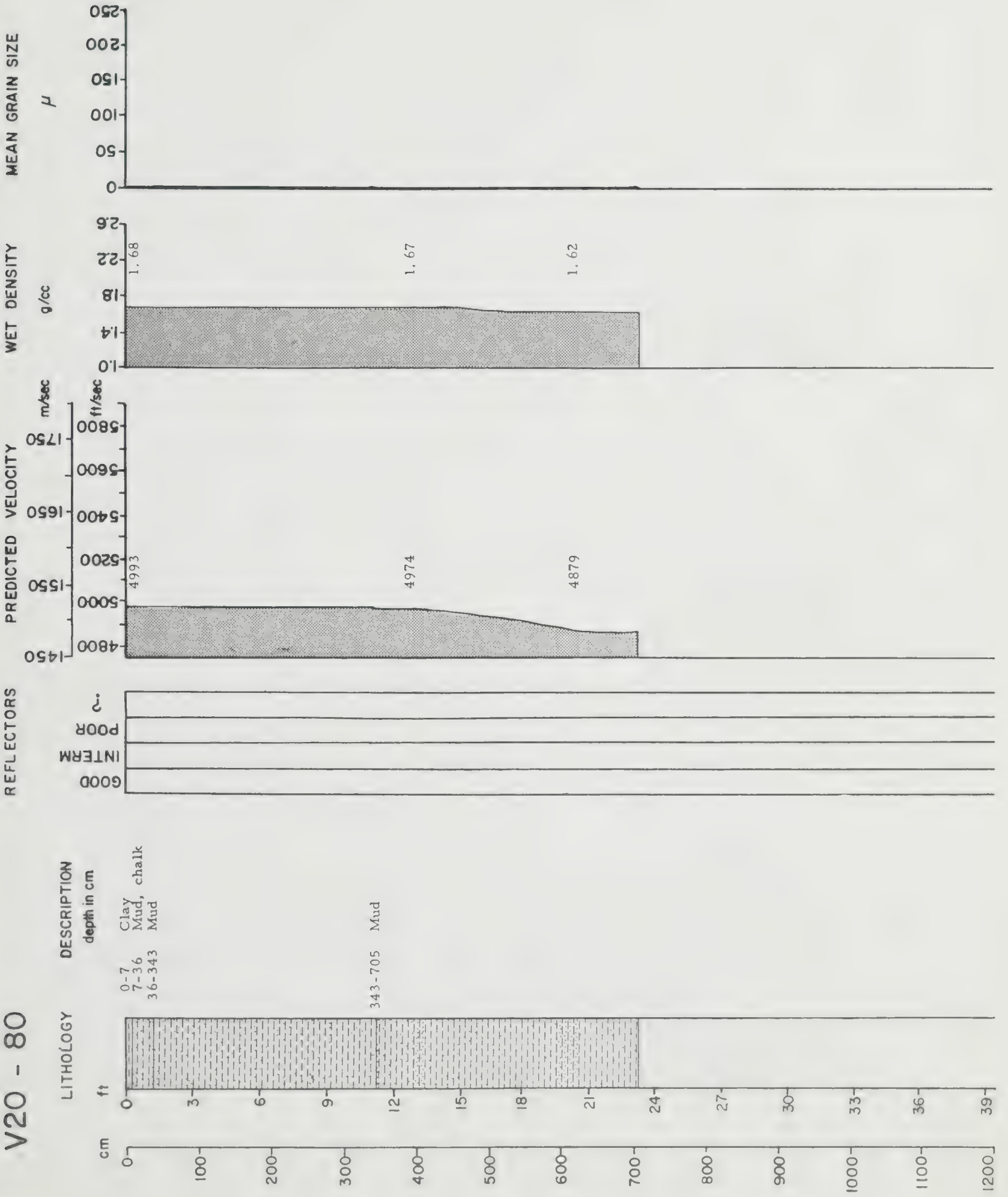
V20 - 78



V20 - 79



V20 - 80

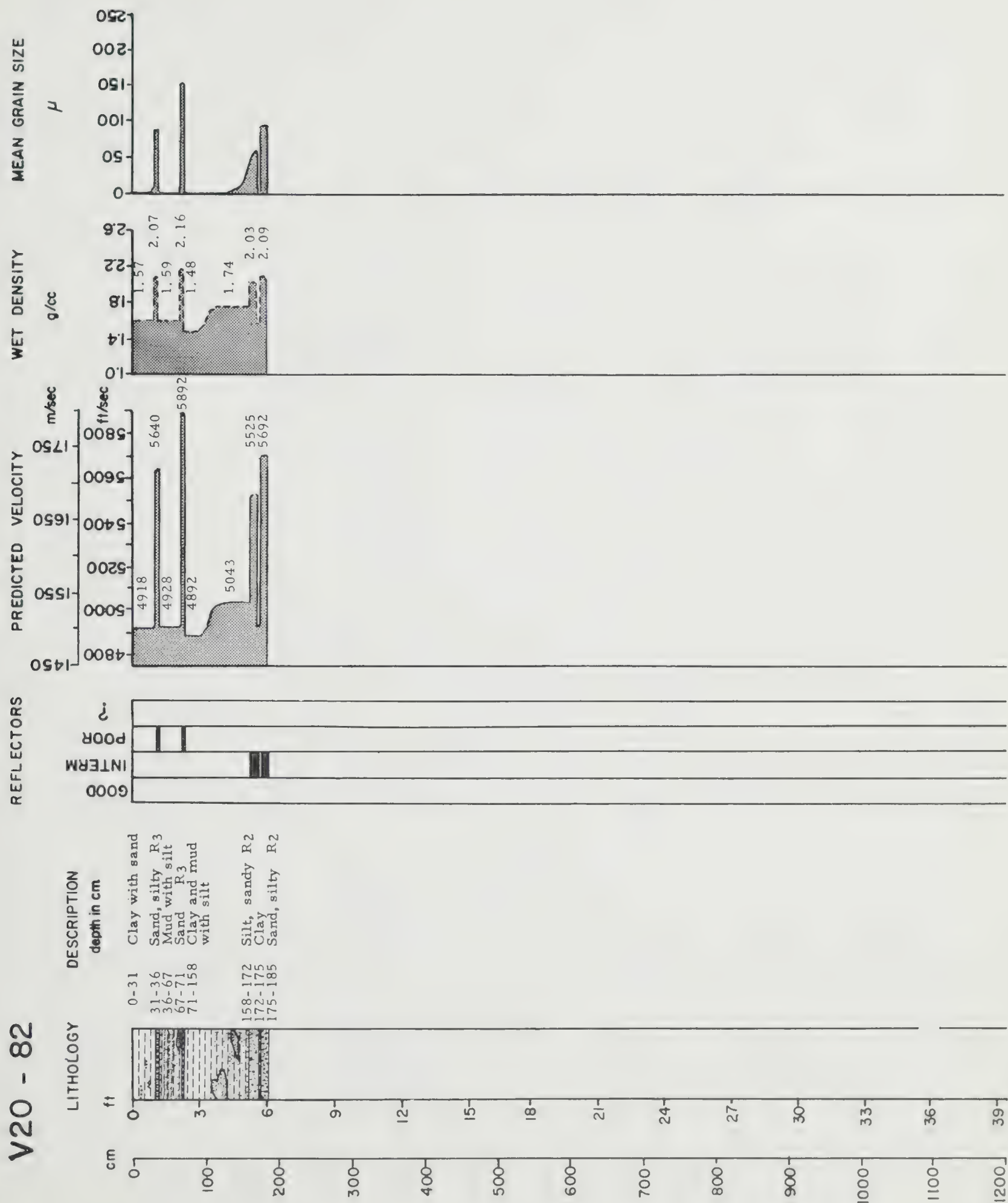


V20 - 81





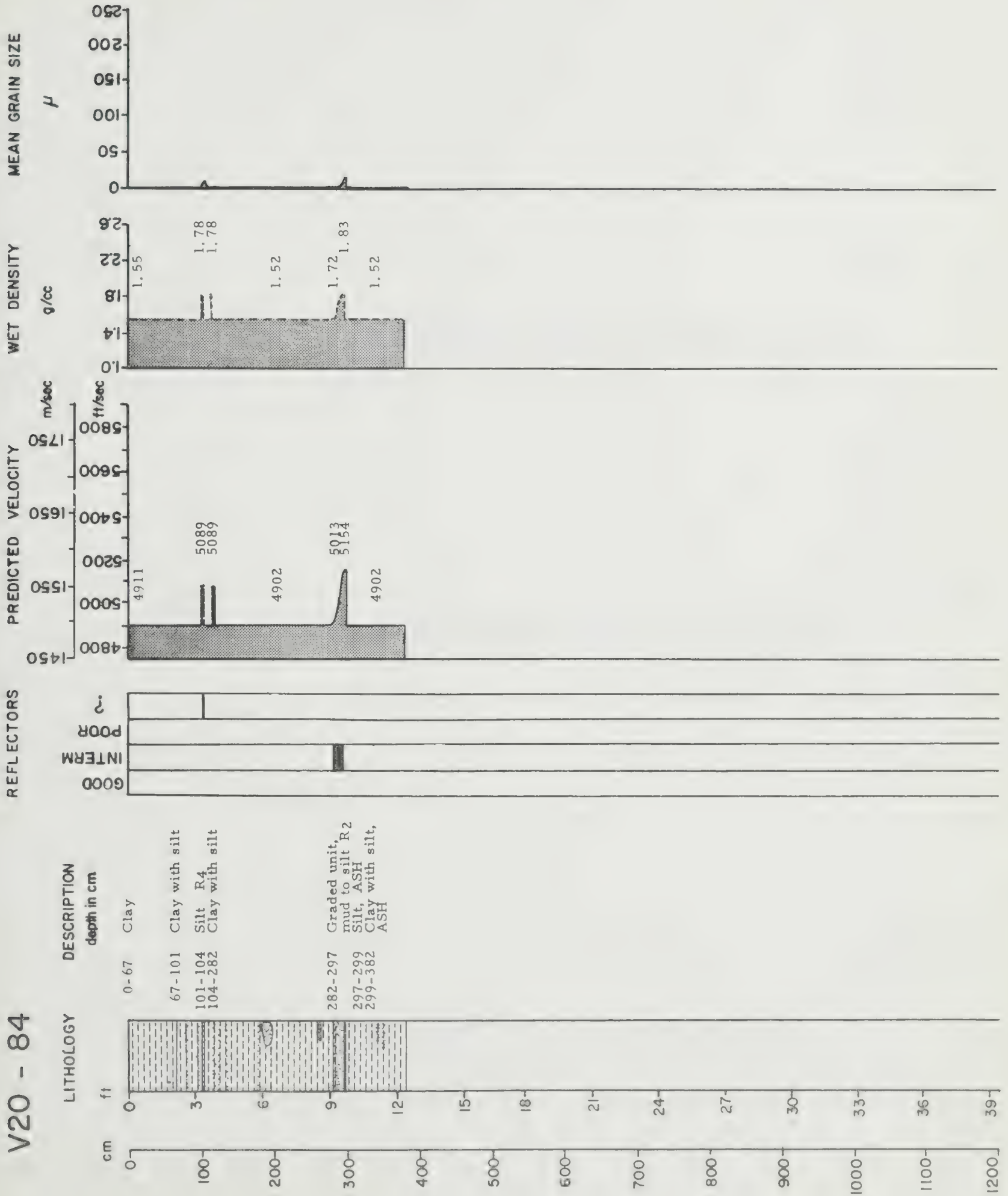
V20 - 82

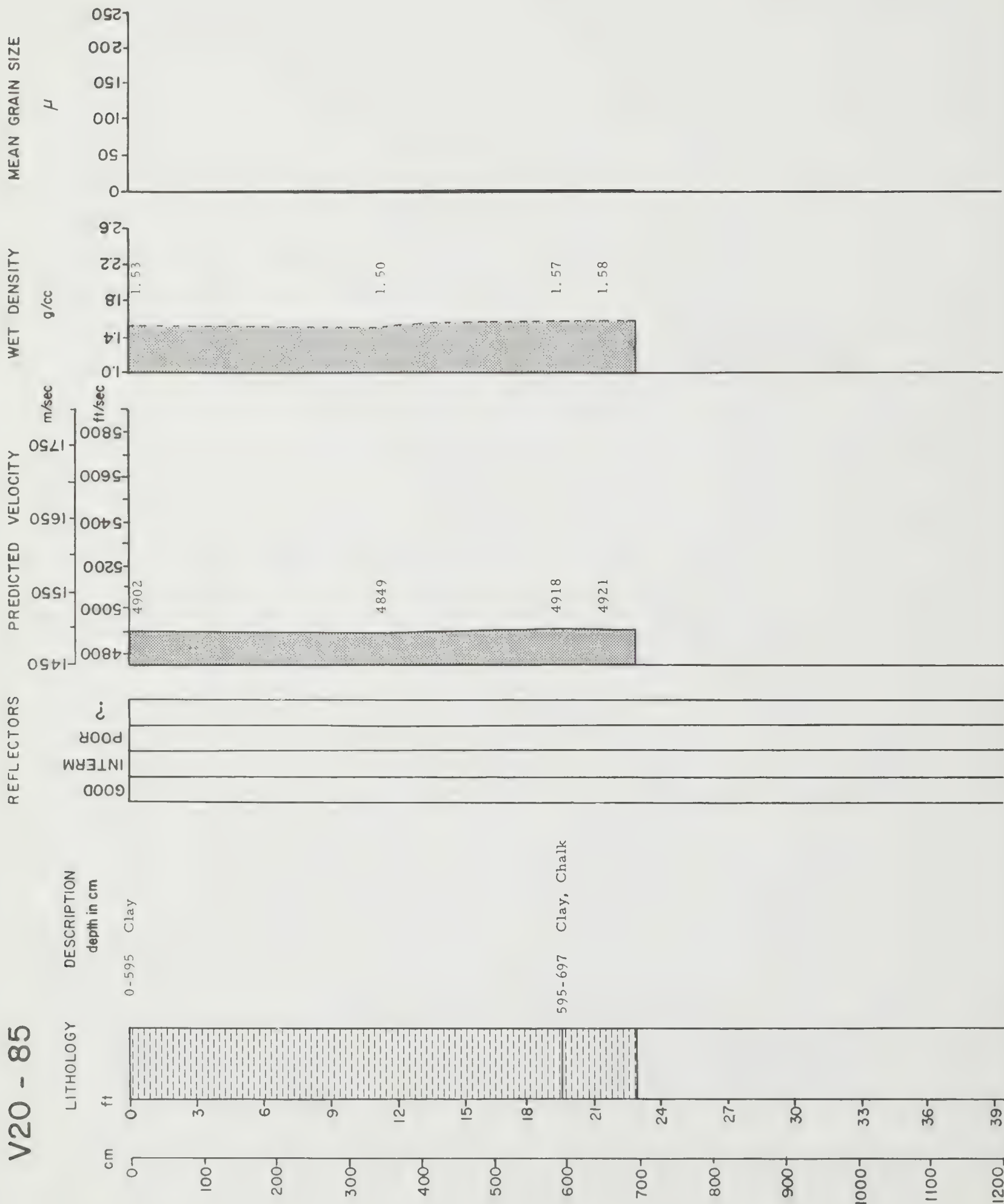


V20 - 83



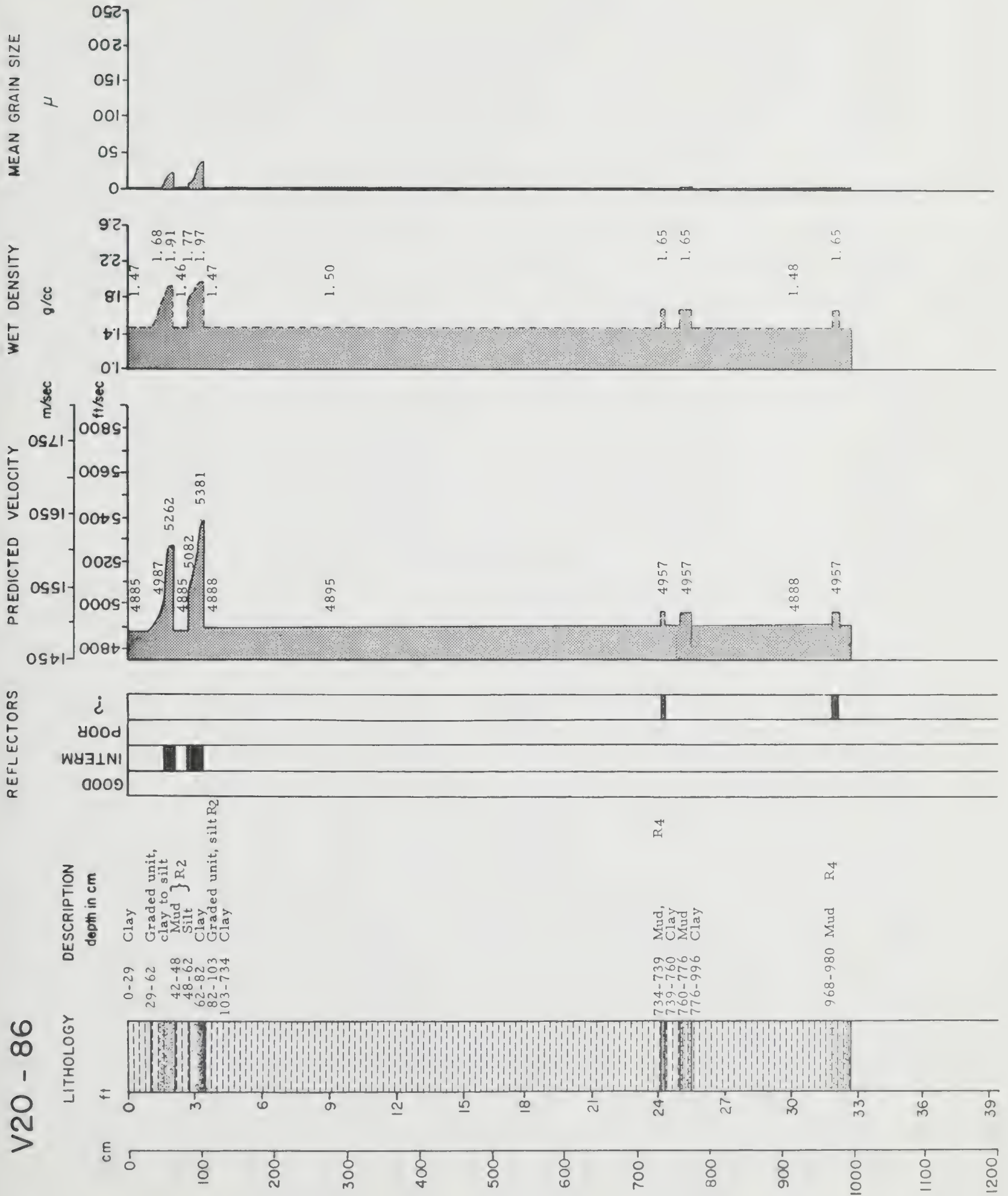
V20 - 84



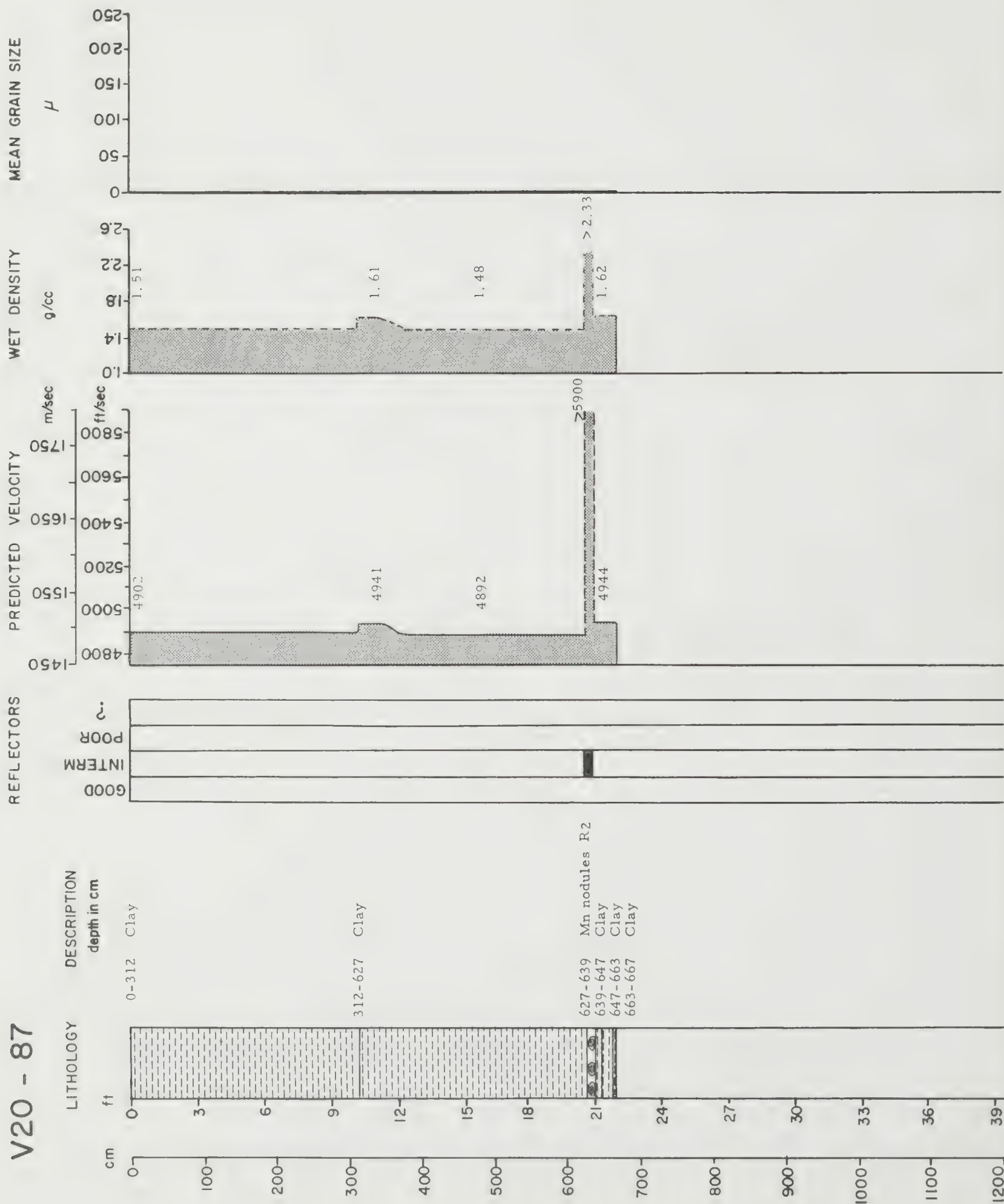




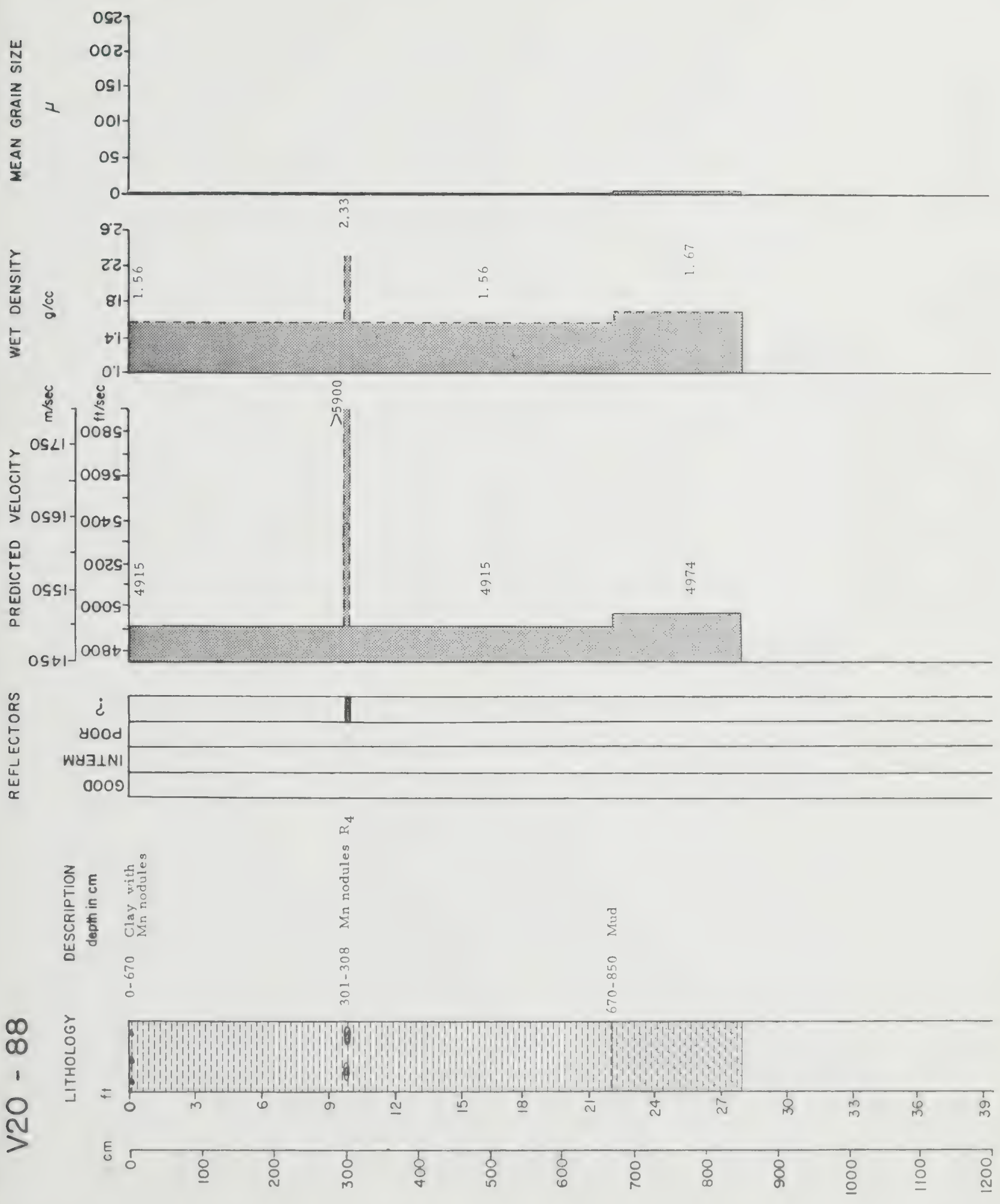
V20 - 86



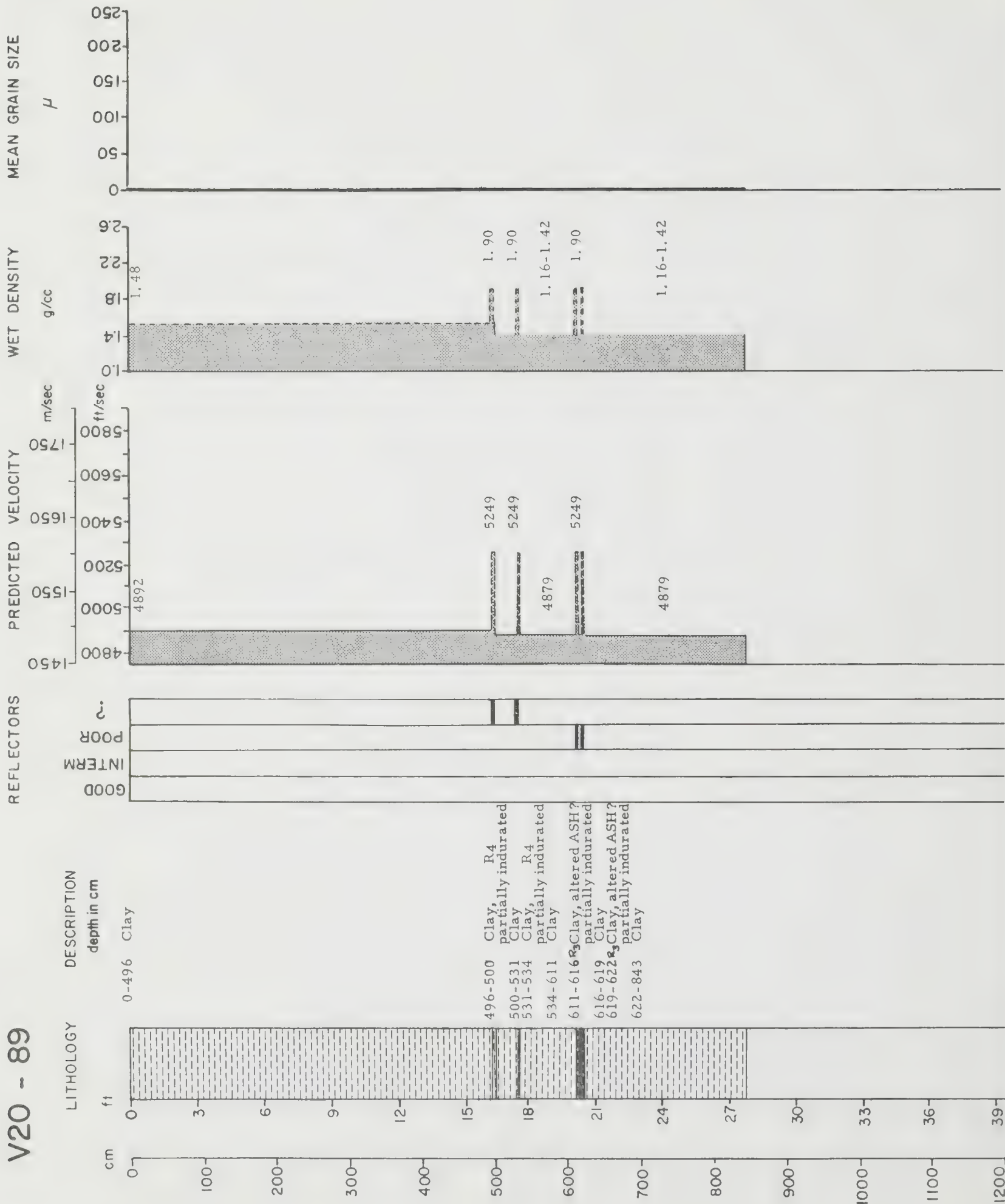
# V20 - 87



V20 - 88

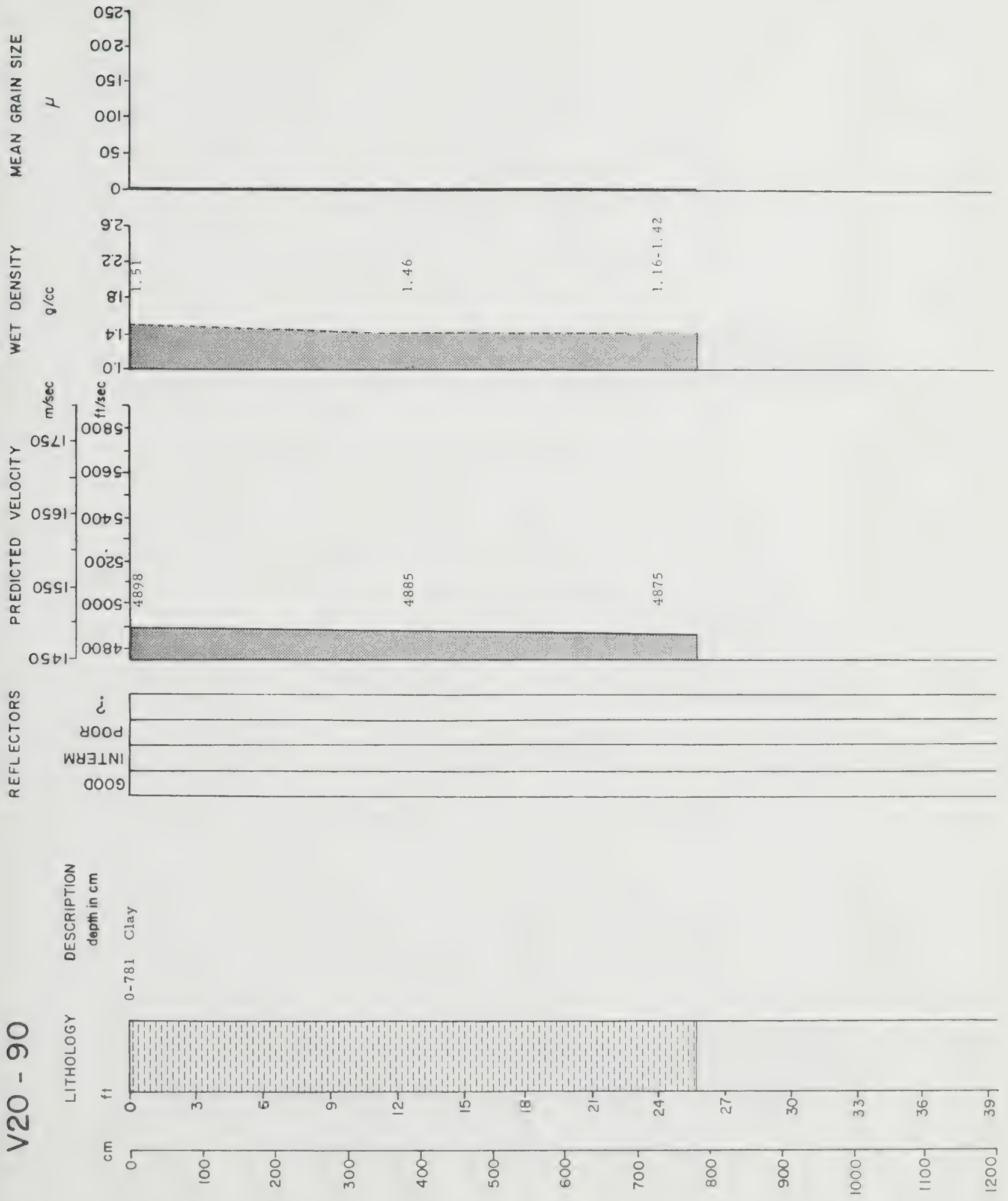


V20 - 89

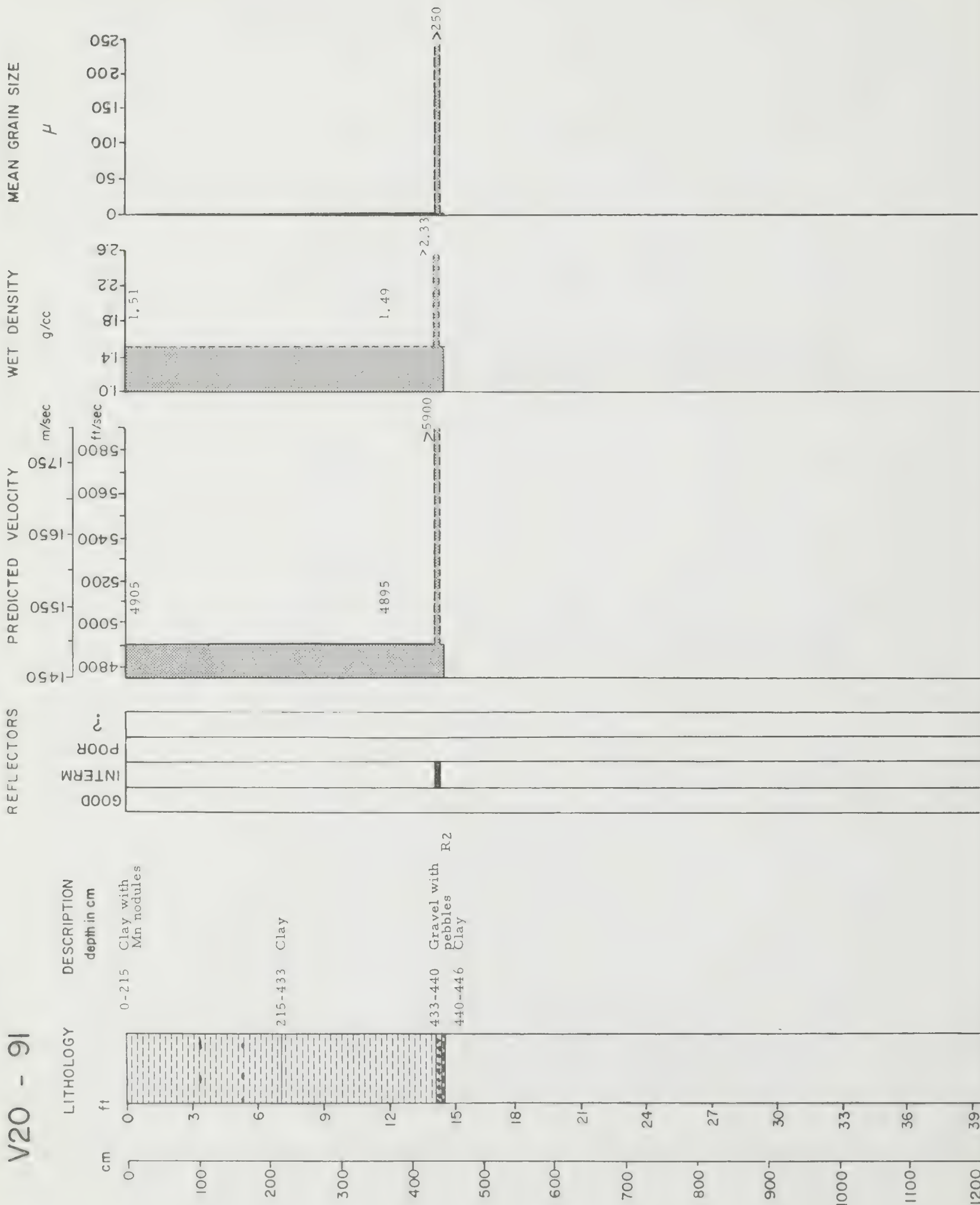




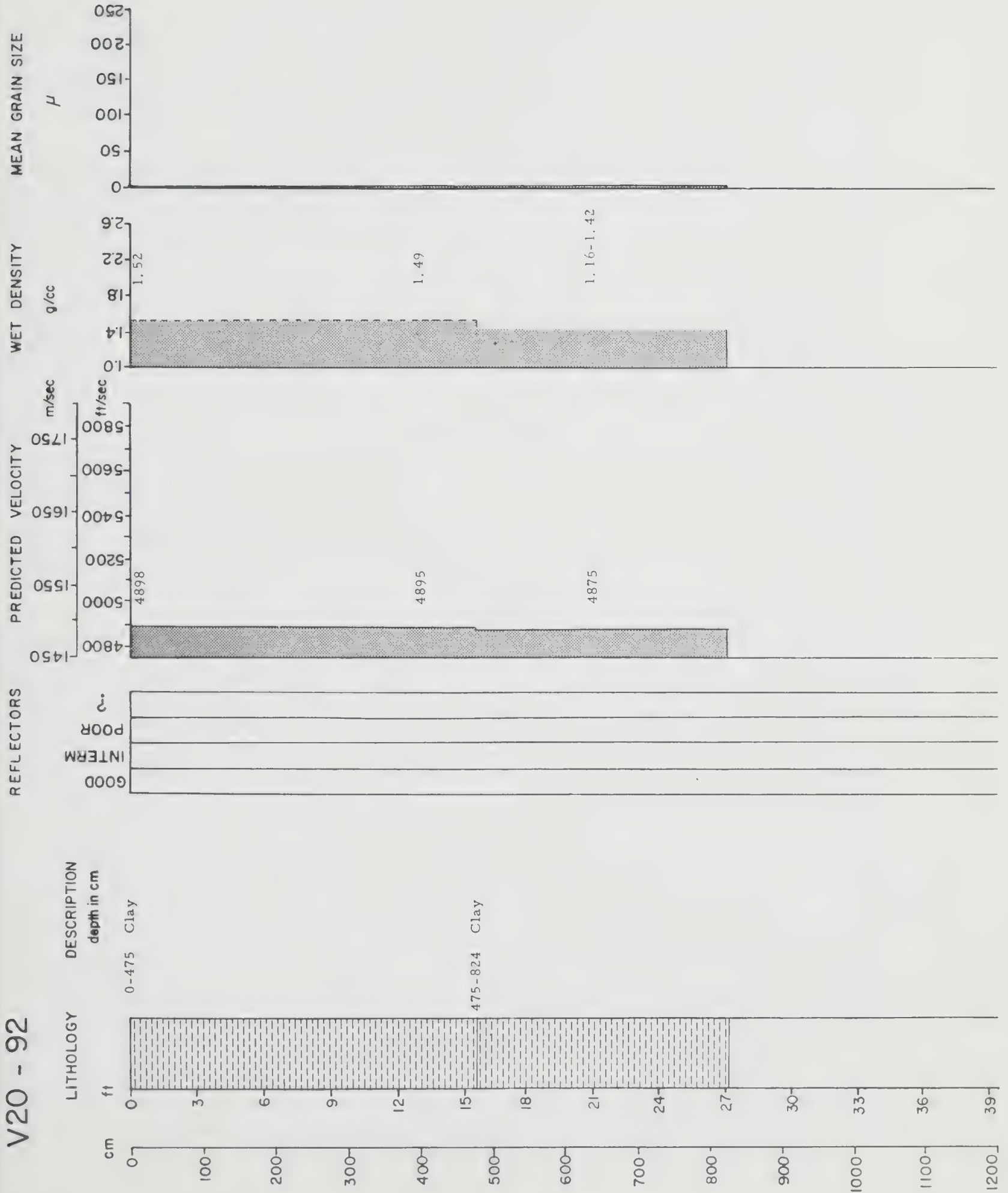
V20 - 90



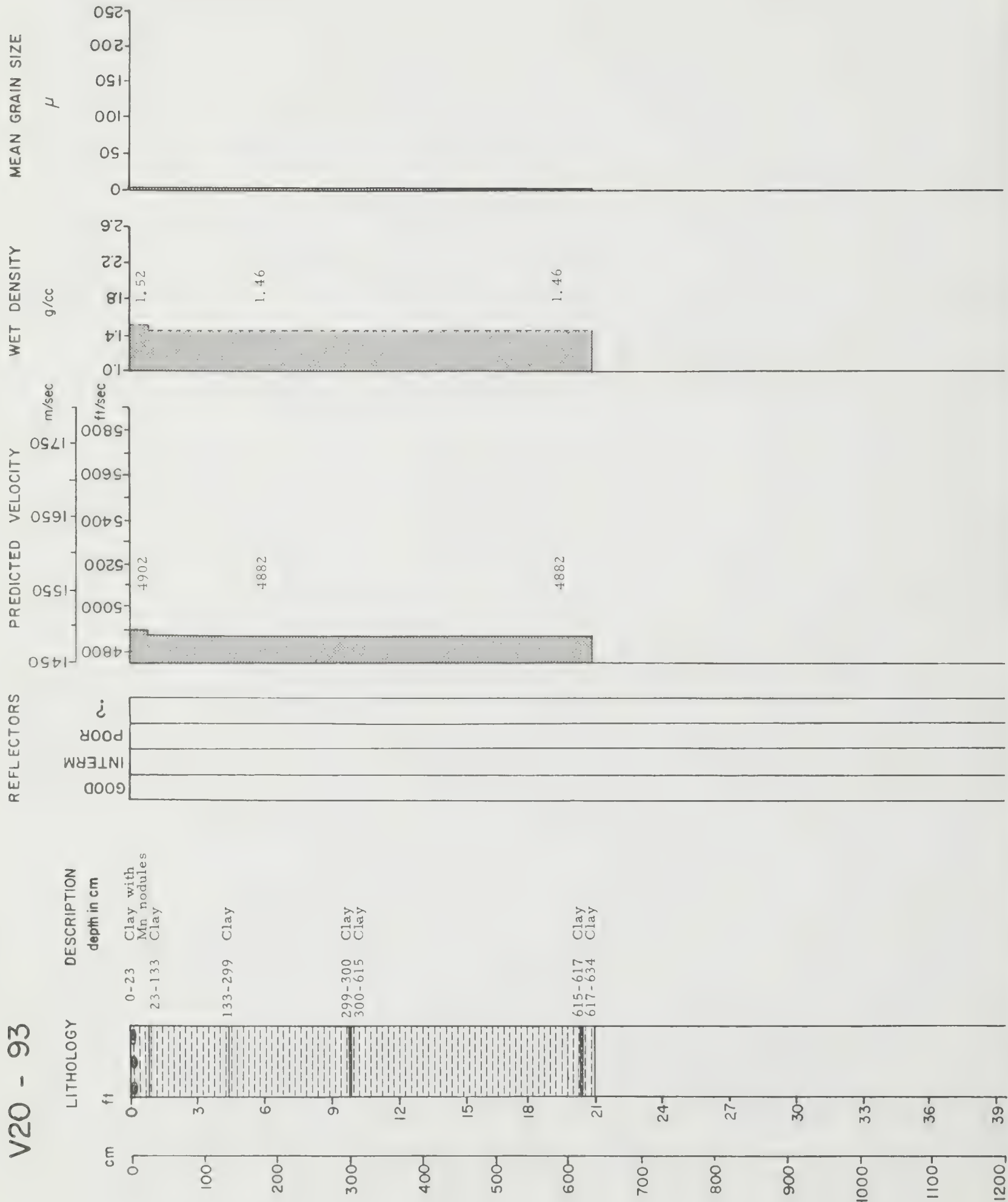
# V20 - 91



# V20 - 92

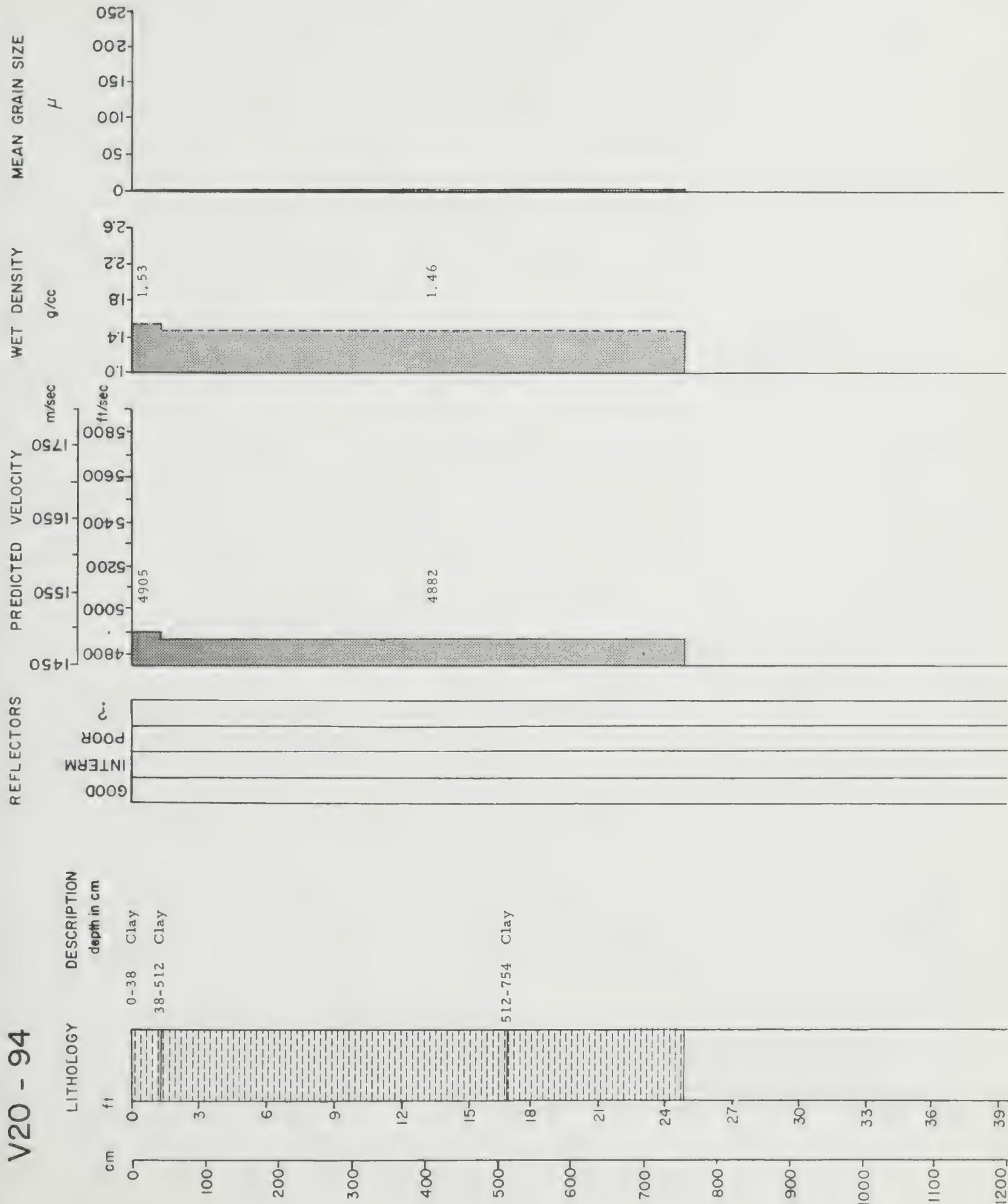


# V20 - 93

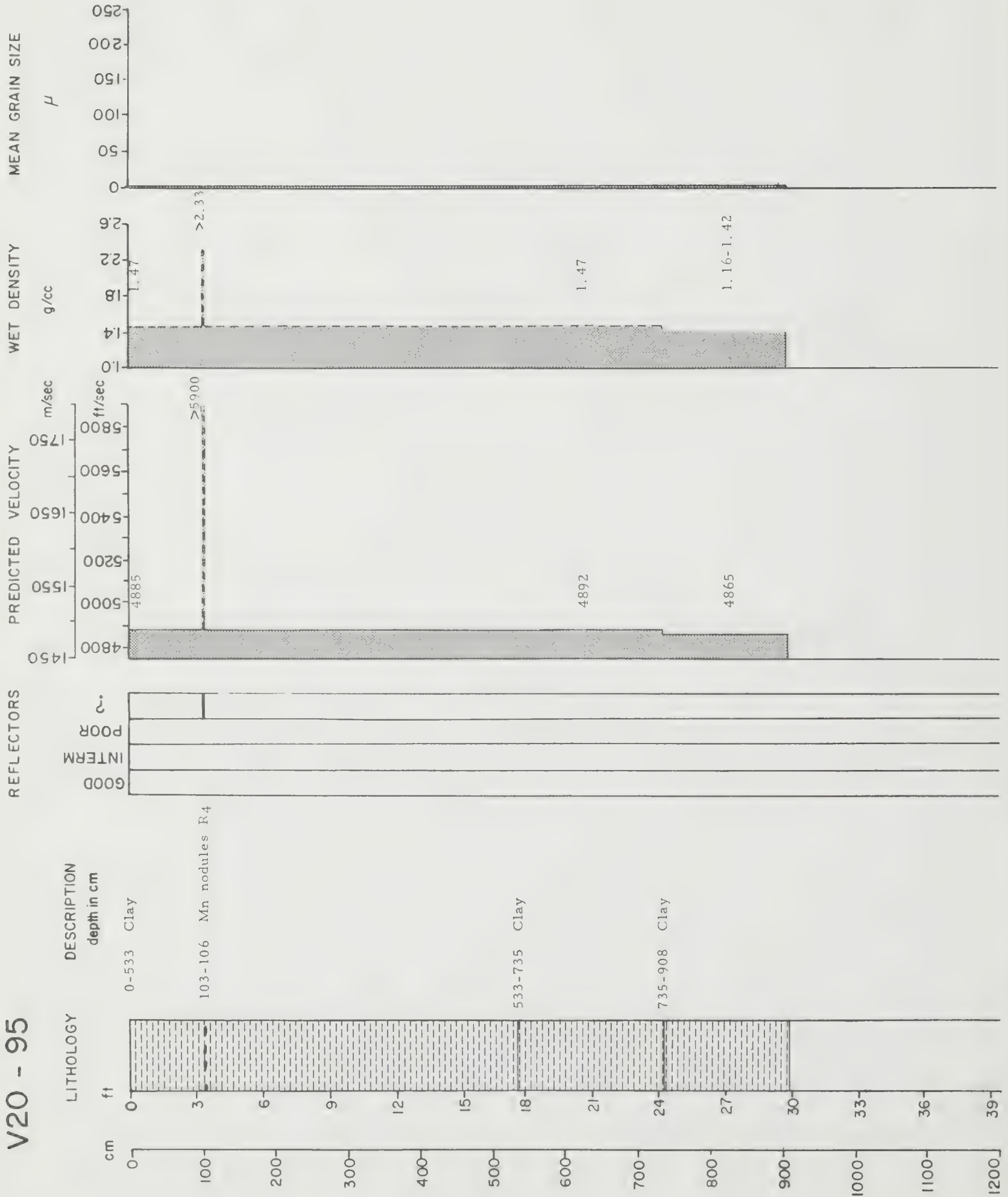




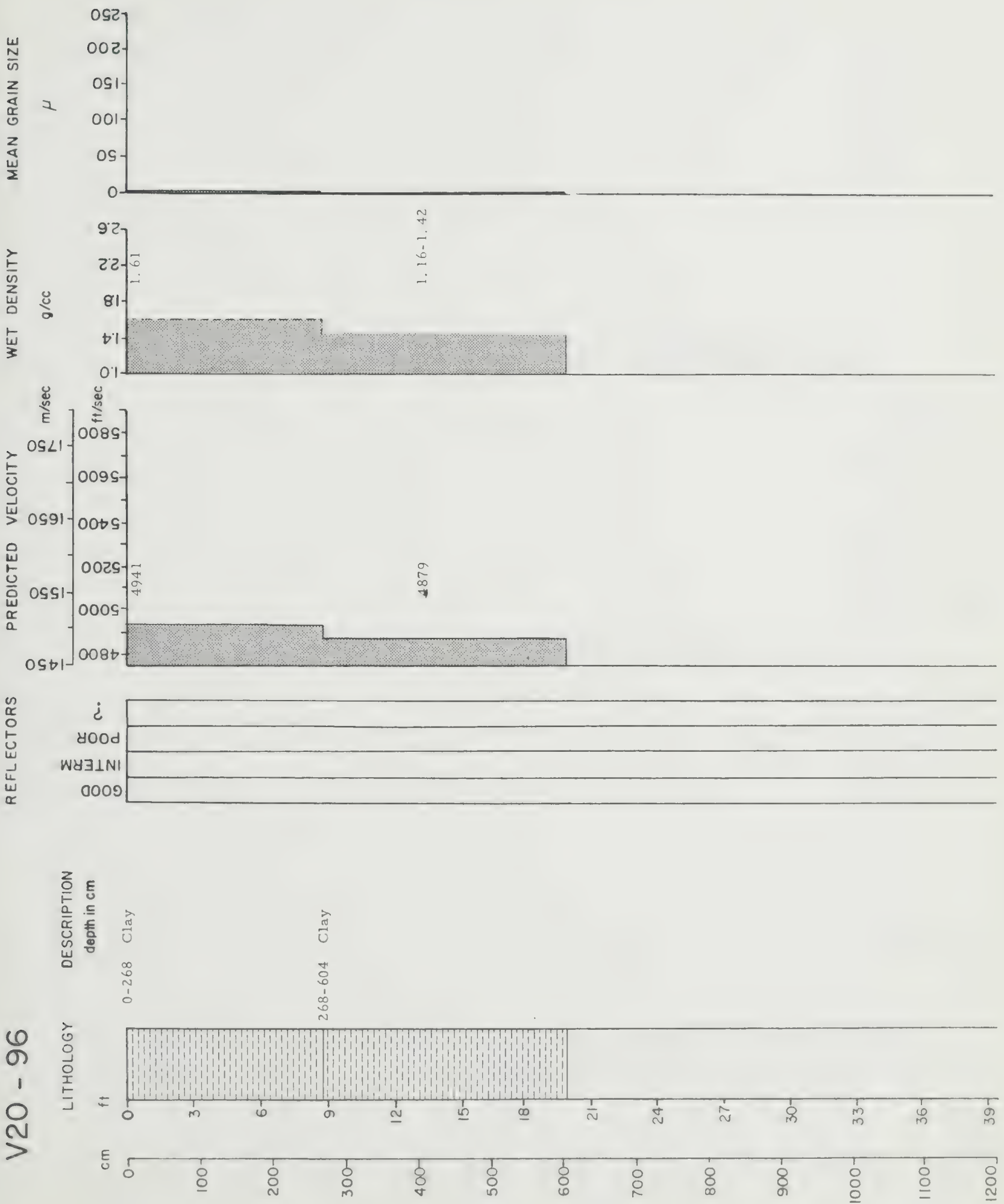
# V20 - 94



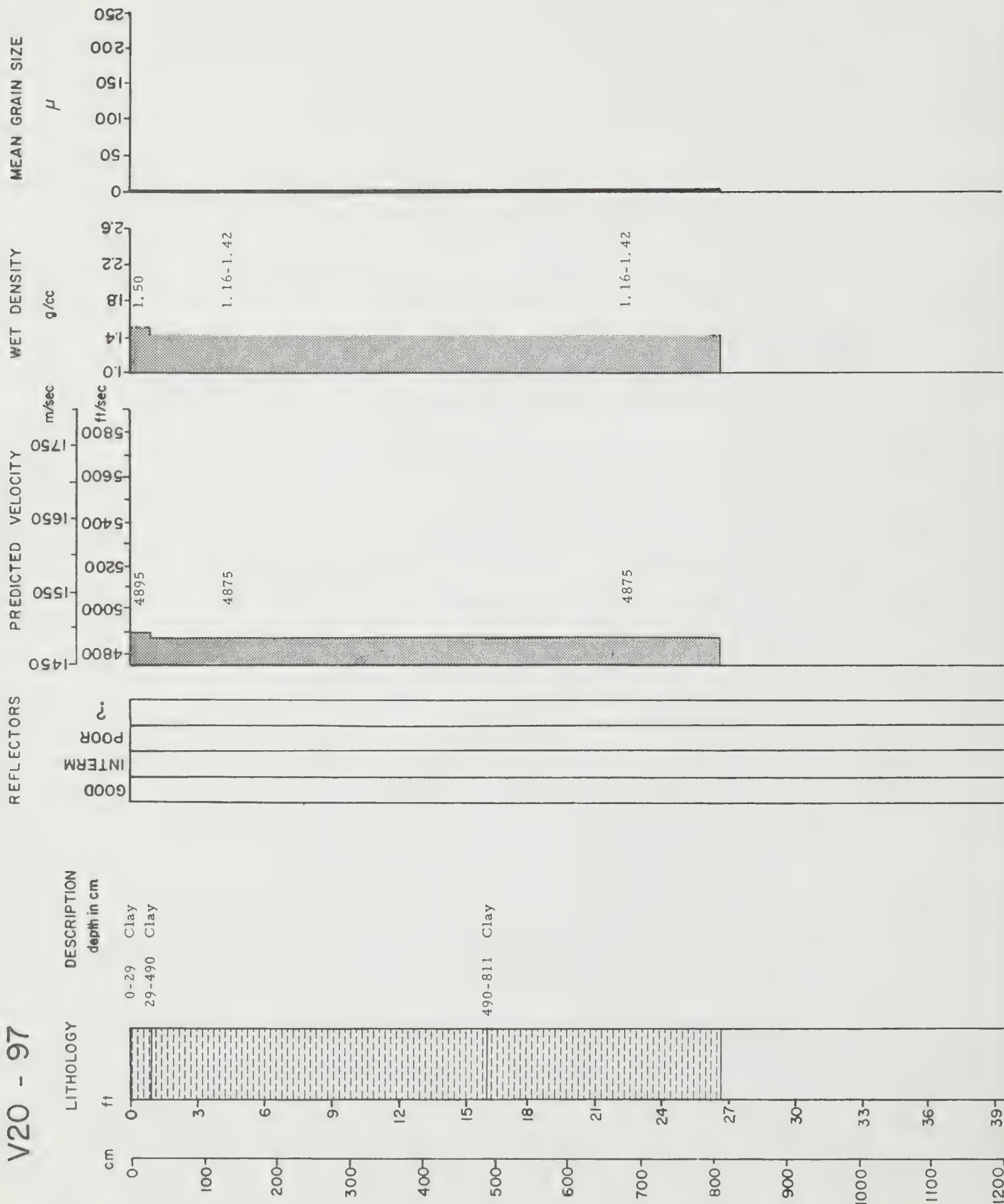
V20 - 95



# V20 - 96

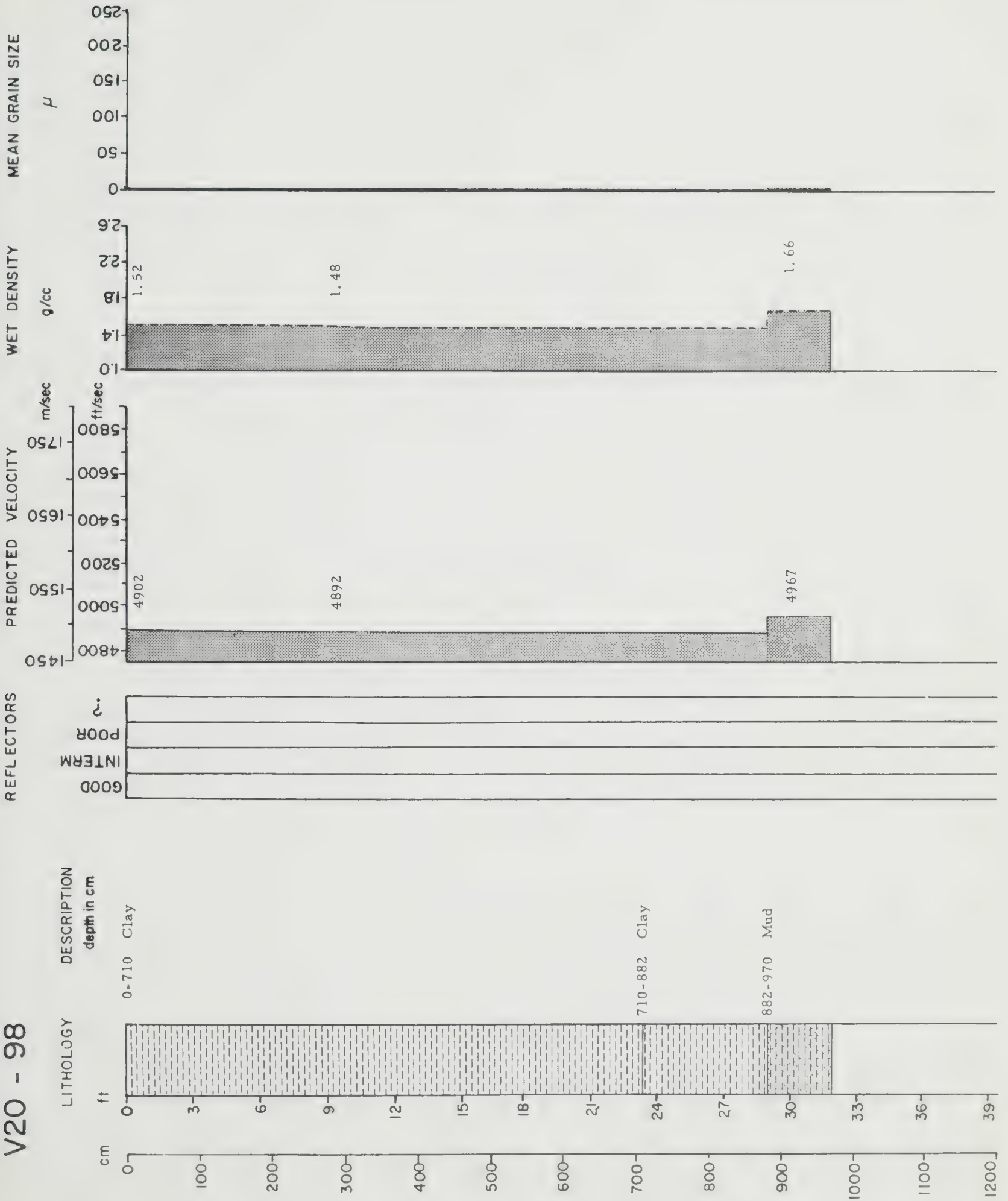


V20 - 97





# V20 - 98



V20 - 99

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

DESCRIPTION

LITHOLOGY

depth in cm

ft

cm

GOOD  
INTERM  
POOR  
?

$\mu$

g/cc

m/sec  
ft/sec

250  
200  
150  
100  
50  
0

2.6  
2.2  
1.8  
1.4  
1.0

1750  
1500  
1250  
1000  
750  
500  
250  
0

1450  
1500  
1550  
1600  
1650  
1700  
1750  
1800

1.90  
1.51  
1.65  
1.90  
1.79  
1.79  
1.51

5249  
4902  
4961  
5249  
5095  
5089  
4902

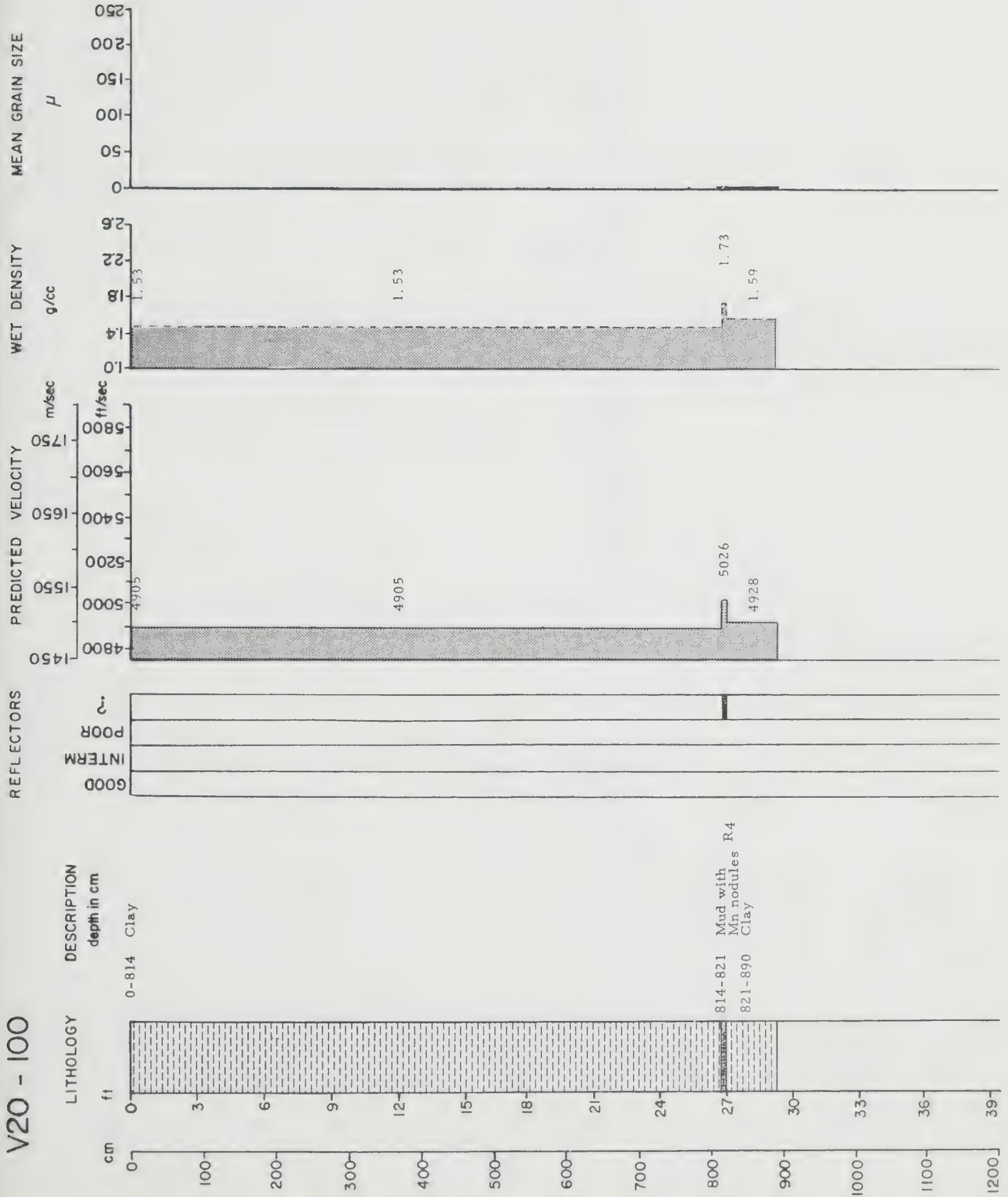
0-2  
2-17  
17-43  
43-45  
45-73  
73-84  
84-110  
110-135  
135-225  
225-228  
228-233  
233-234  
234-245

Clay  
Graded unit, silt R3  
Clay  
Silt  
Mud  
Graded unit, R3  
mud to silt  
Clay R2  
Silt  
Clay  
Silt  
Clay

0  
3  
6  
9  
12  
15  
18  
21  
24  
27  
30  
33  
36  
39

0  
100  
200  
300  
400  
500  
600  
700  
800  
900  
1000  
1100  
1200

# V20 - 100



V20 - 101

REFLECTORS

PREDICTED VELOCITY

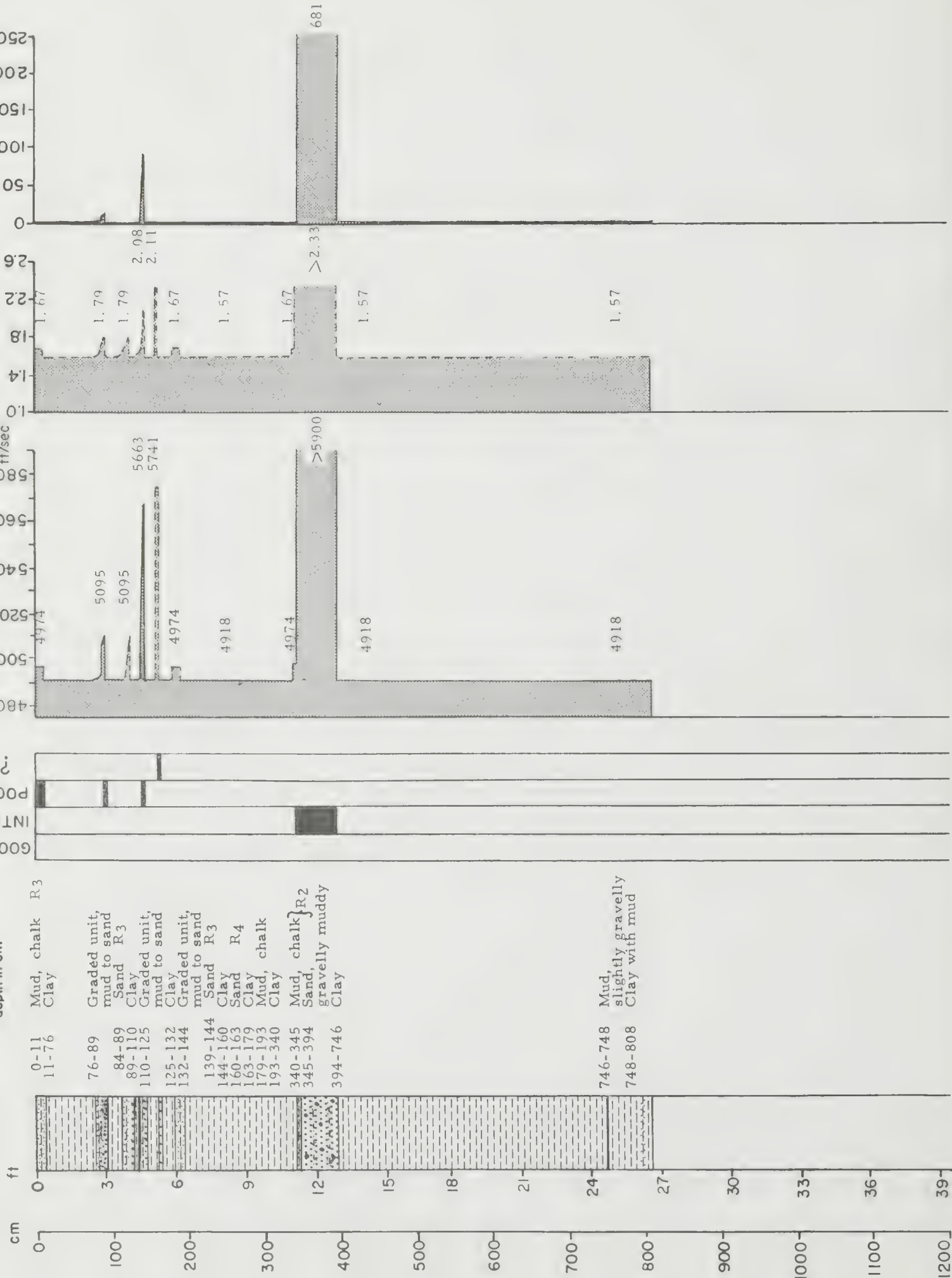
WET DENSITY

MEAN GRAIN SIZE

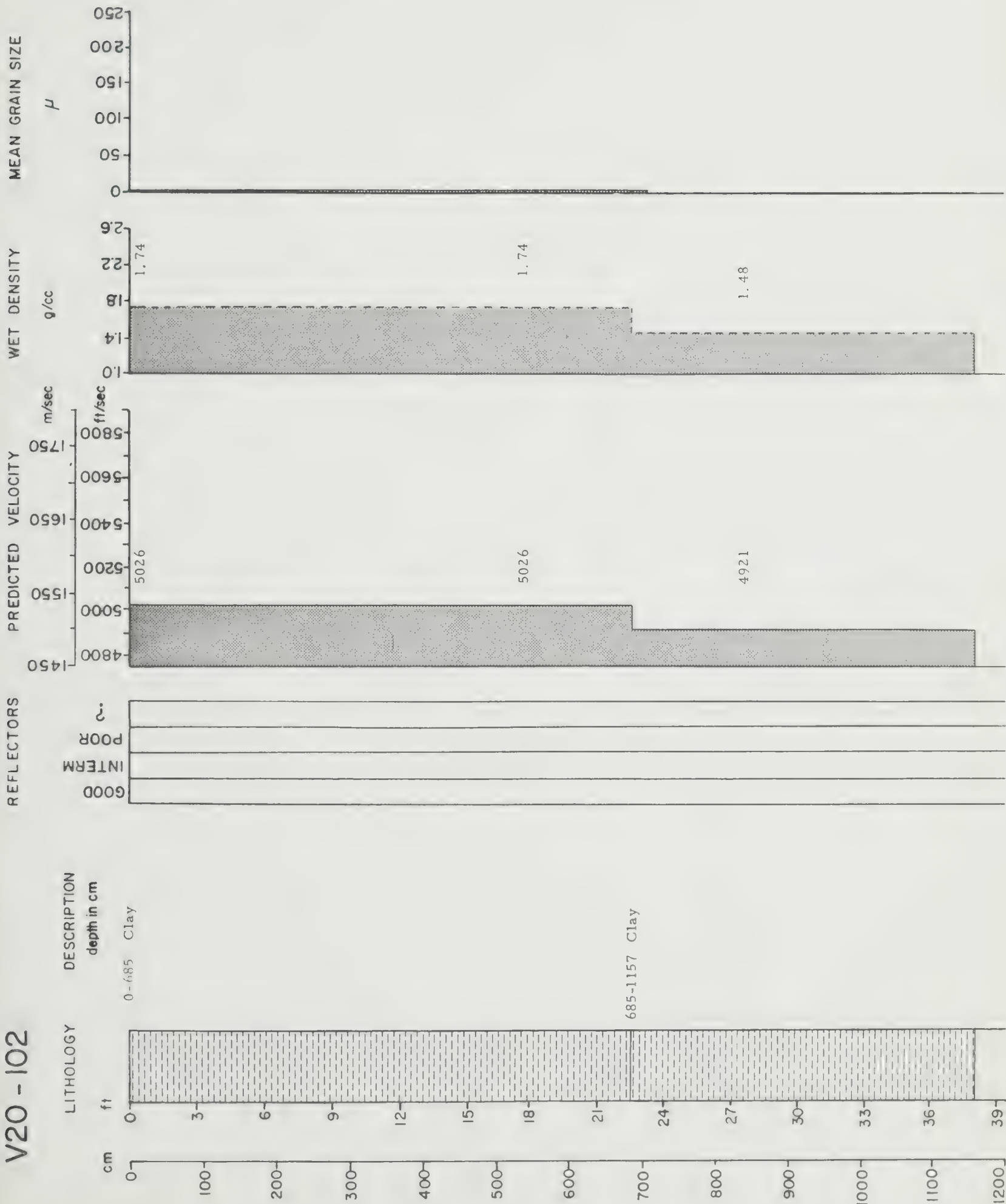
DESCRIPTION

depth in cm

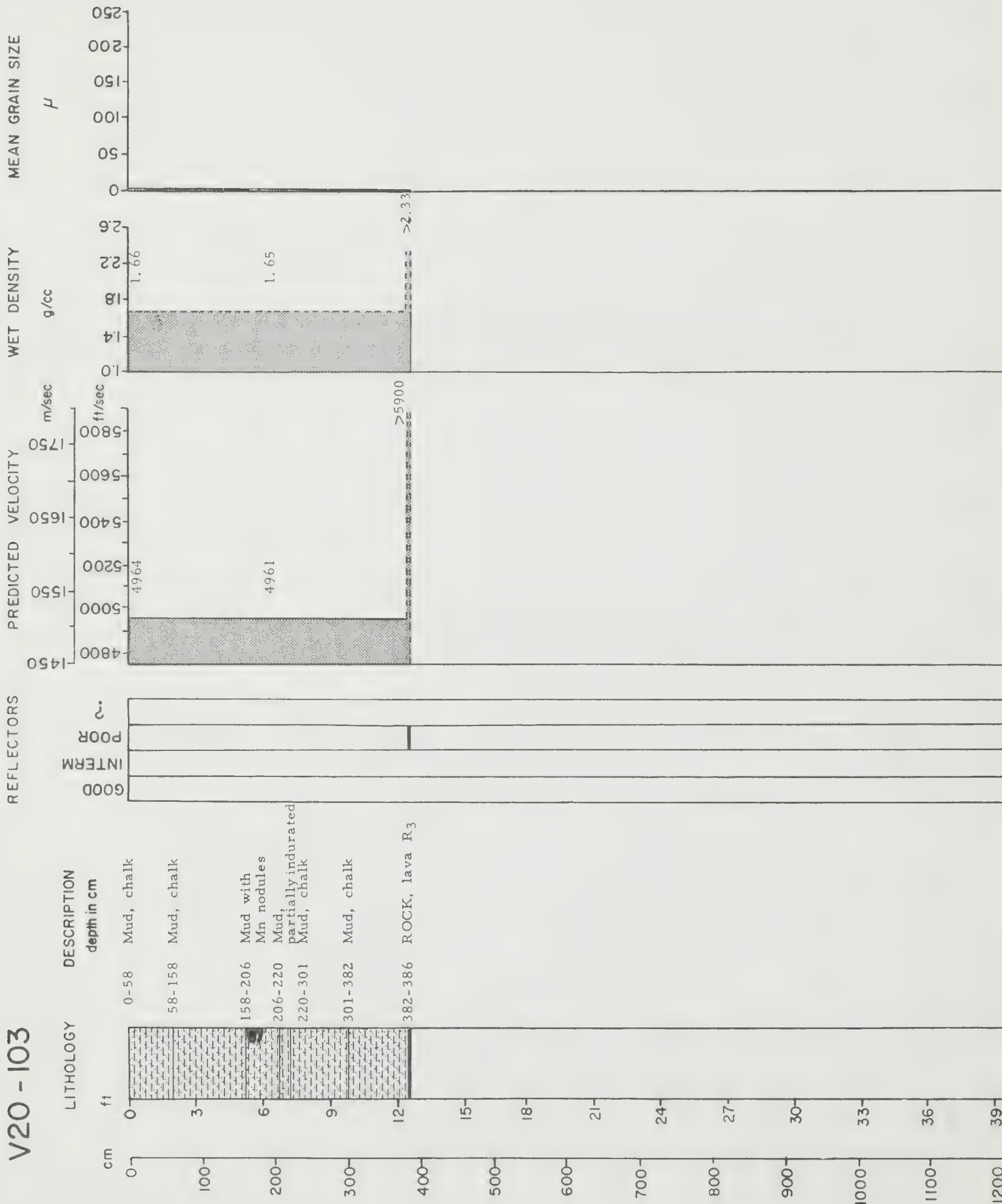
LITHOLOGY



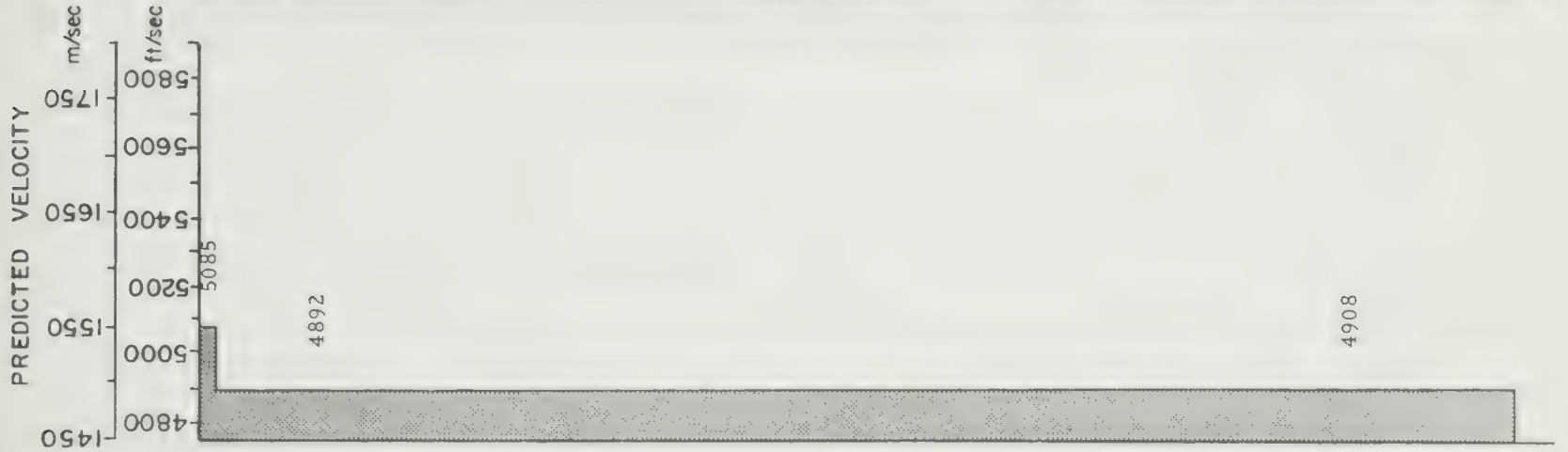
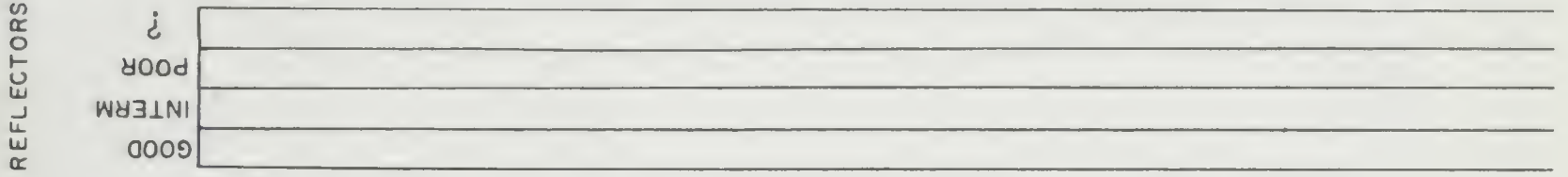
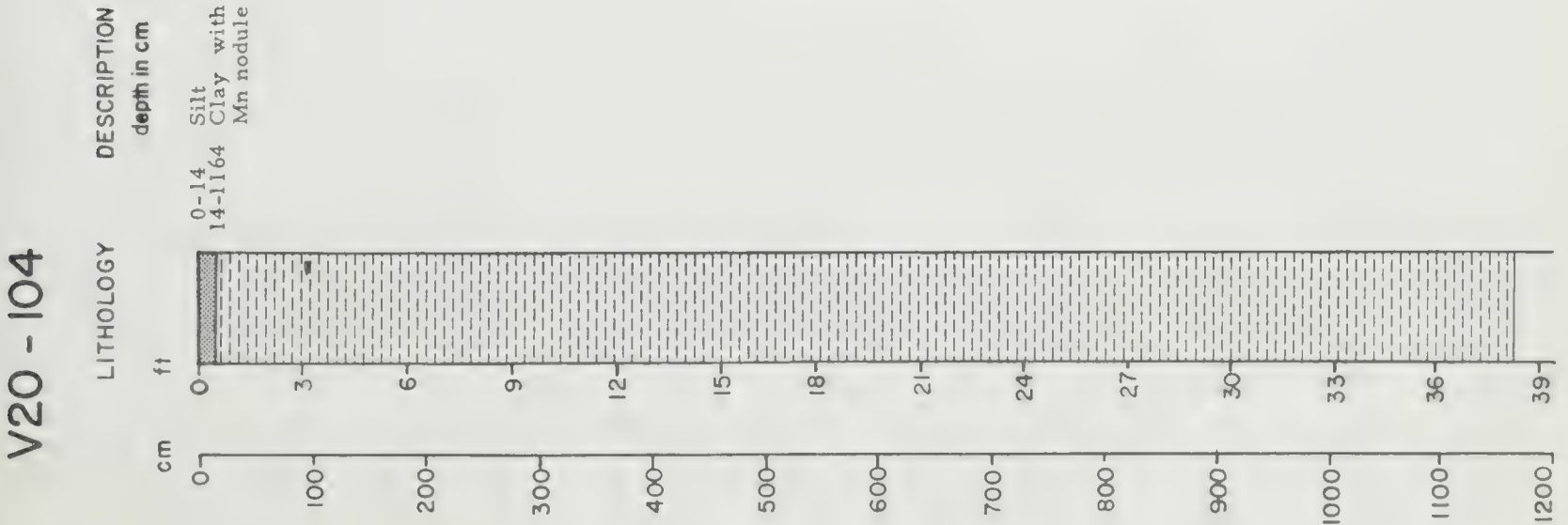


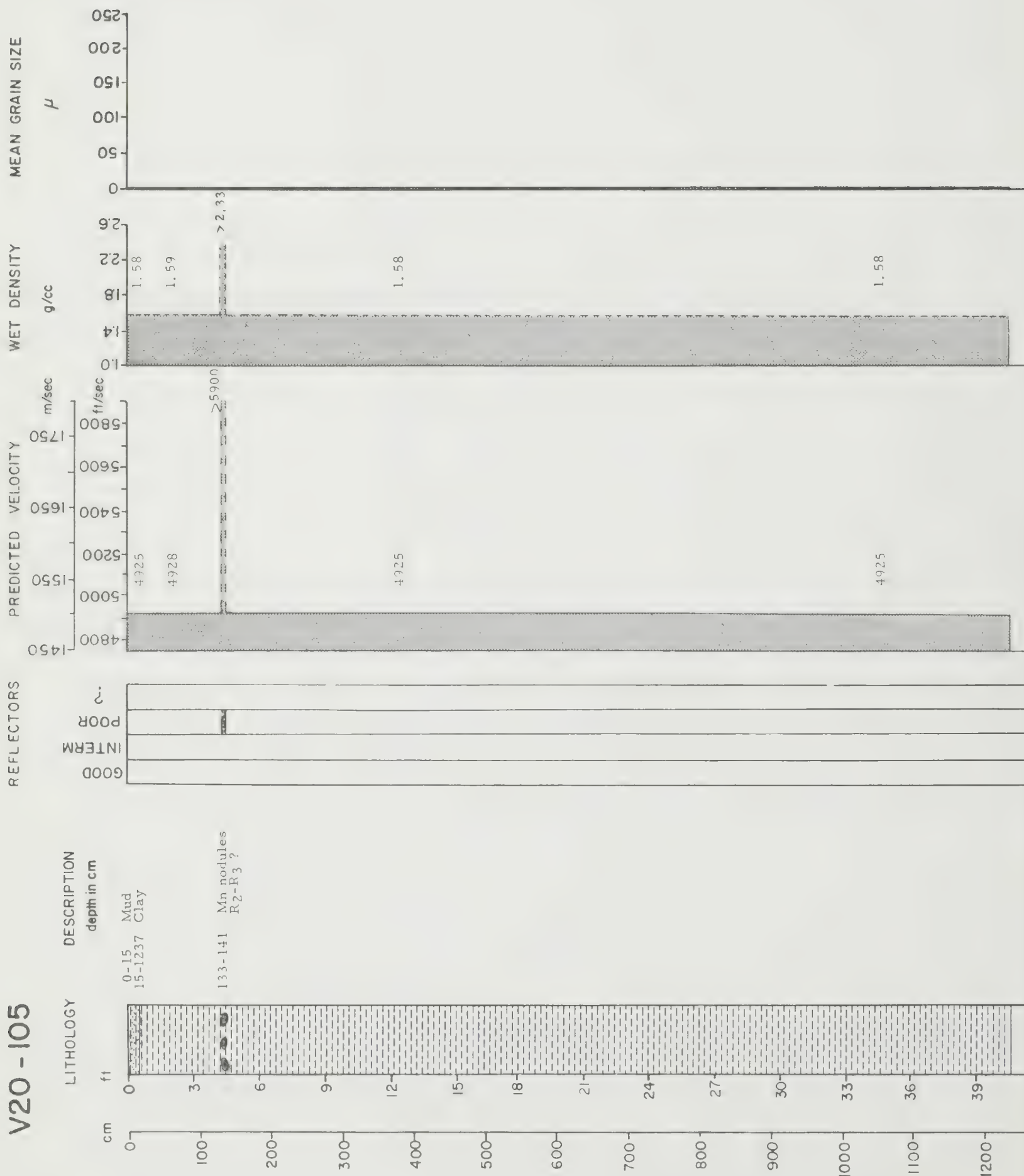


V20 - 103

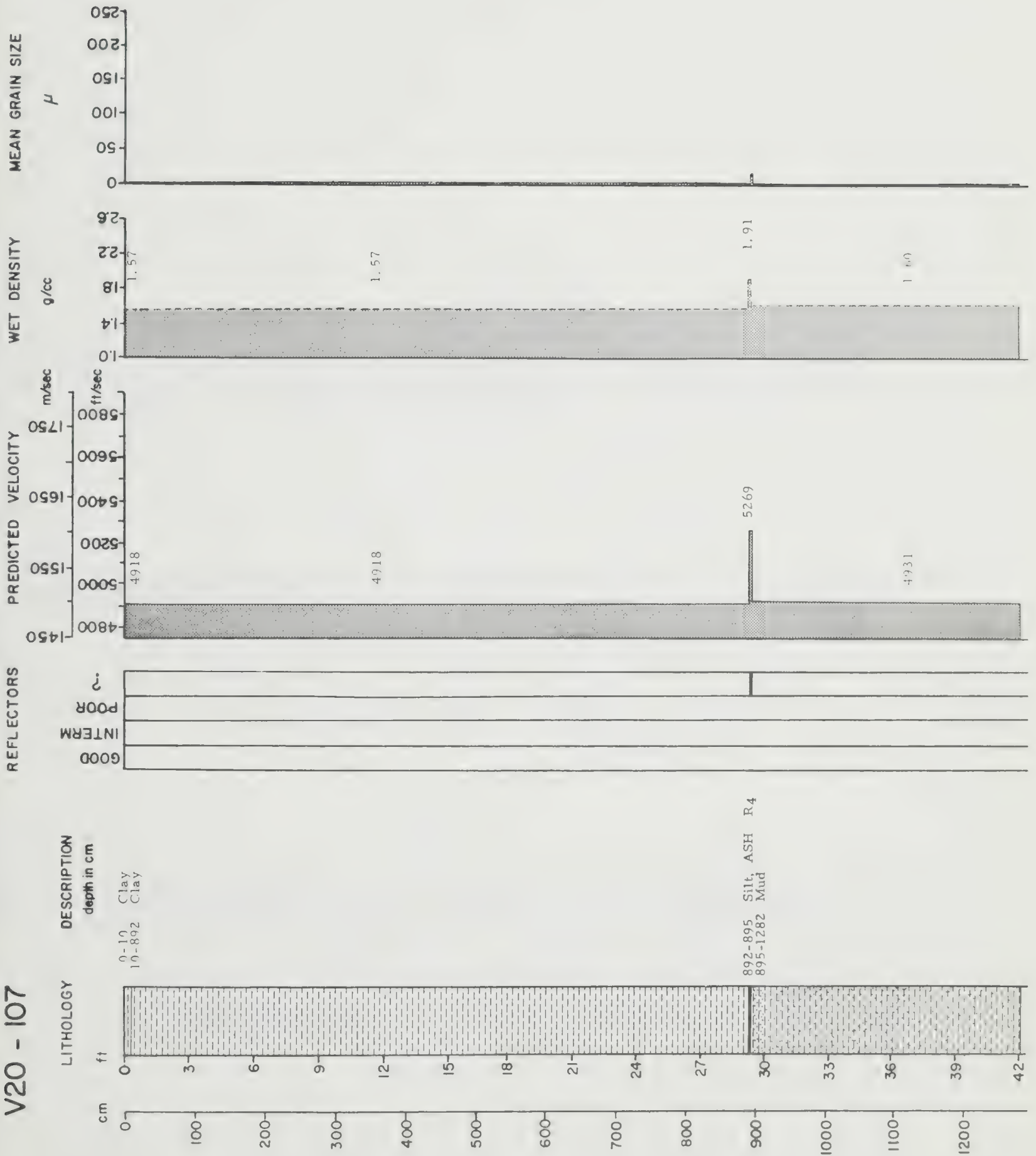


V20 - 104

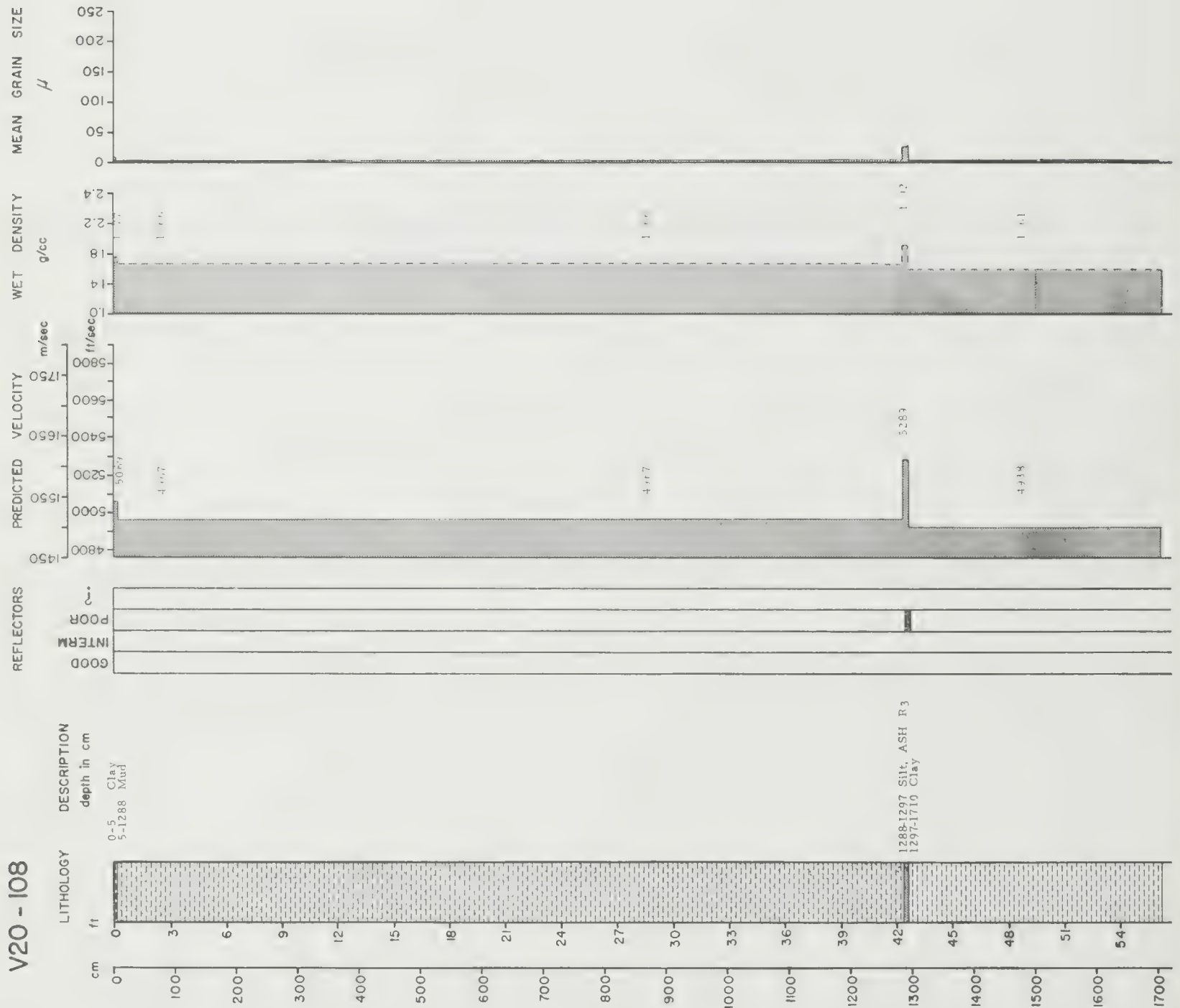




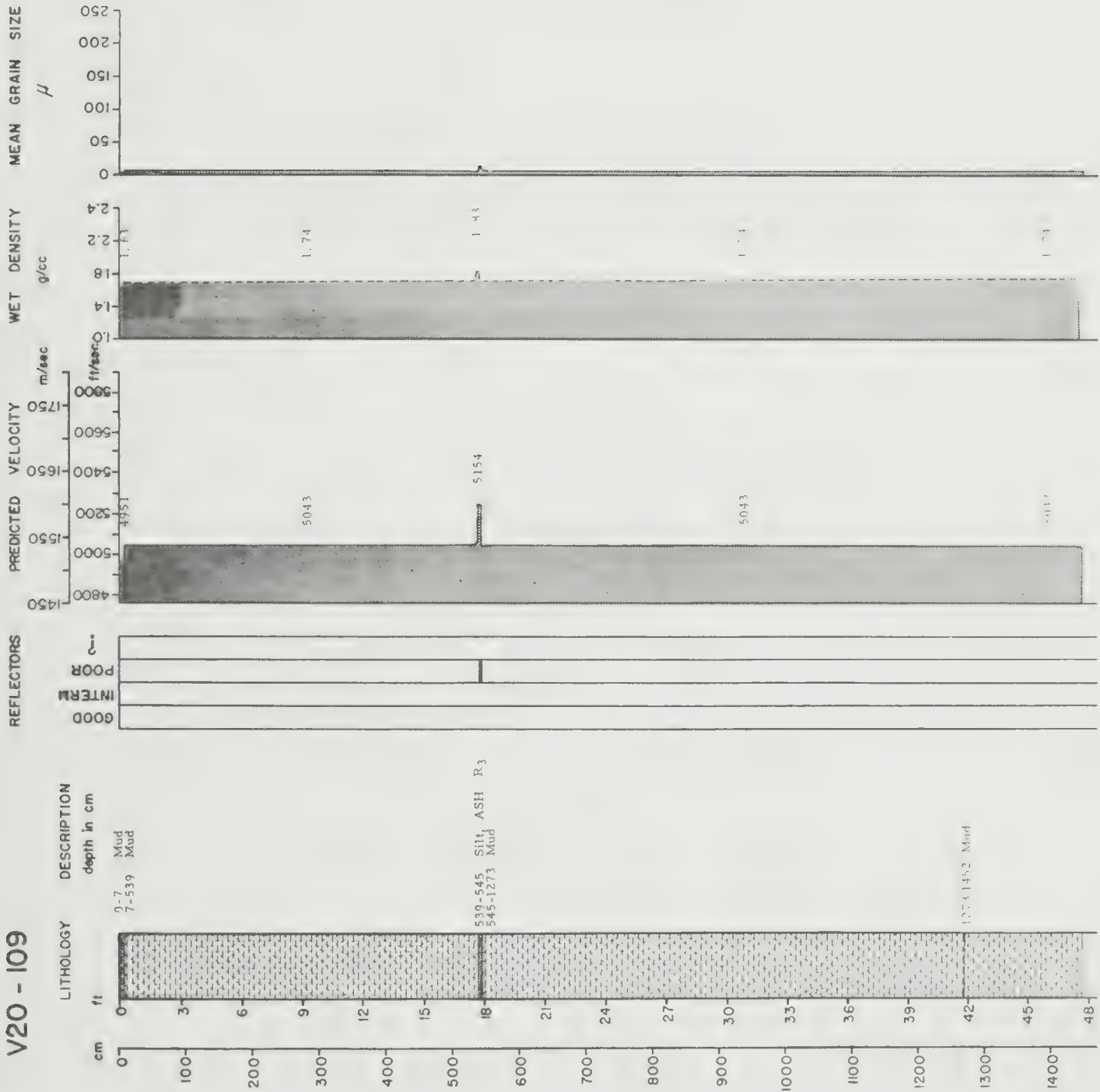




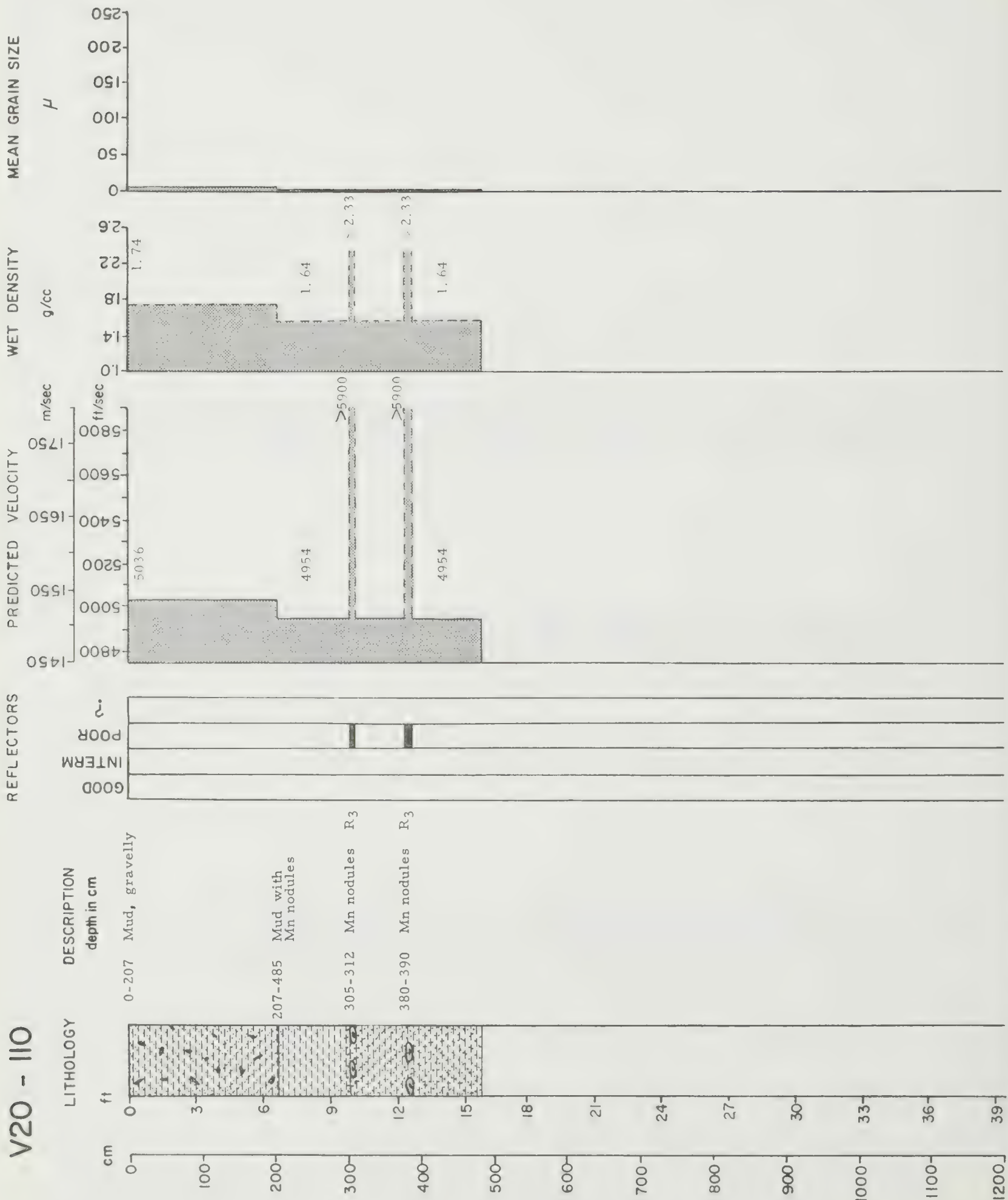
V20 - 108



V20 - 109

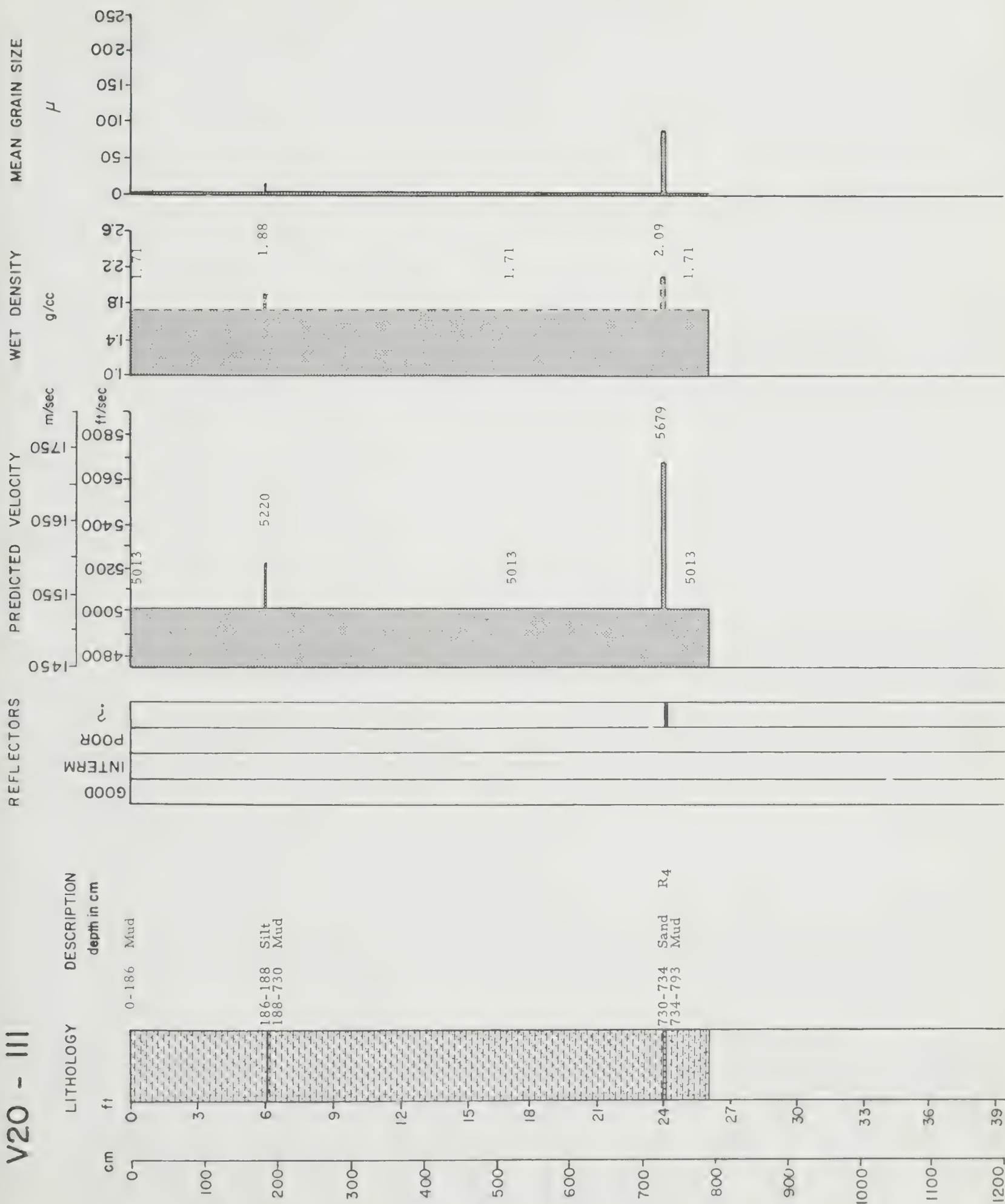


# V20 - 110

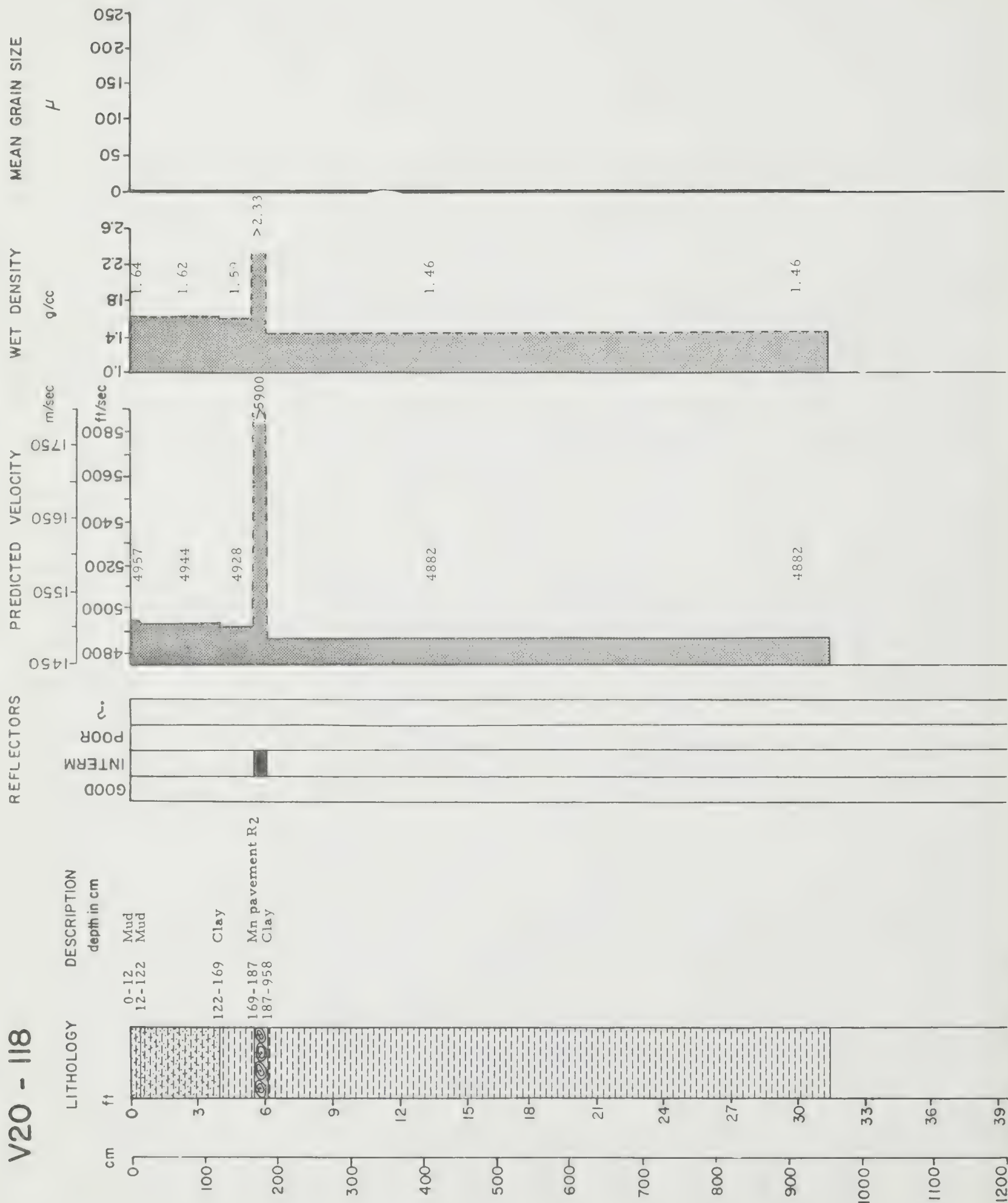


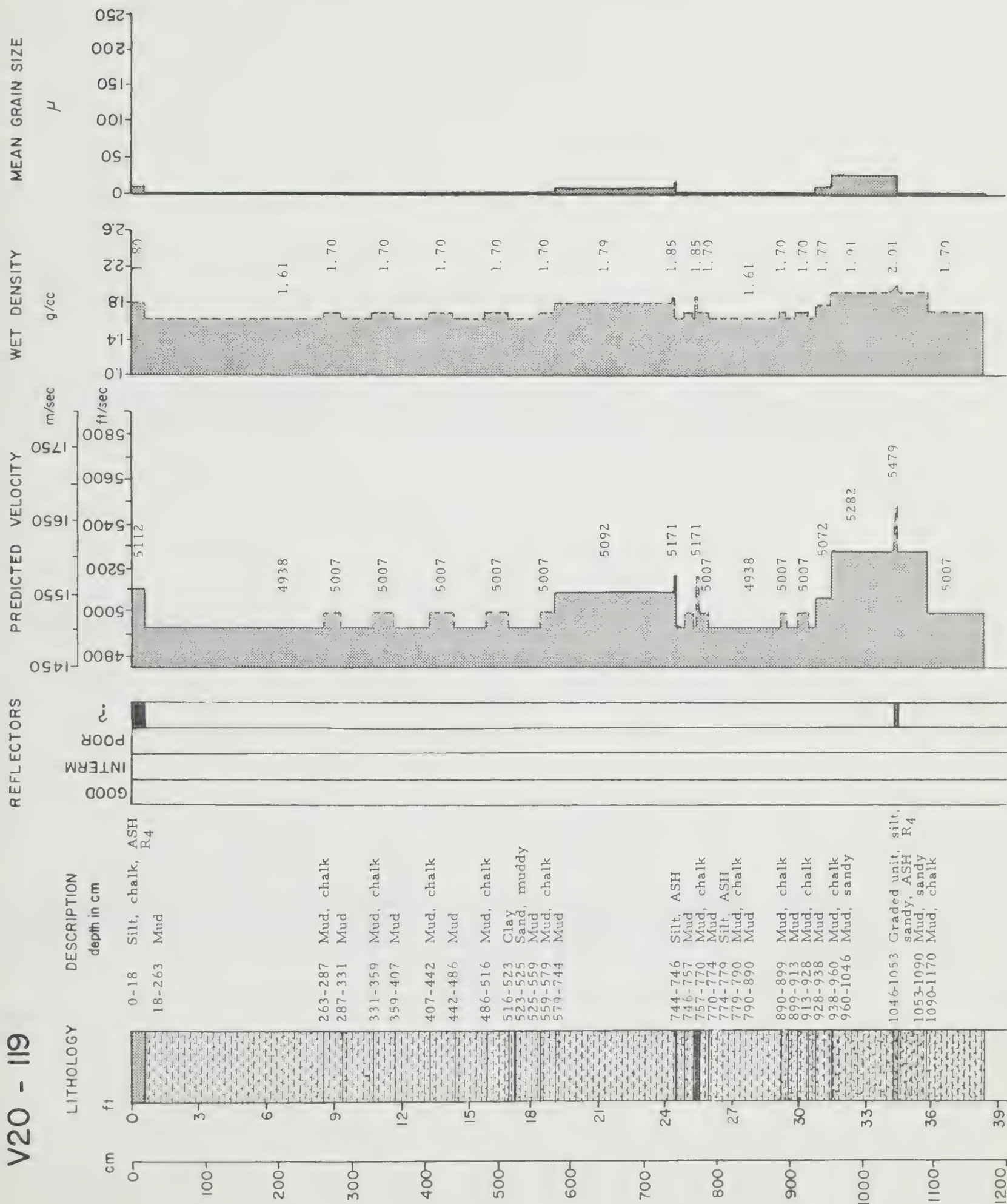


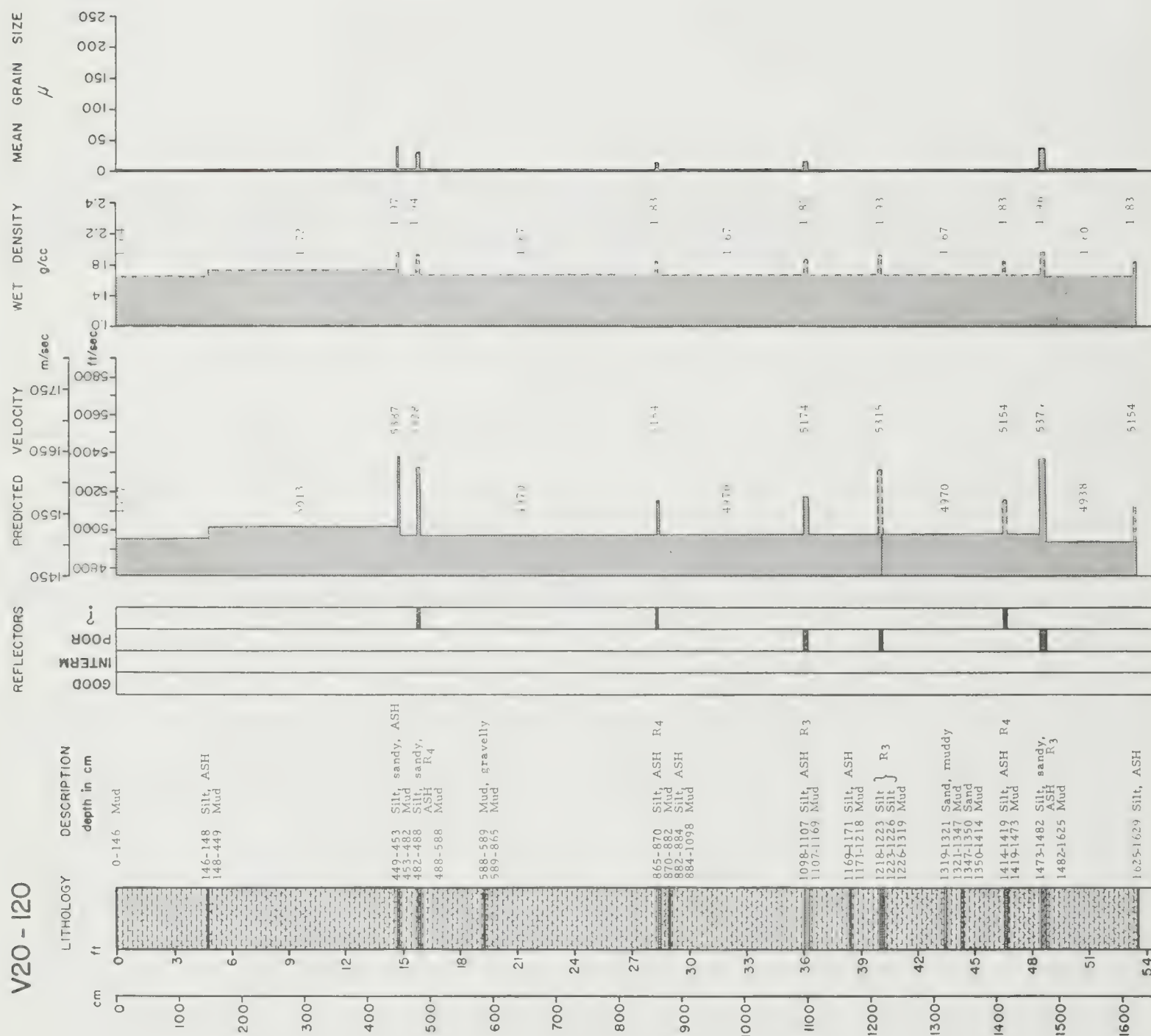
## V20 - III



V20 - 118

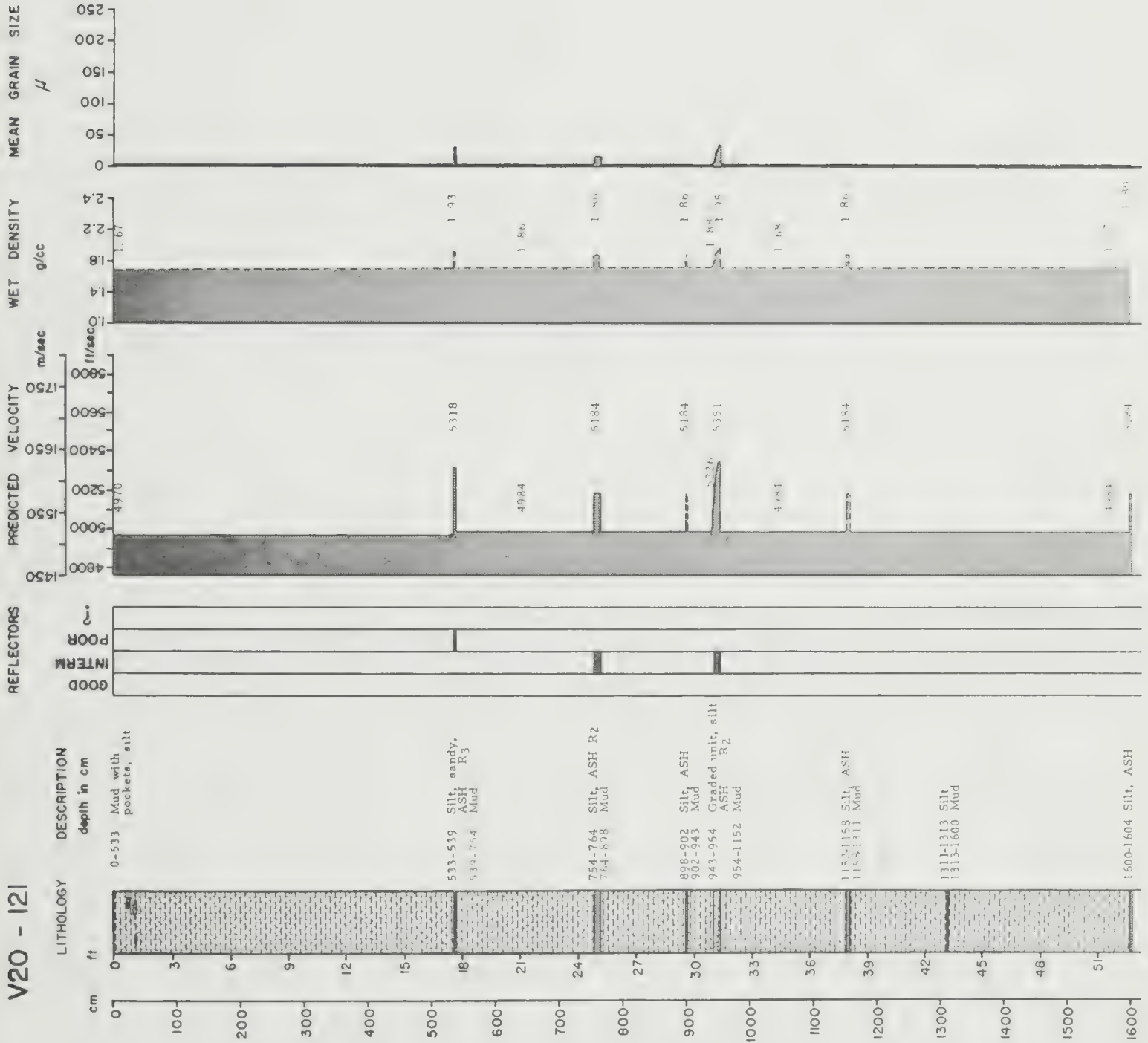


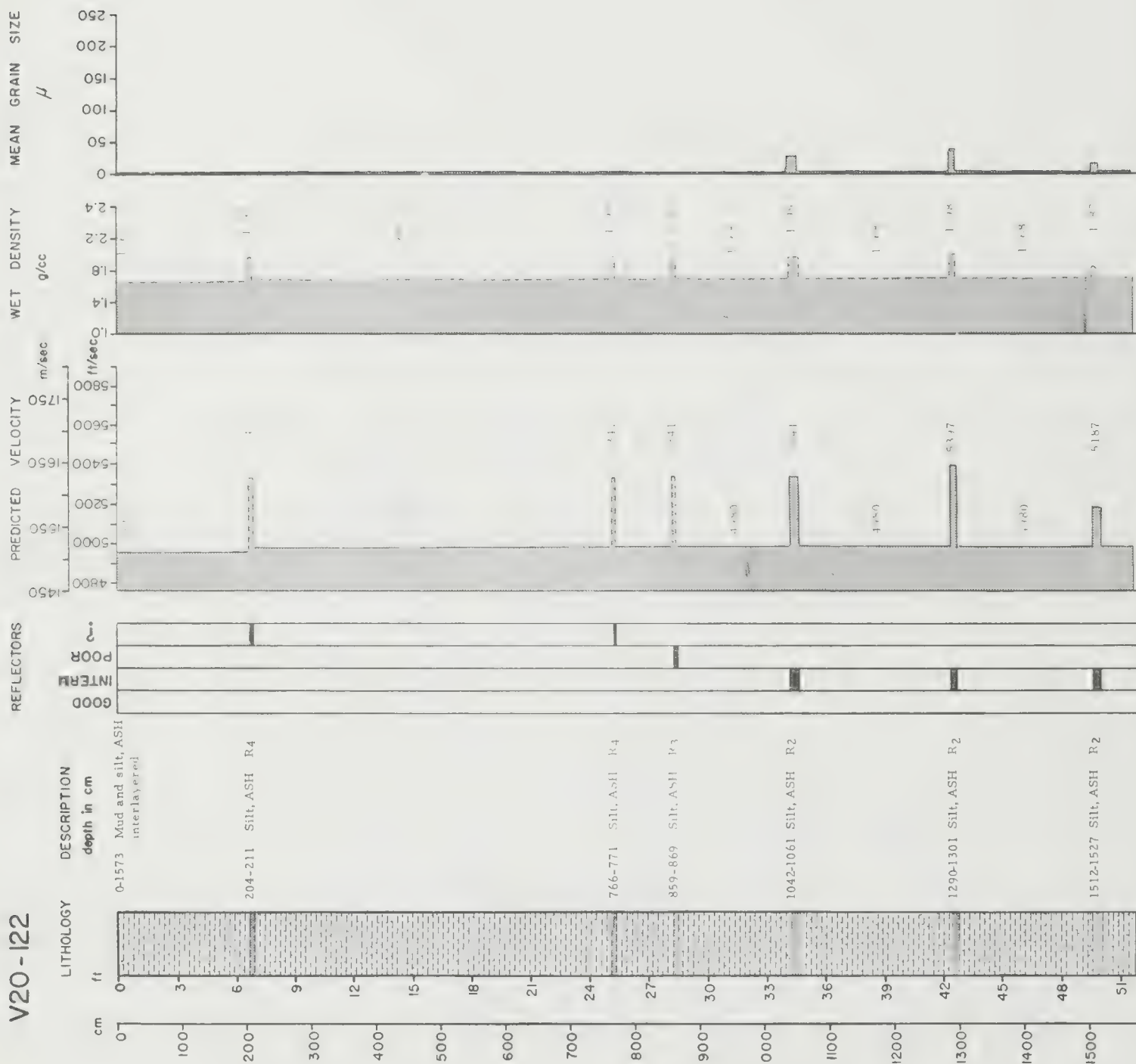


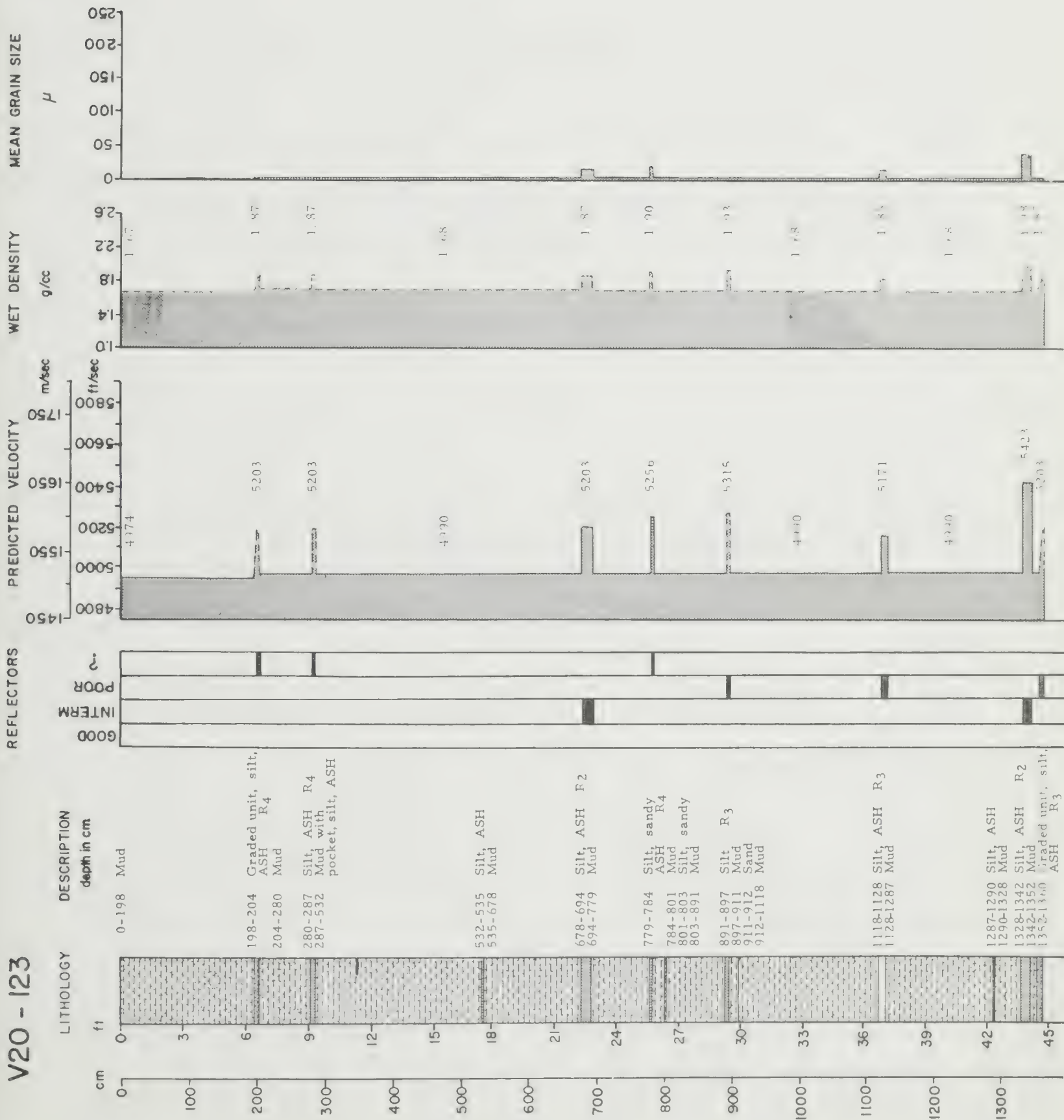




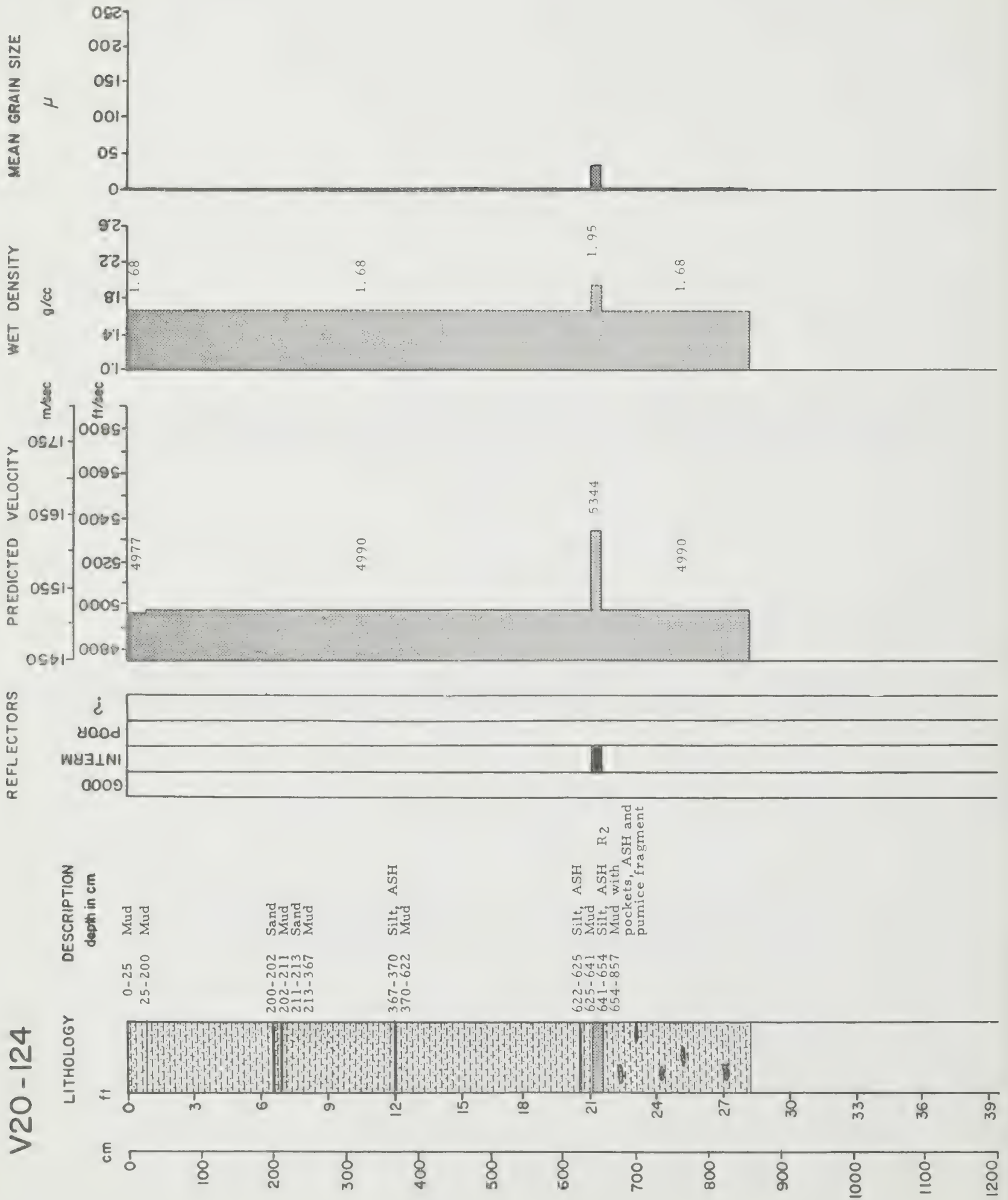
V20 - 121



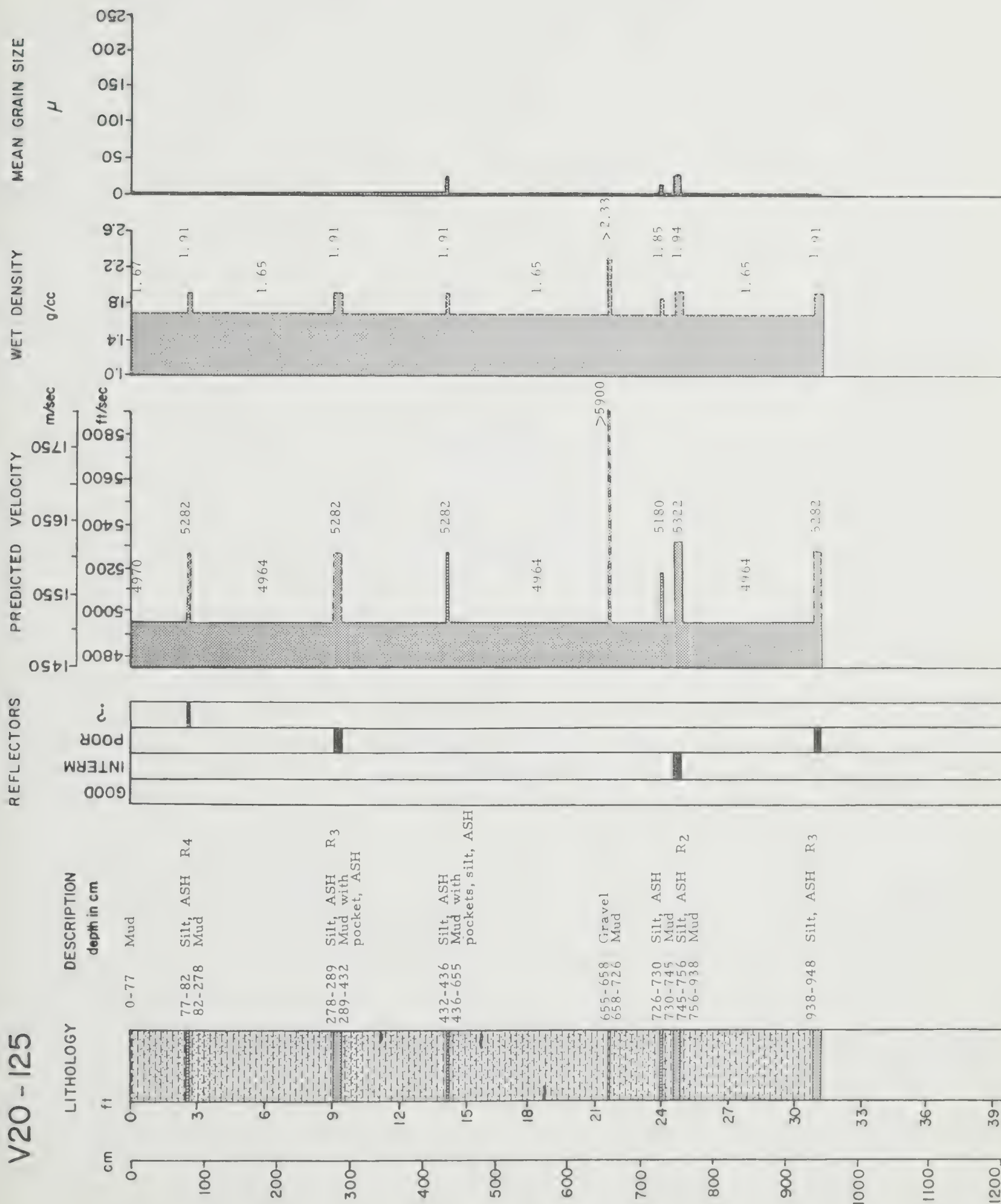


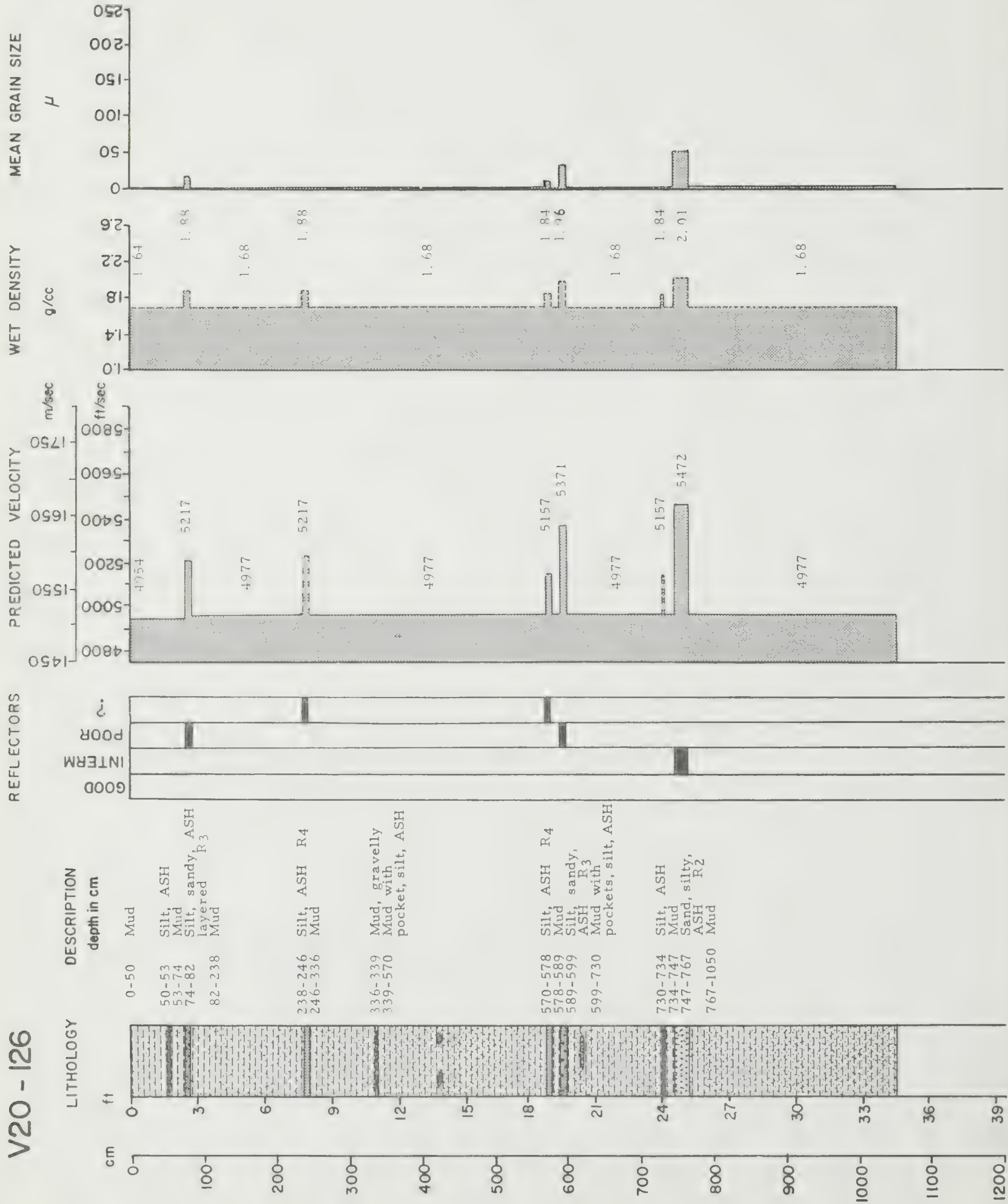


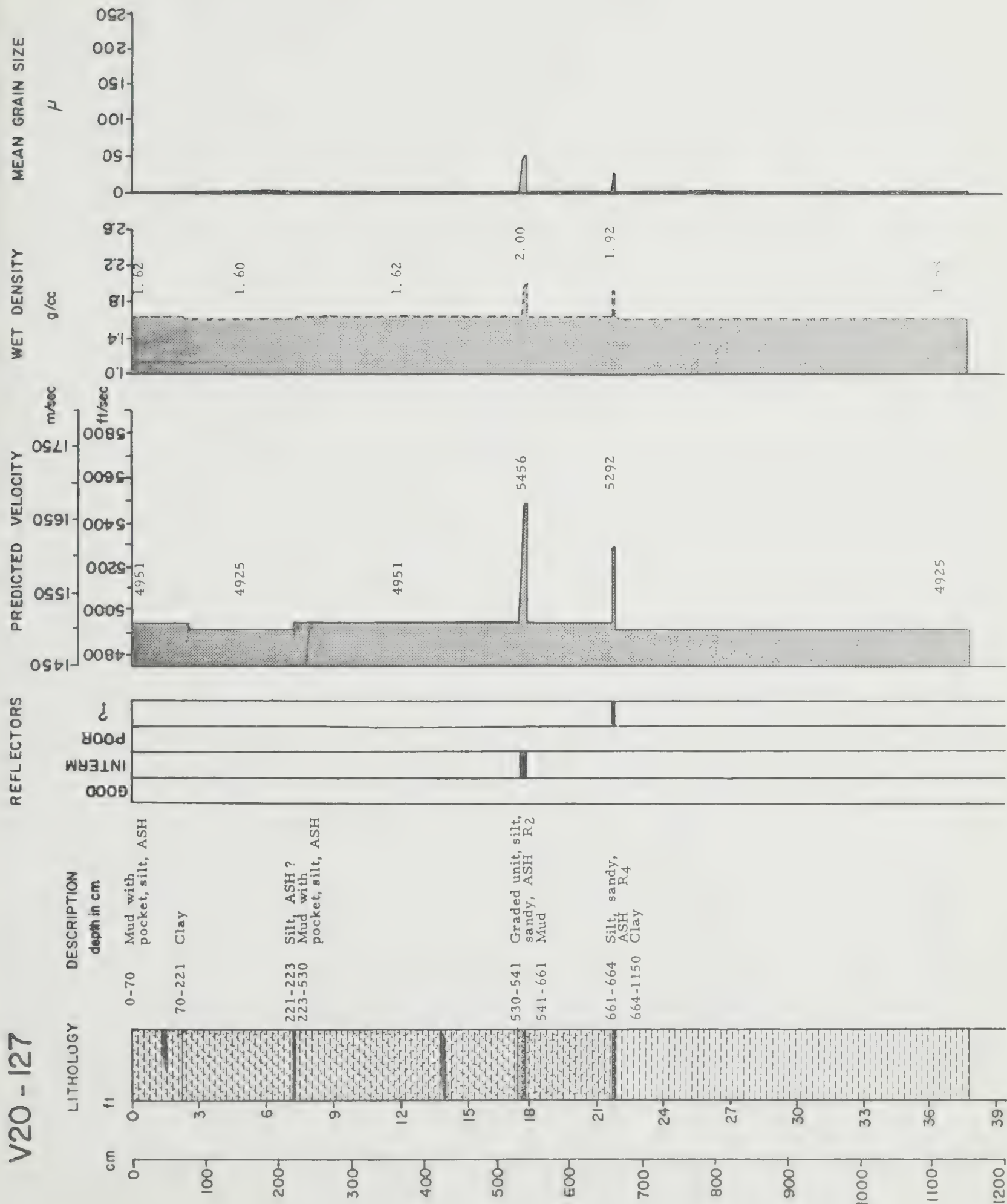
V20-124



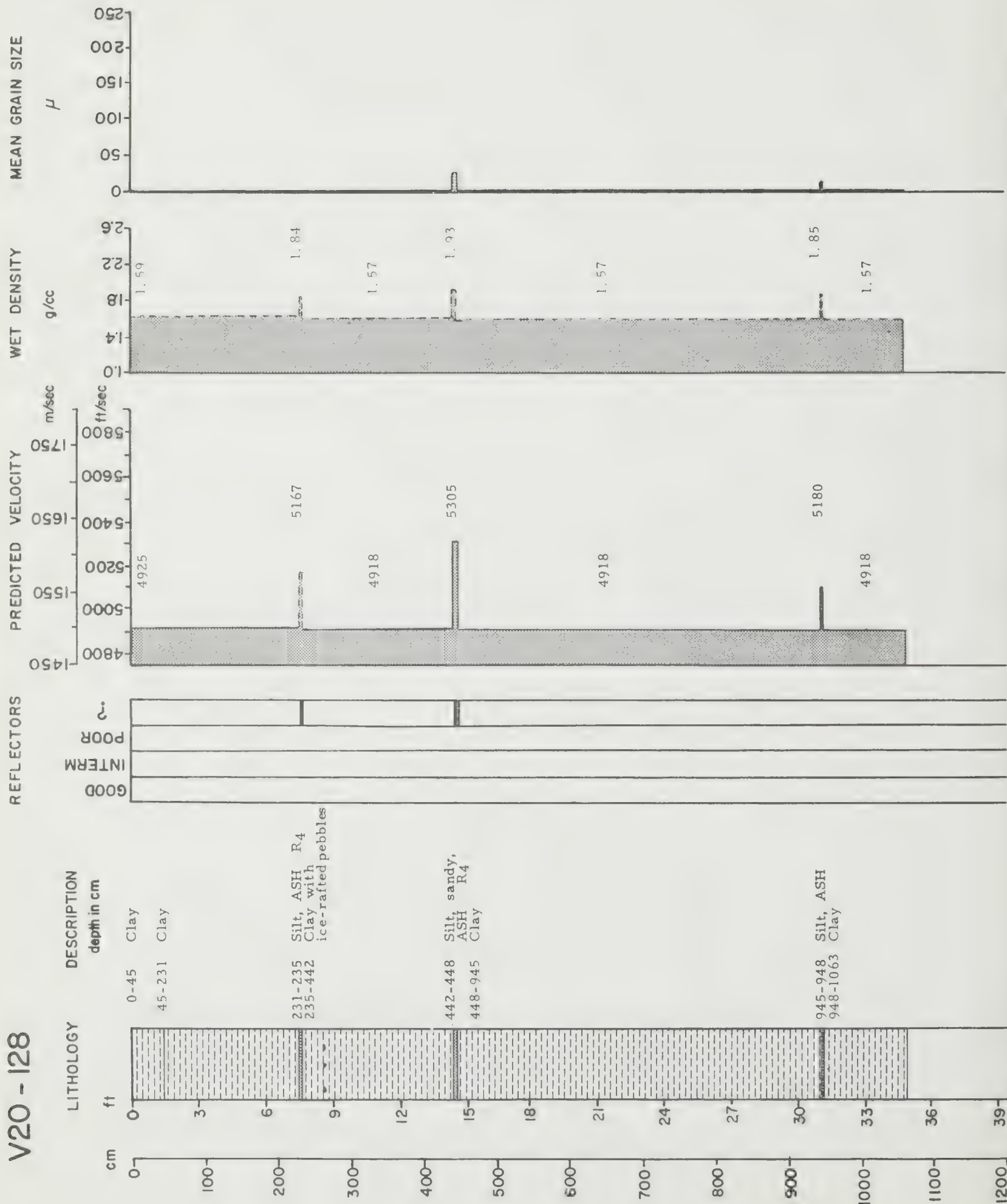






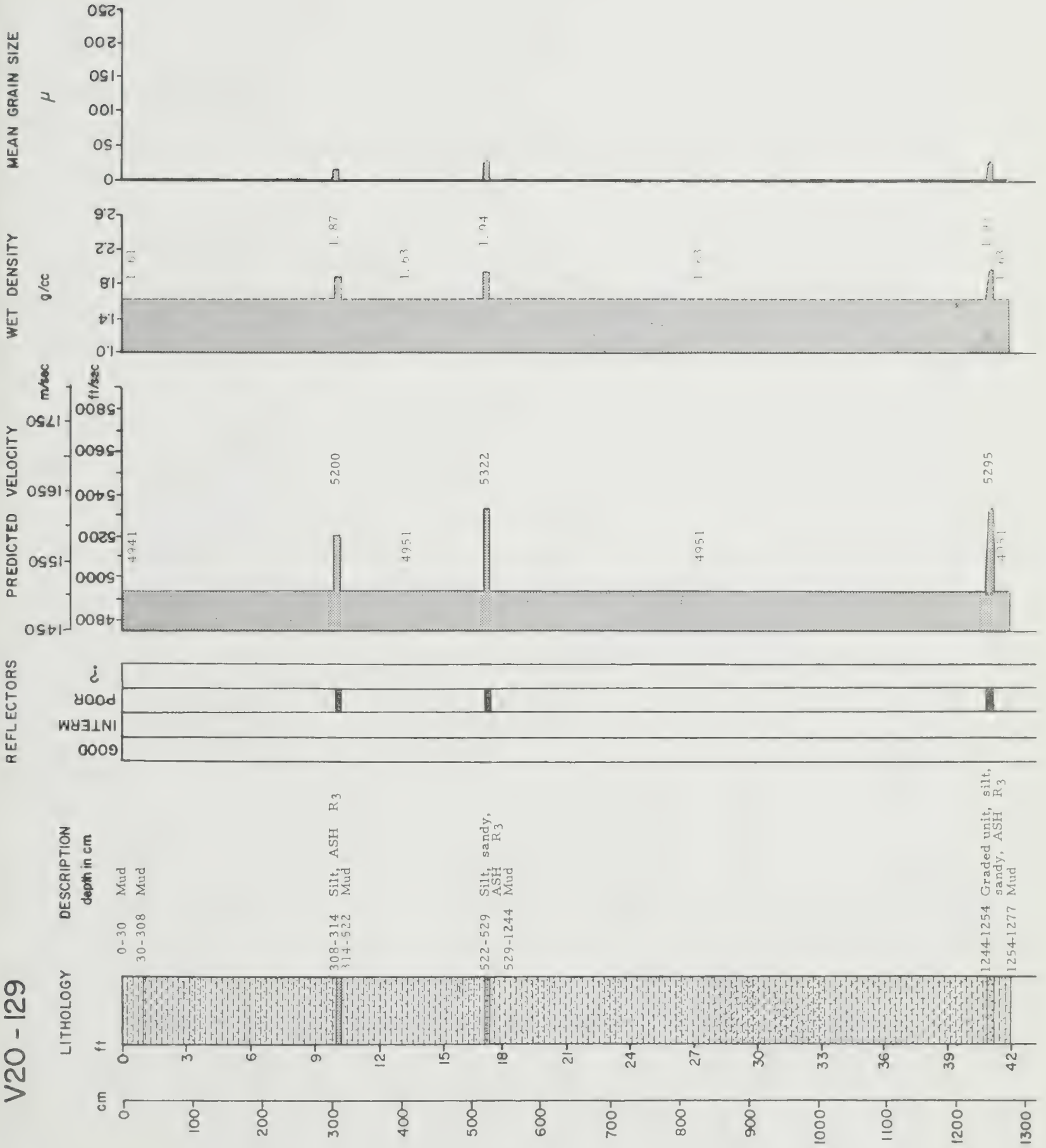


# V20 - 128

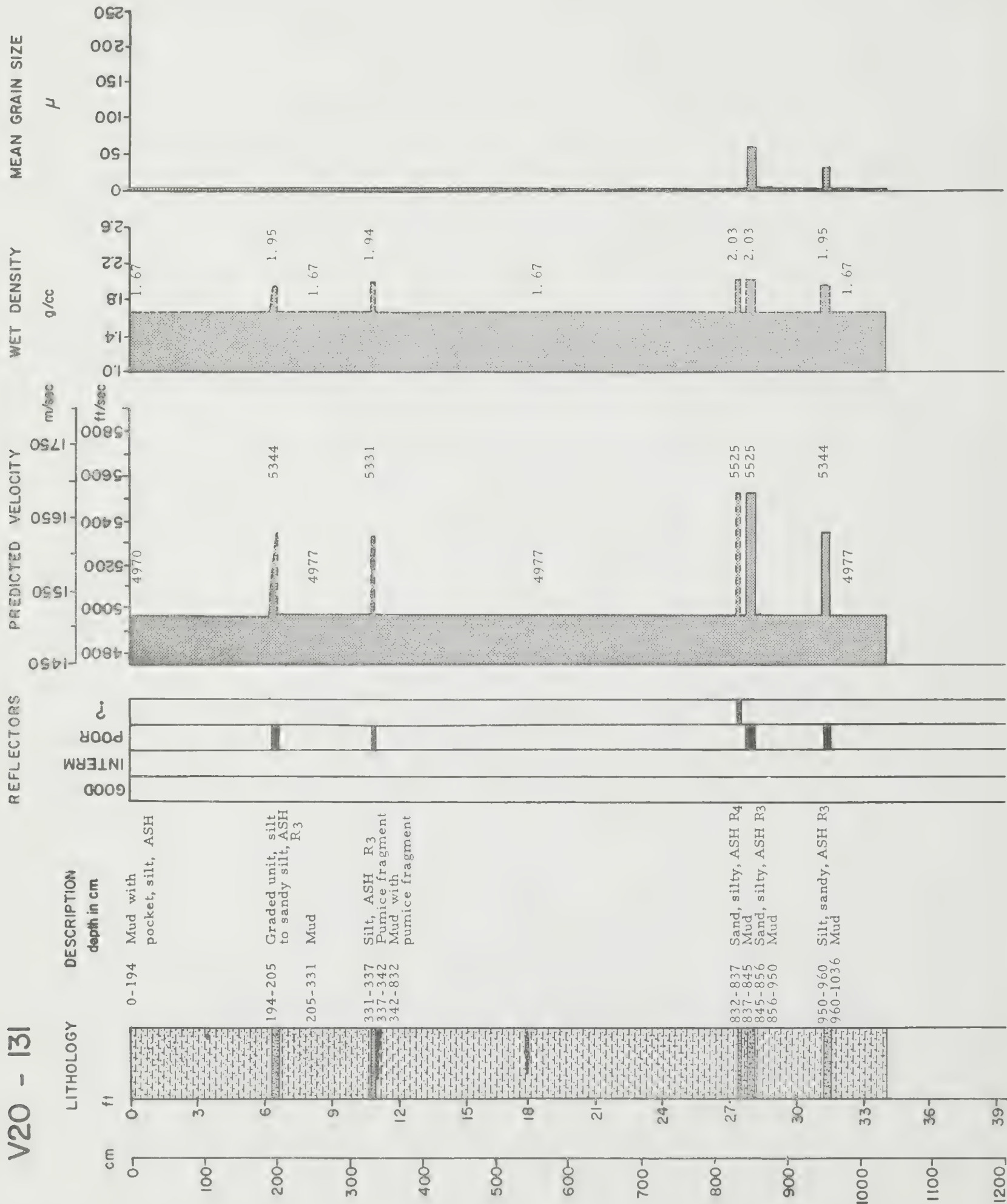


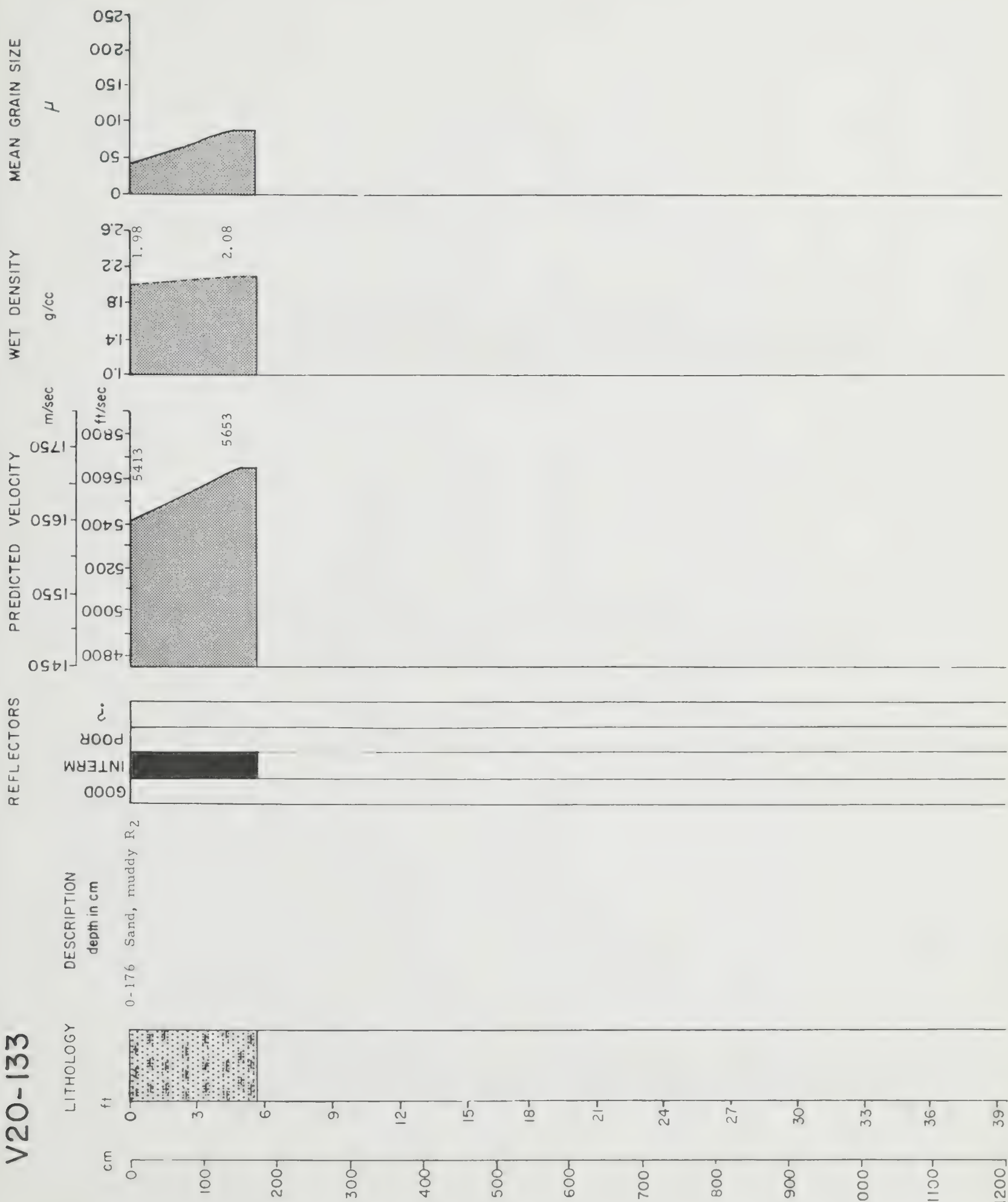


# V20 - 129



V20 - 131





V20-135

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

DESCRIPTION  
depth in cm

0-783 Mud with sand

71-79 Sand R3

100-103 Sand R4

170-182 Sand R3

201-215 Sand R2

278-288 Sand R2

411-439 Sand R1

530-536 Sand R4

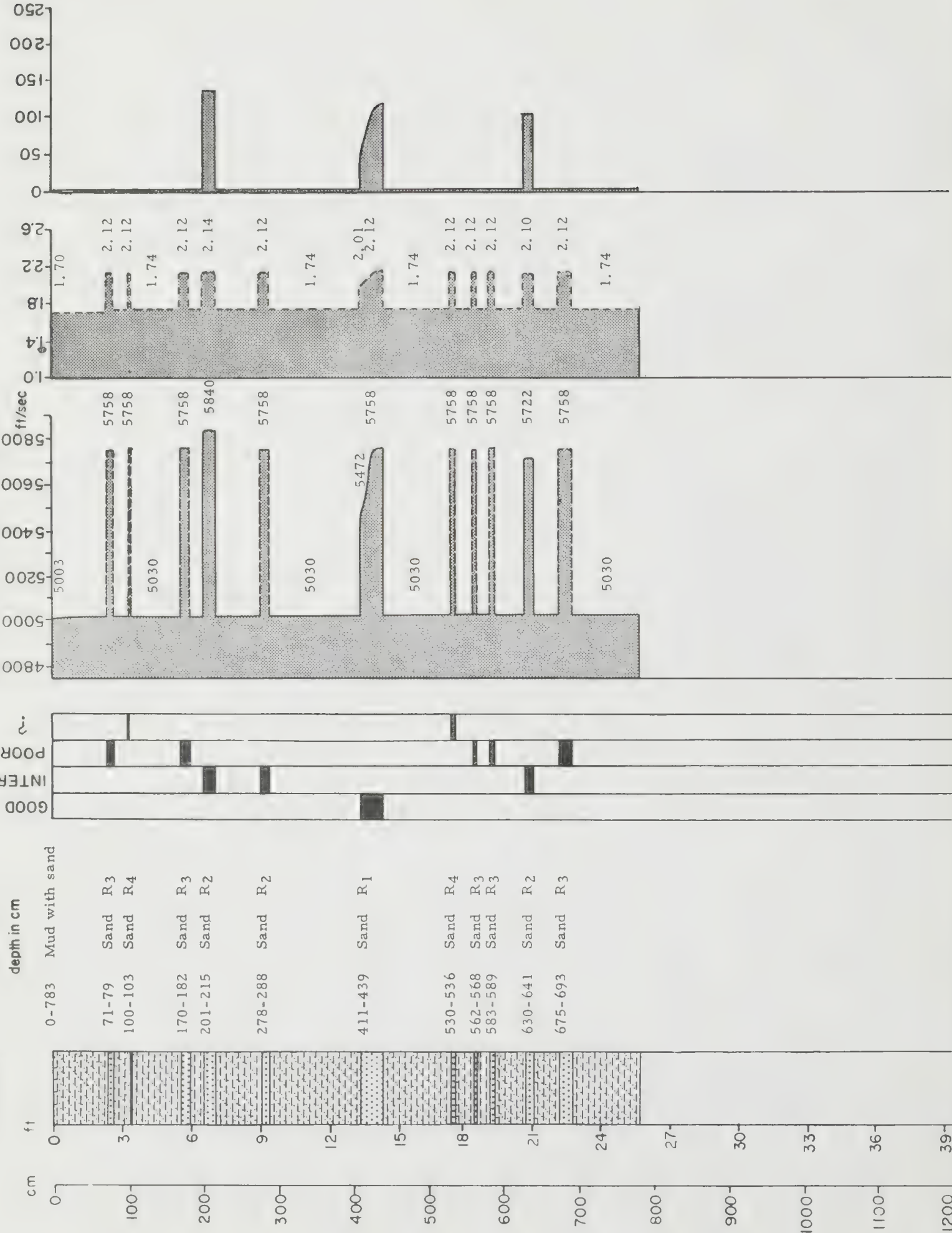
562-568 Sand R3

583-589 Sand R3

630-641 Sand R2

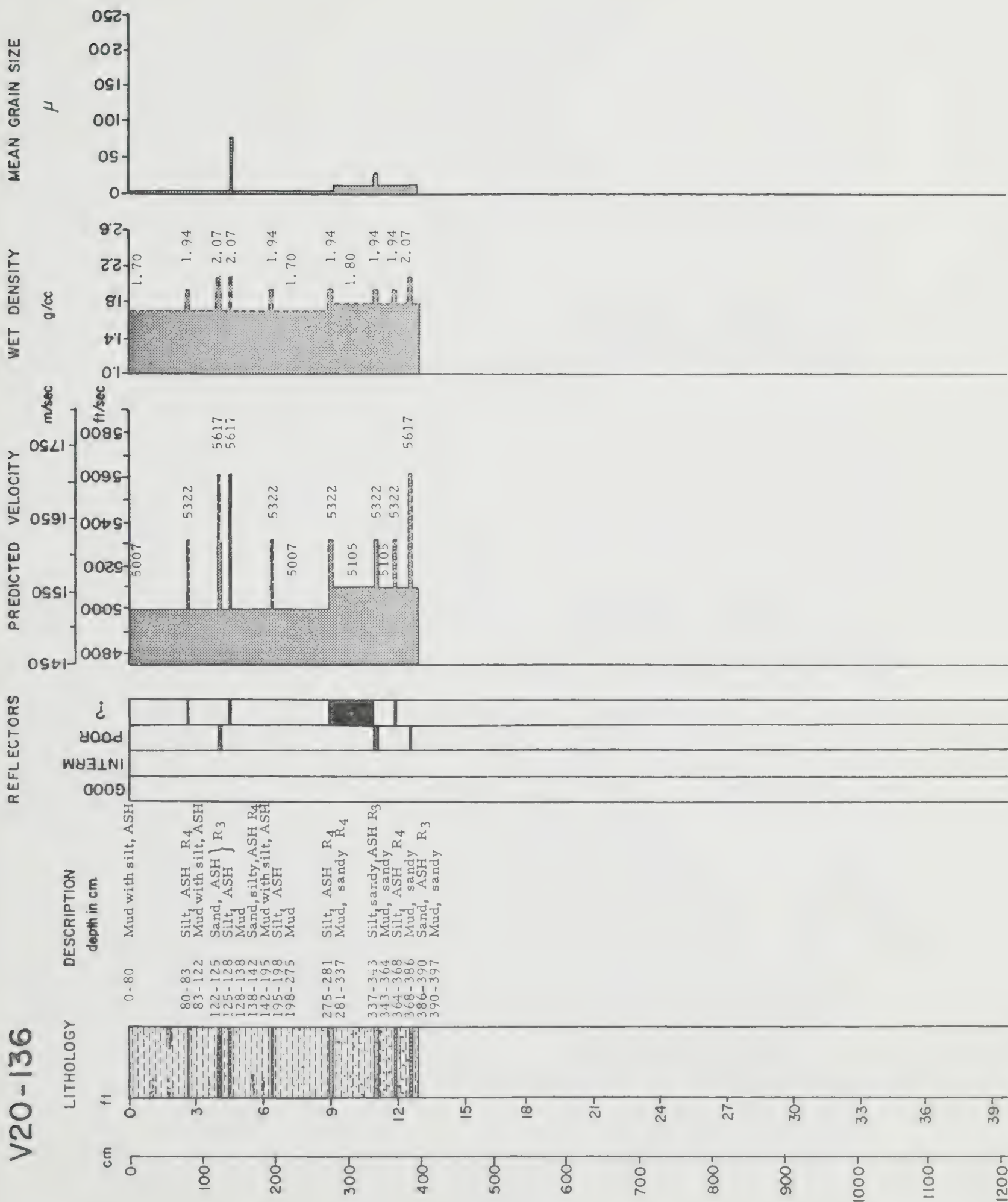
675-693 Sand R3

LITHOLOGY

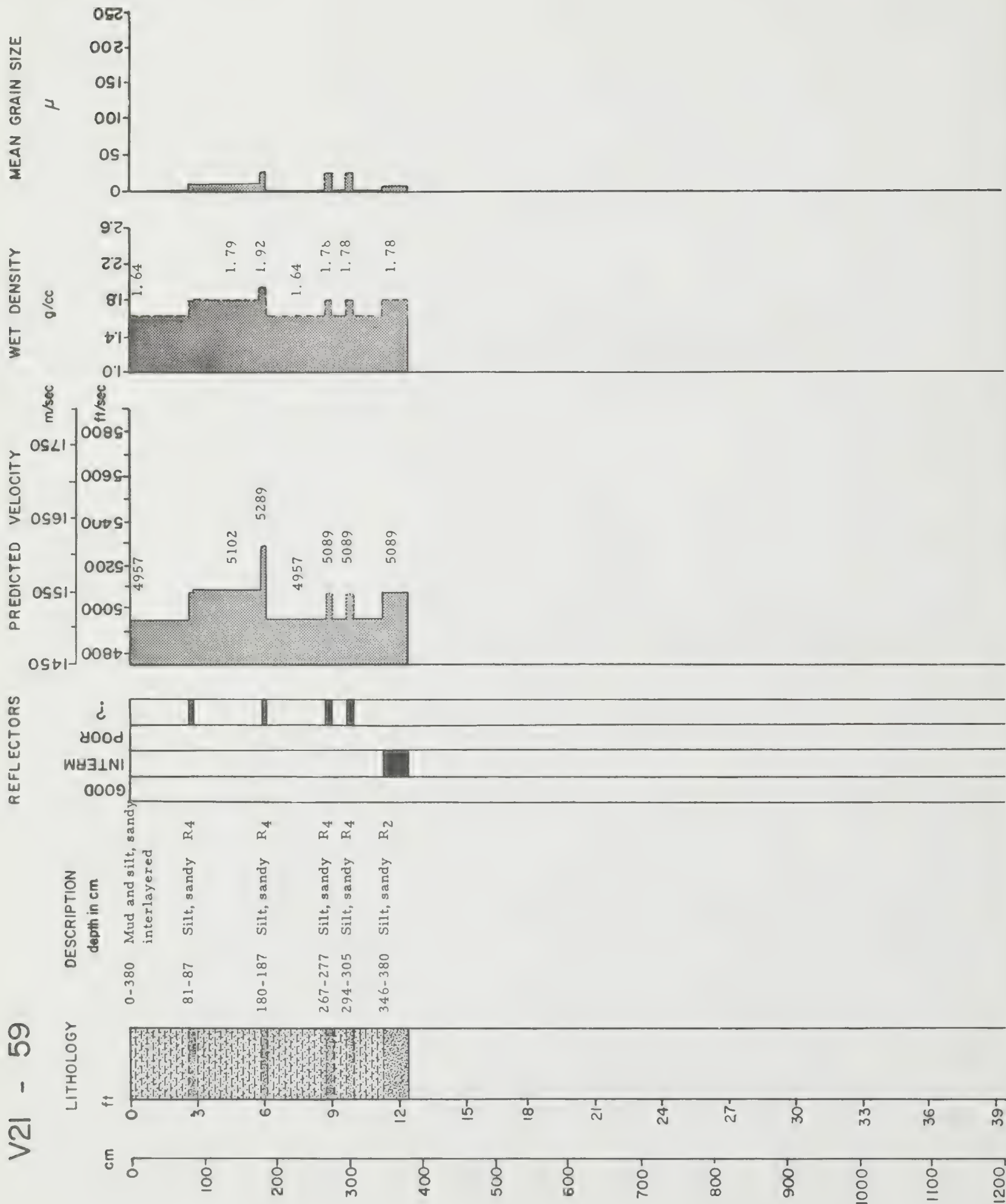




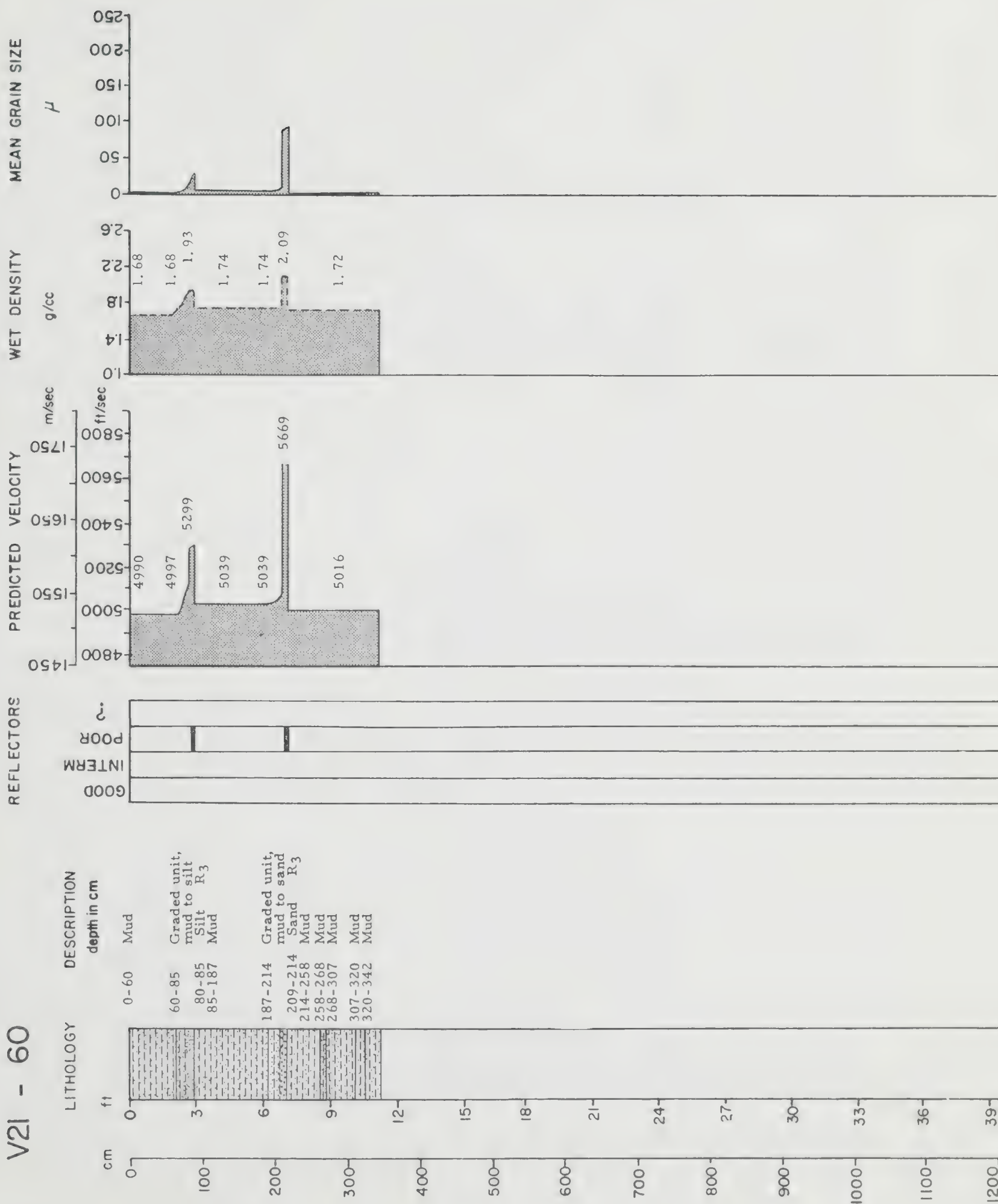
V20-136



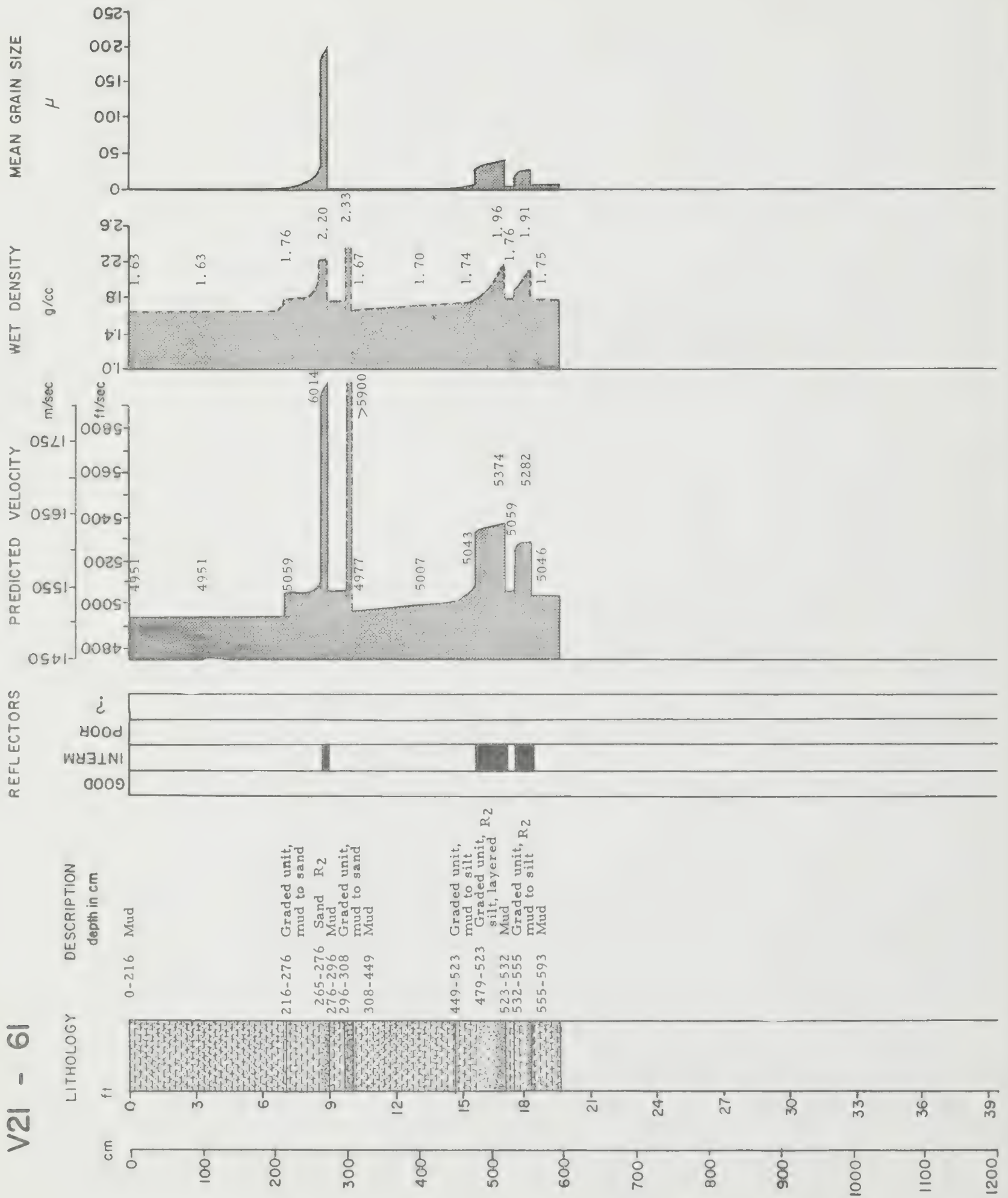
V21 - 59



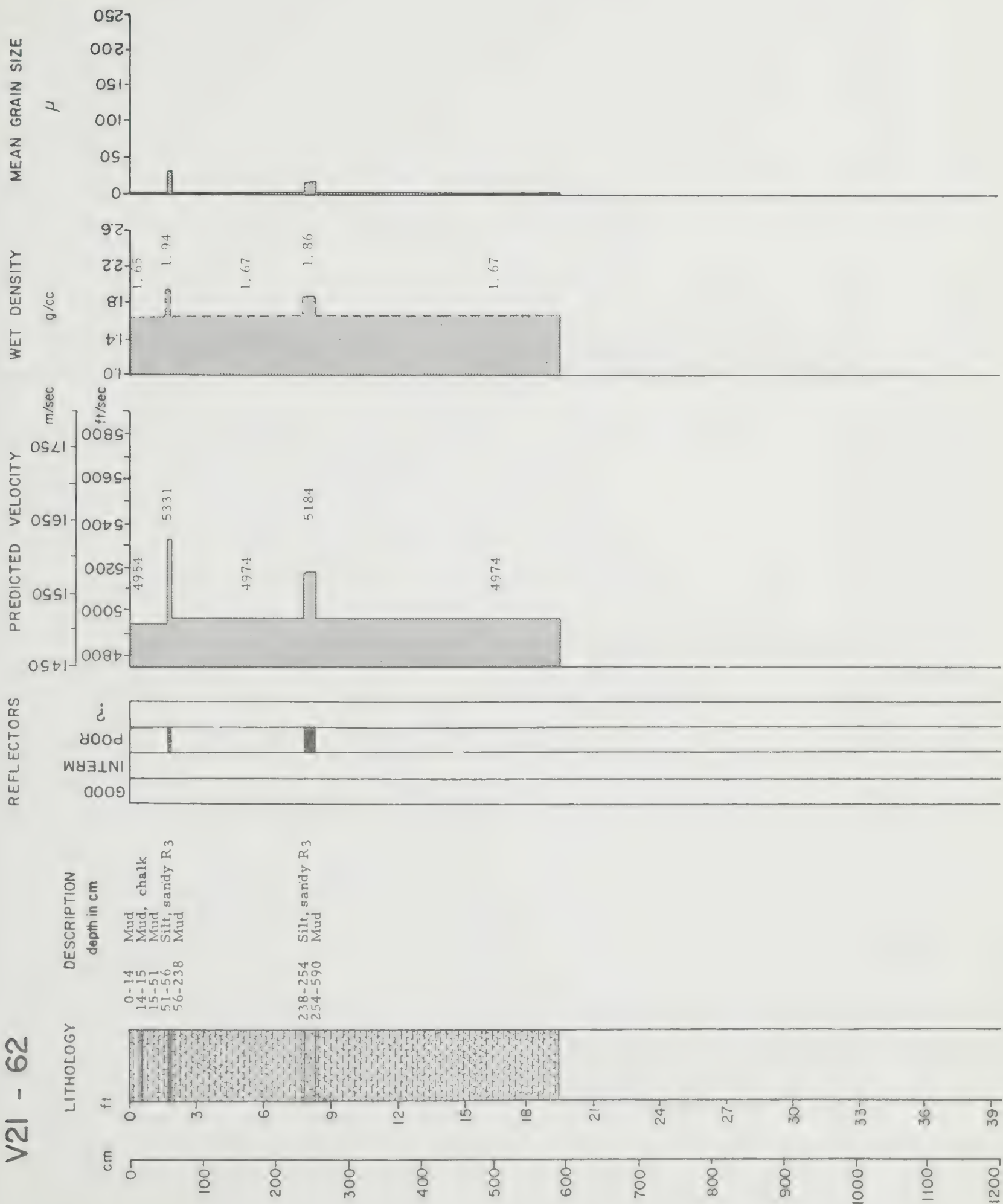
V21 - 60



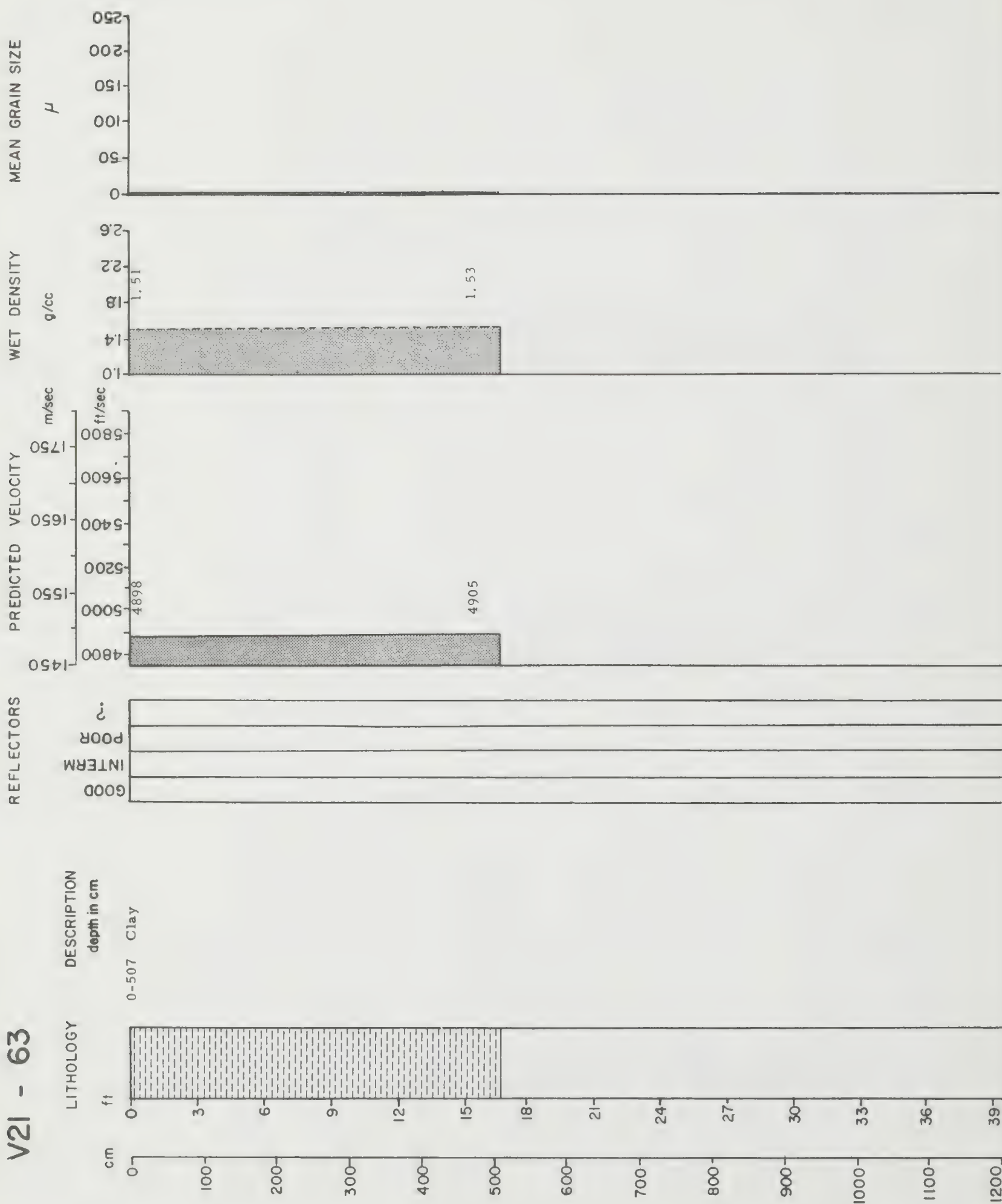
# V21 - 61



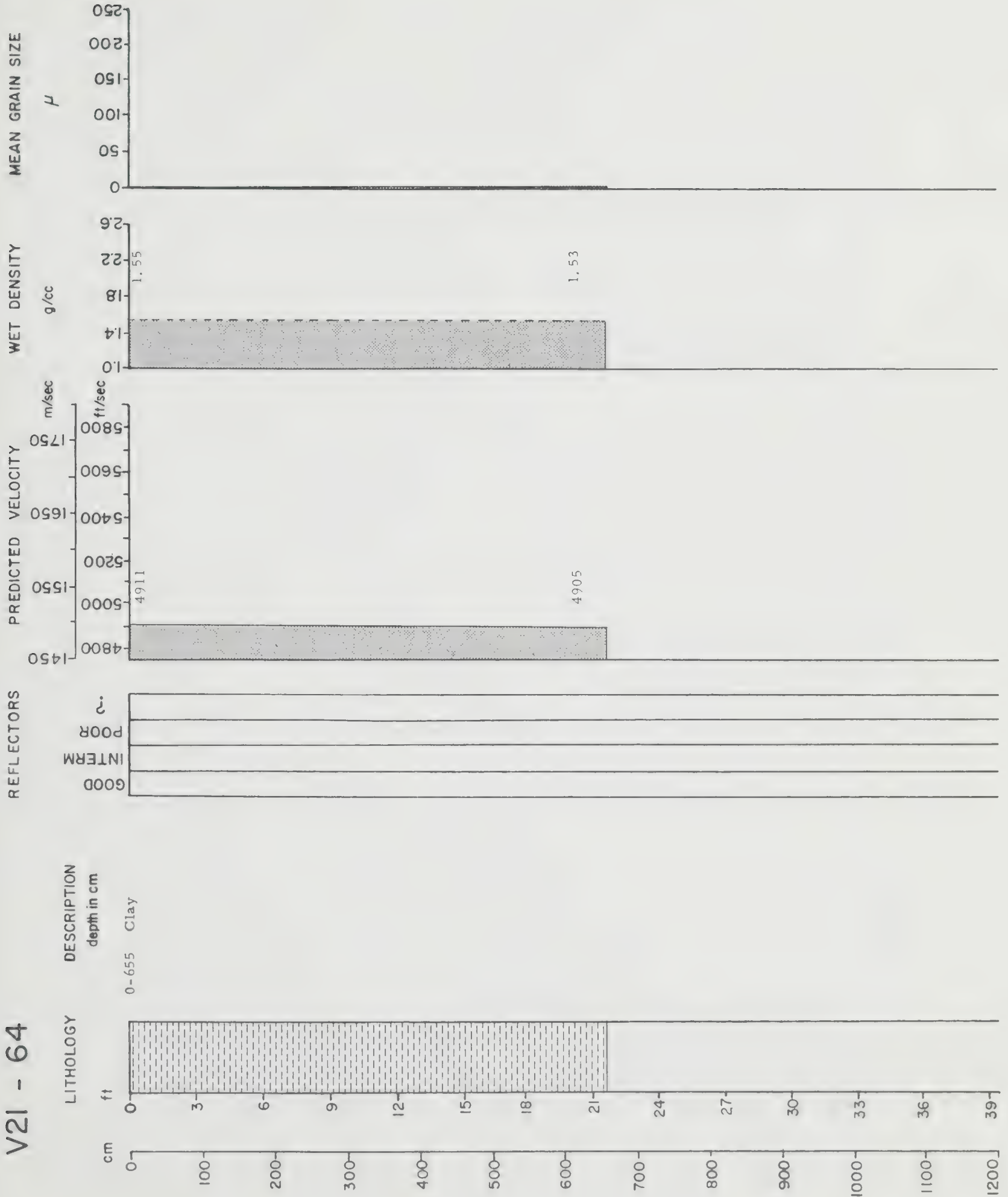




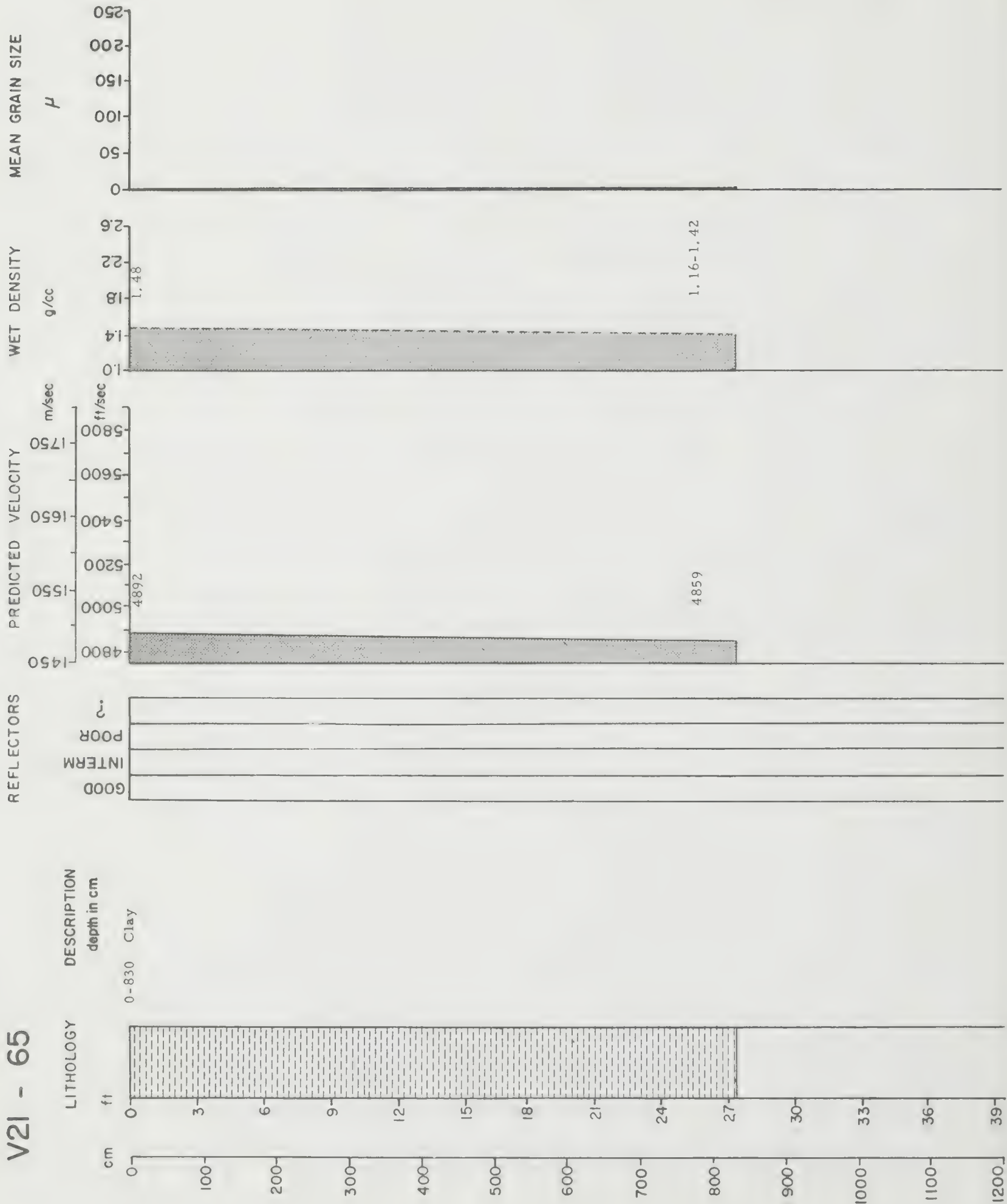
V21 - 63



V21 - 64

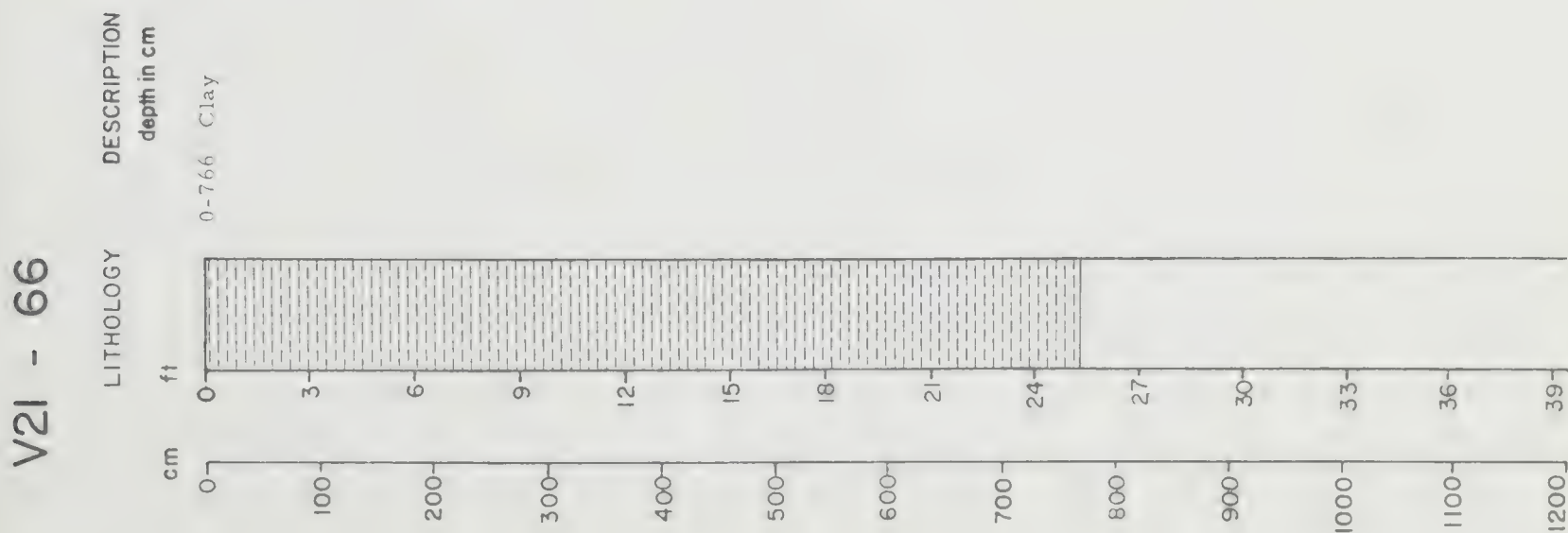


V21 - 65





V21 - 66



**REFLECTORS**

GOOD  
INTERM  
POOR  
?

**PREDICTED VELOCITY**

m/sec

ft/sec

4800 4895 4928

**WET DENSITY**

g/cc

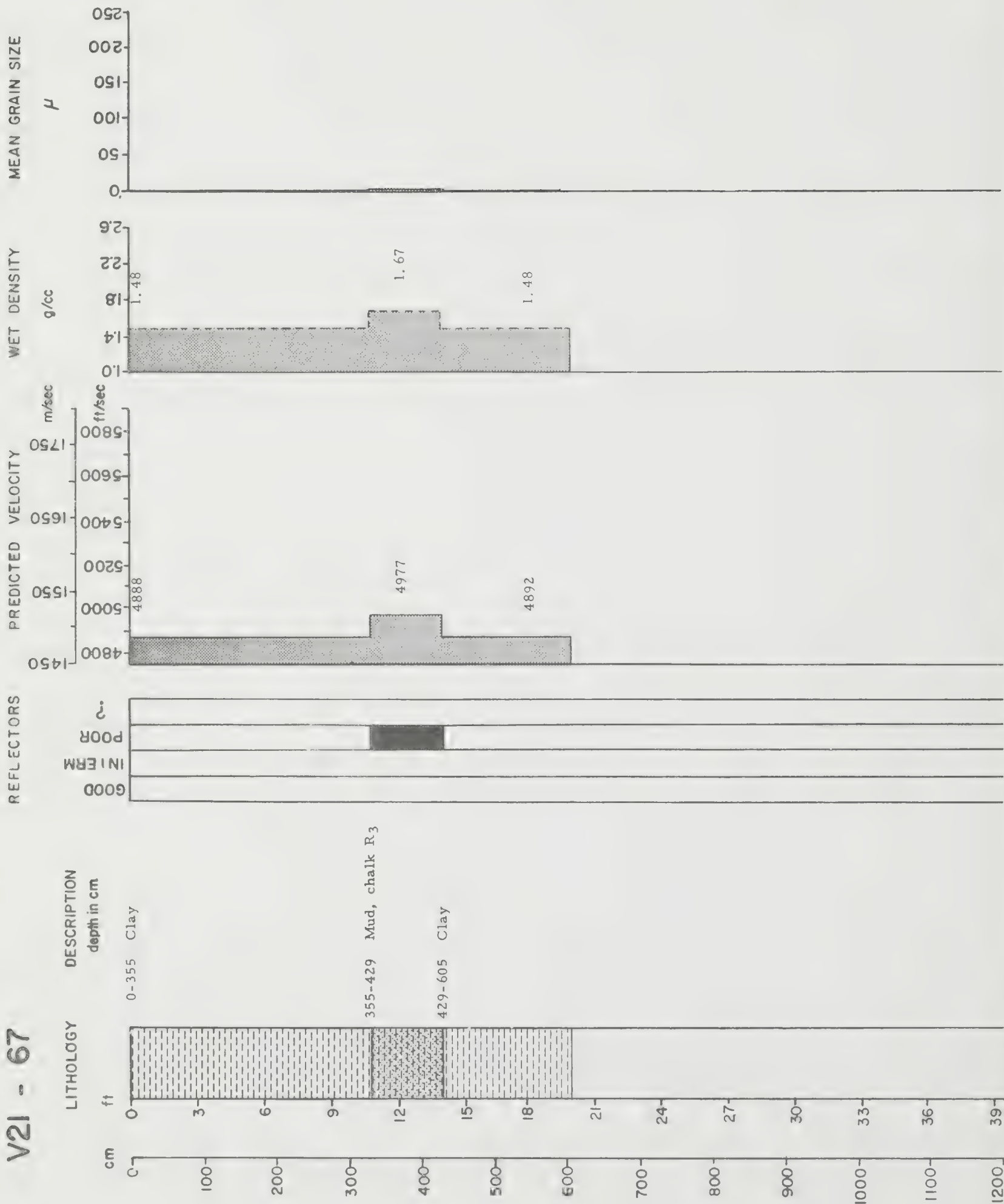
1.0 1.4 1.50 1.66

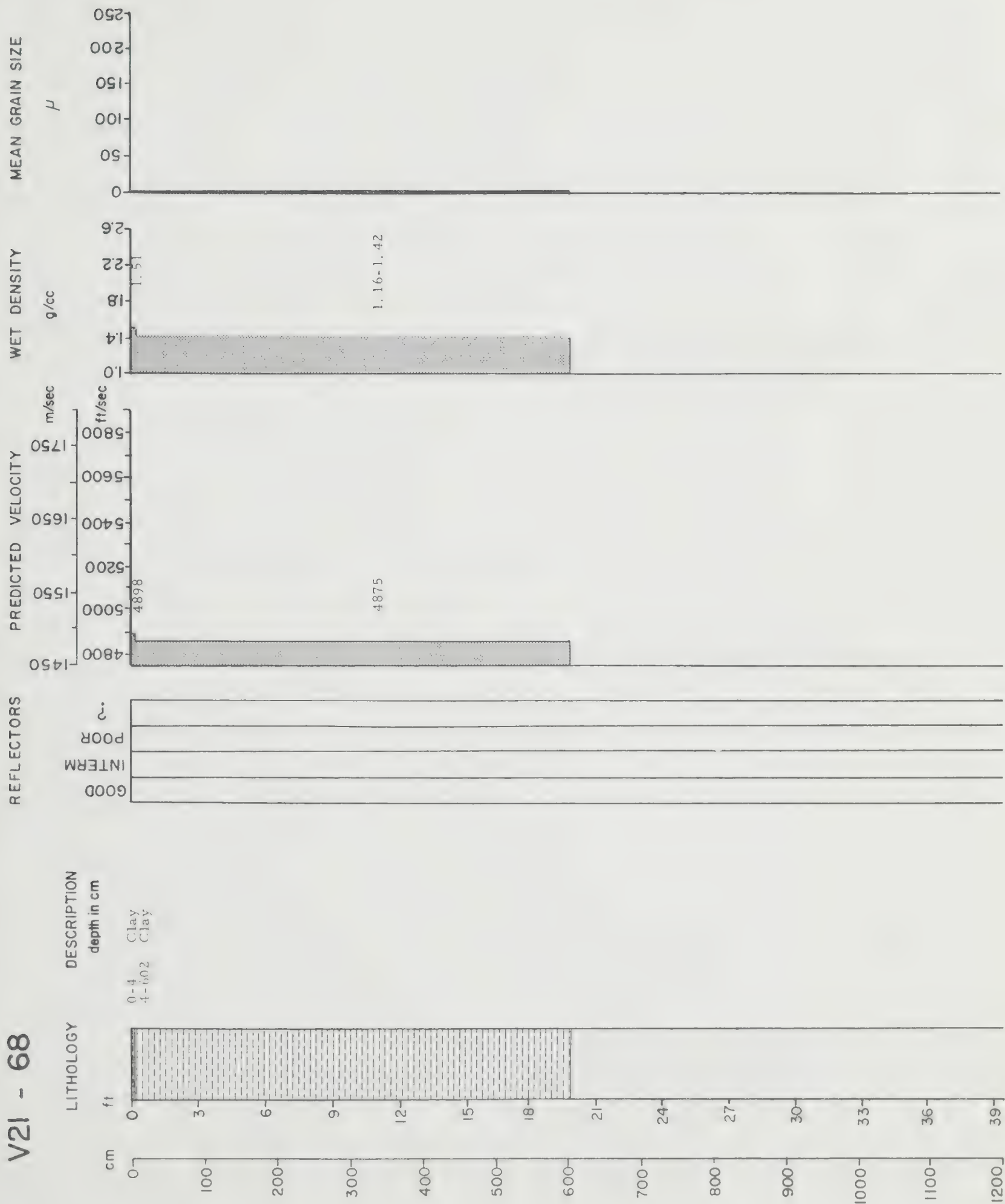
**MEAN GRAIN SIZE**

$\mu$

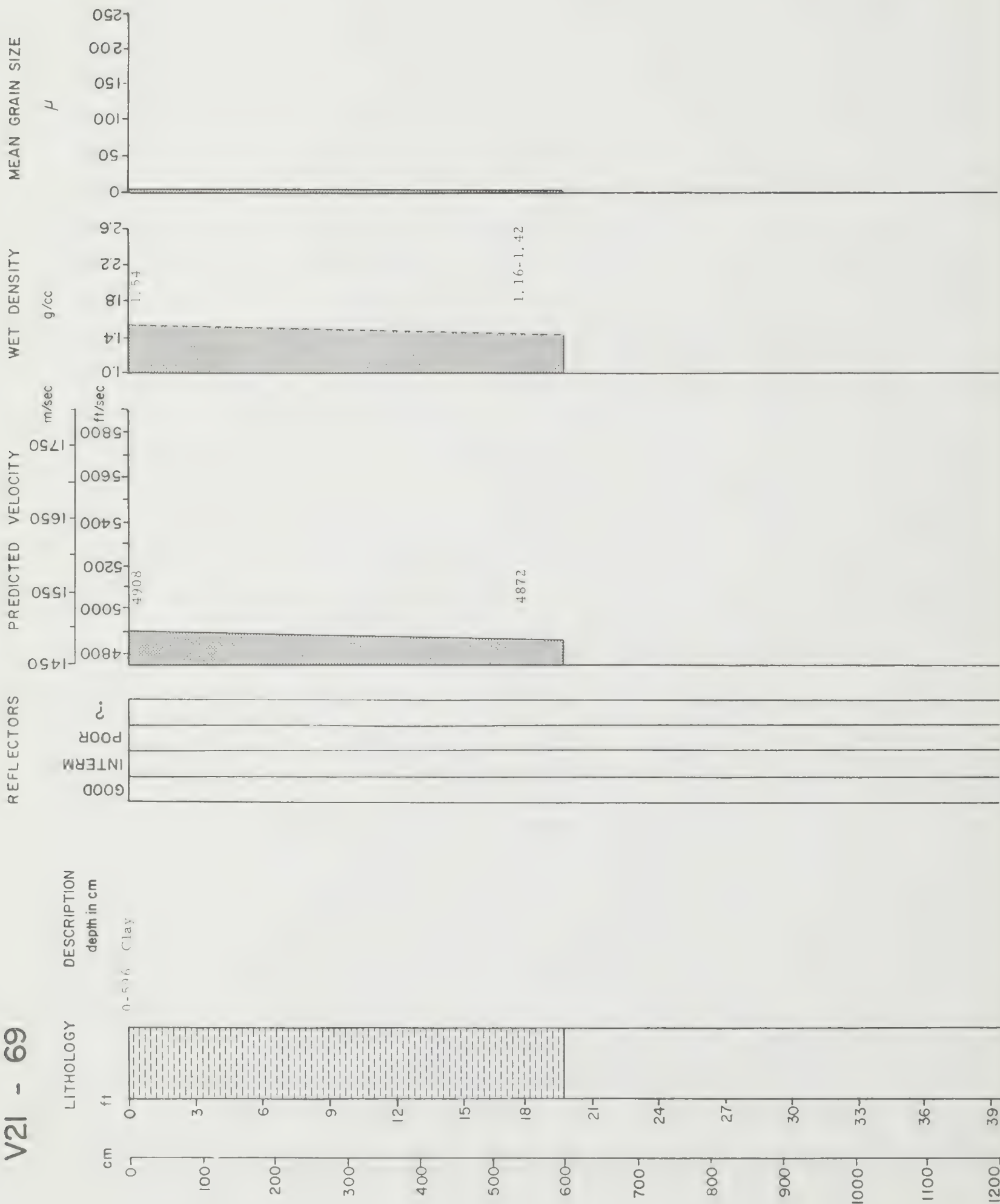
0 50 100 150 200 250

V2I - 67

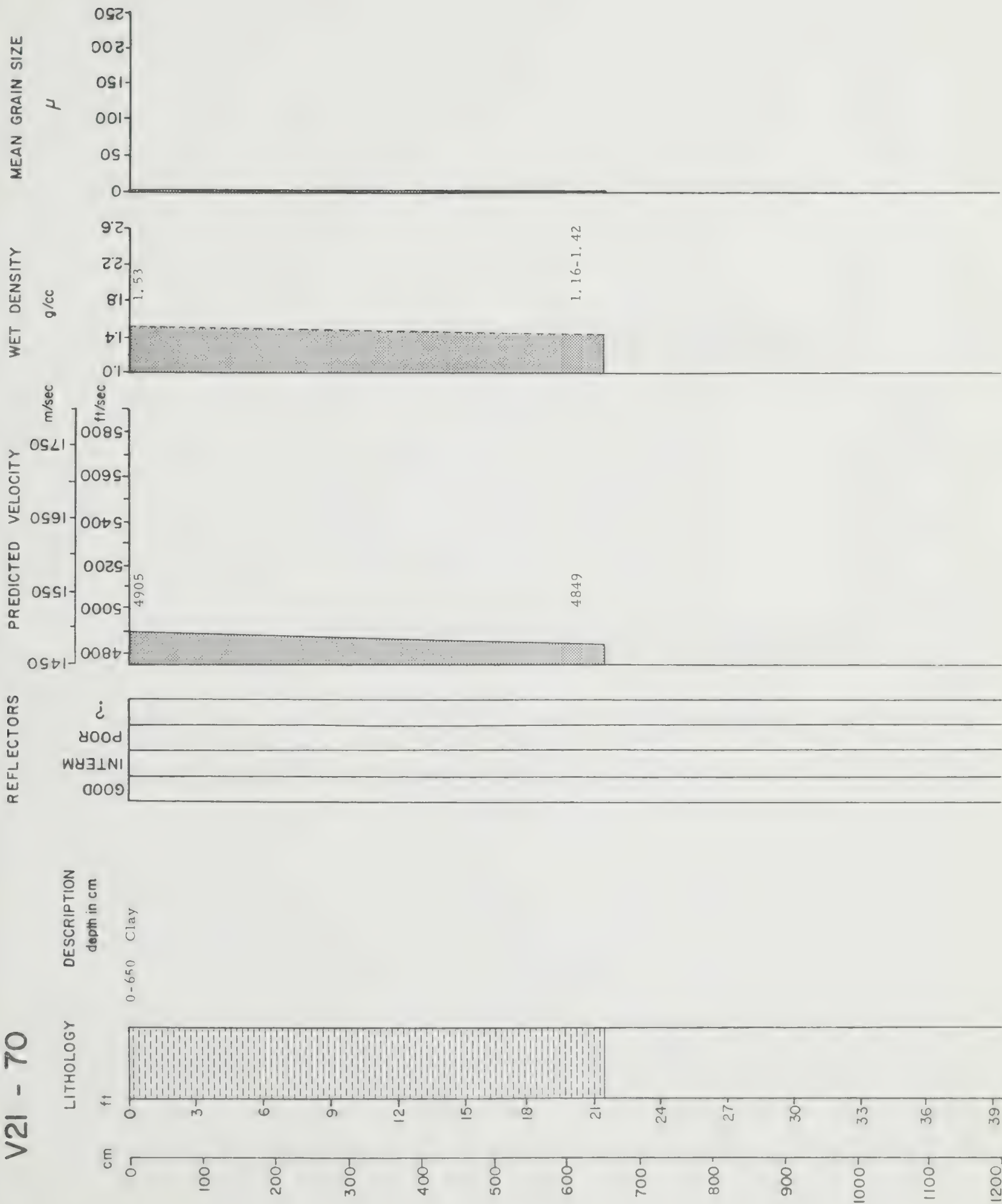


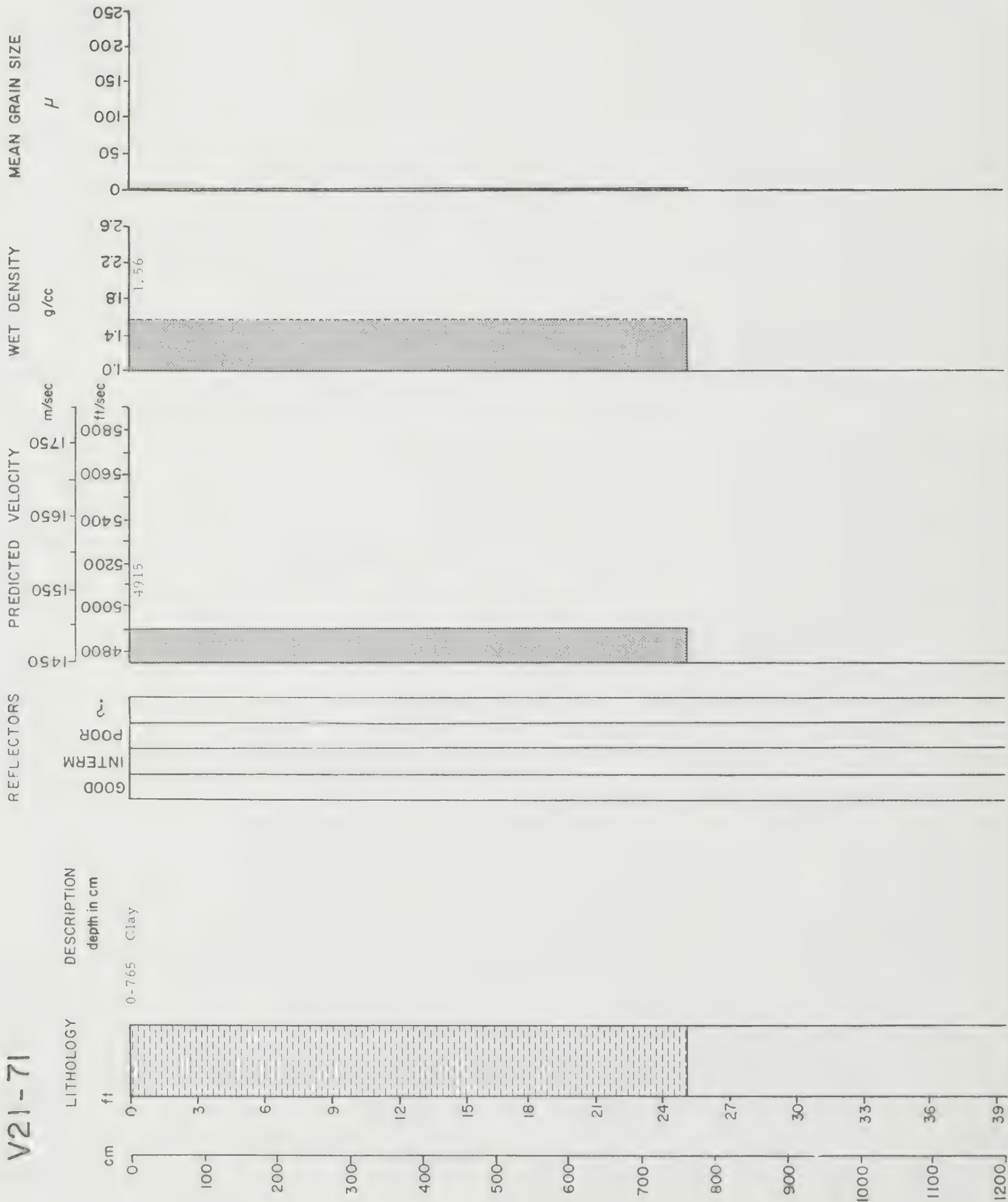


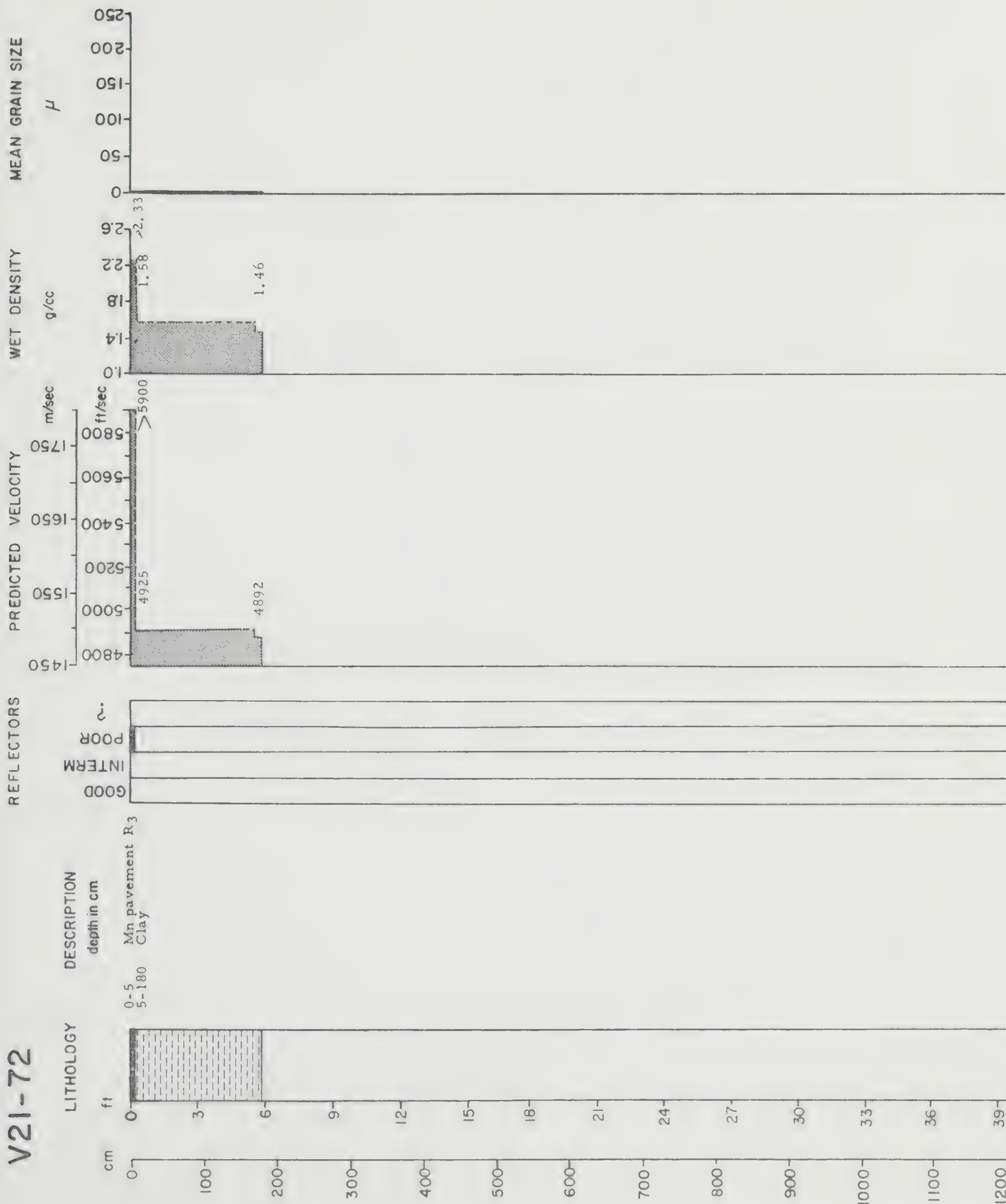
V21 - 69



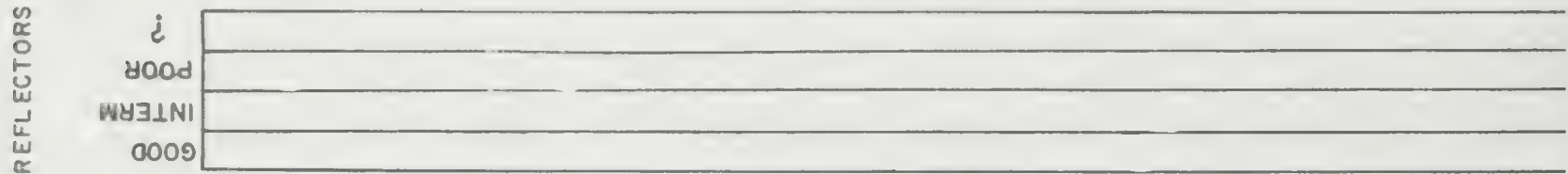
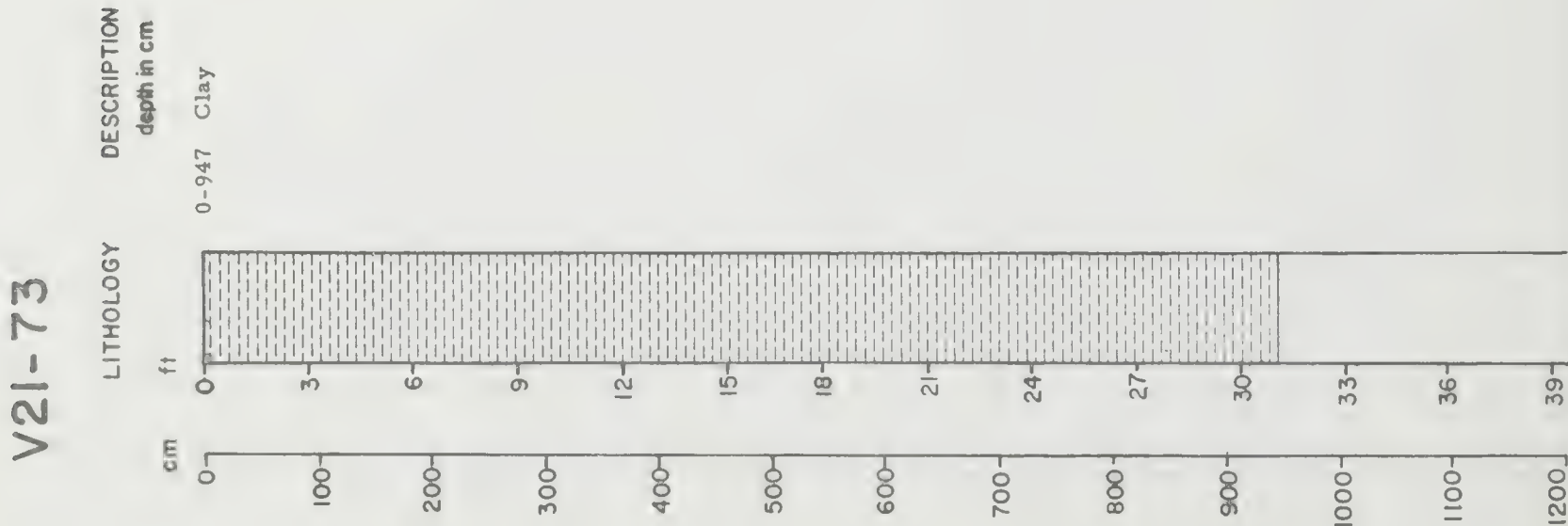






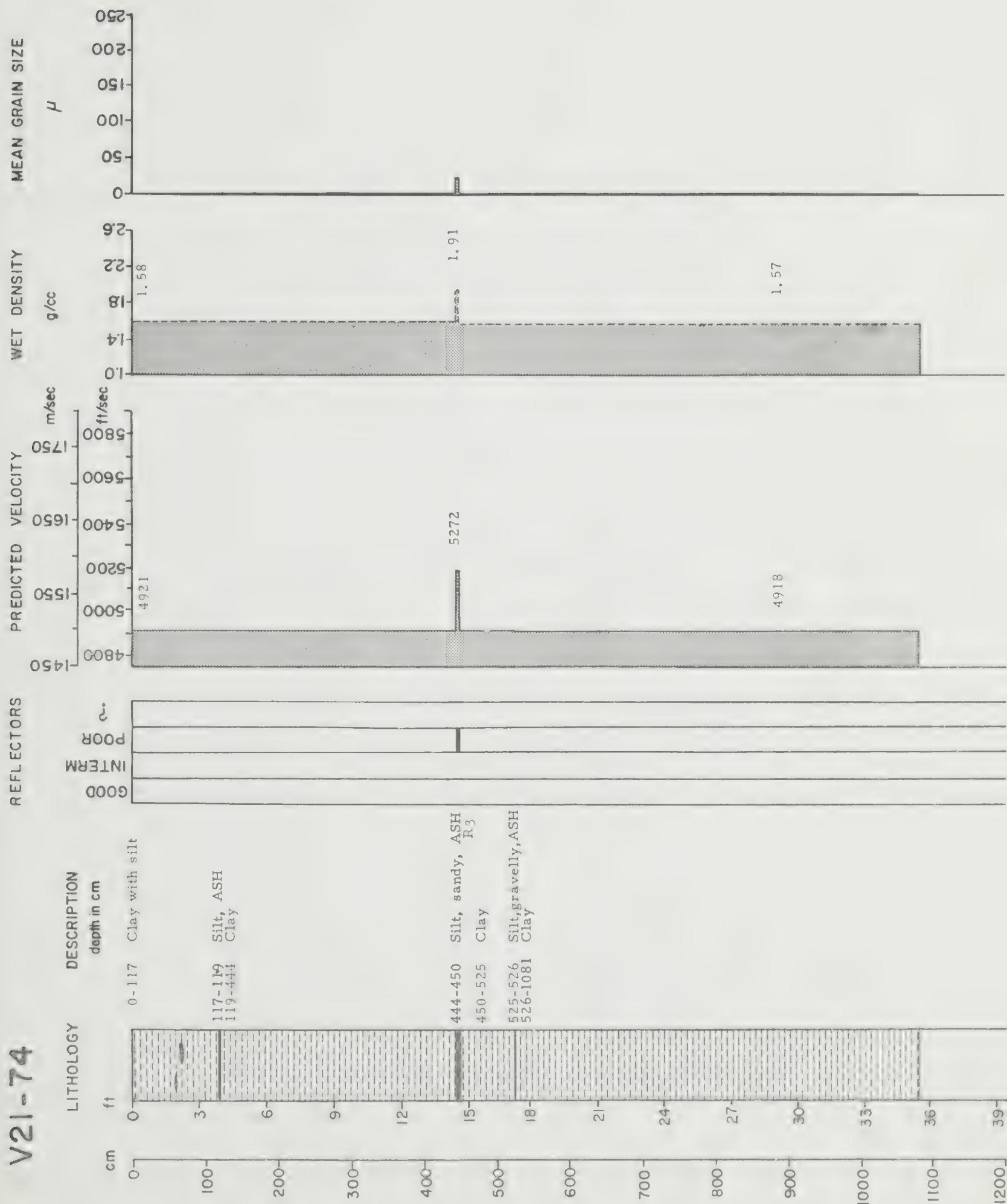


V21-73

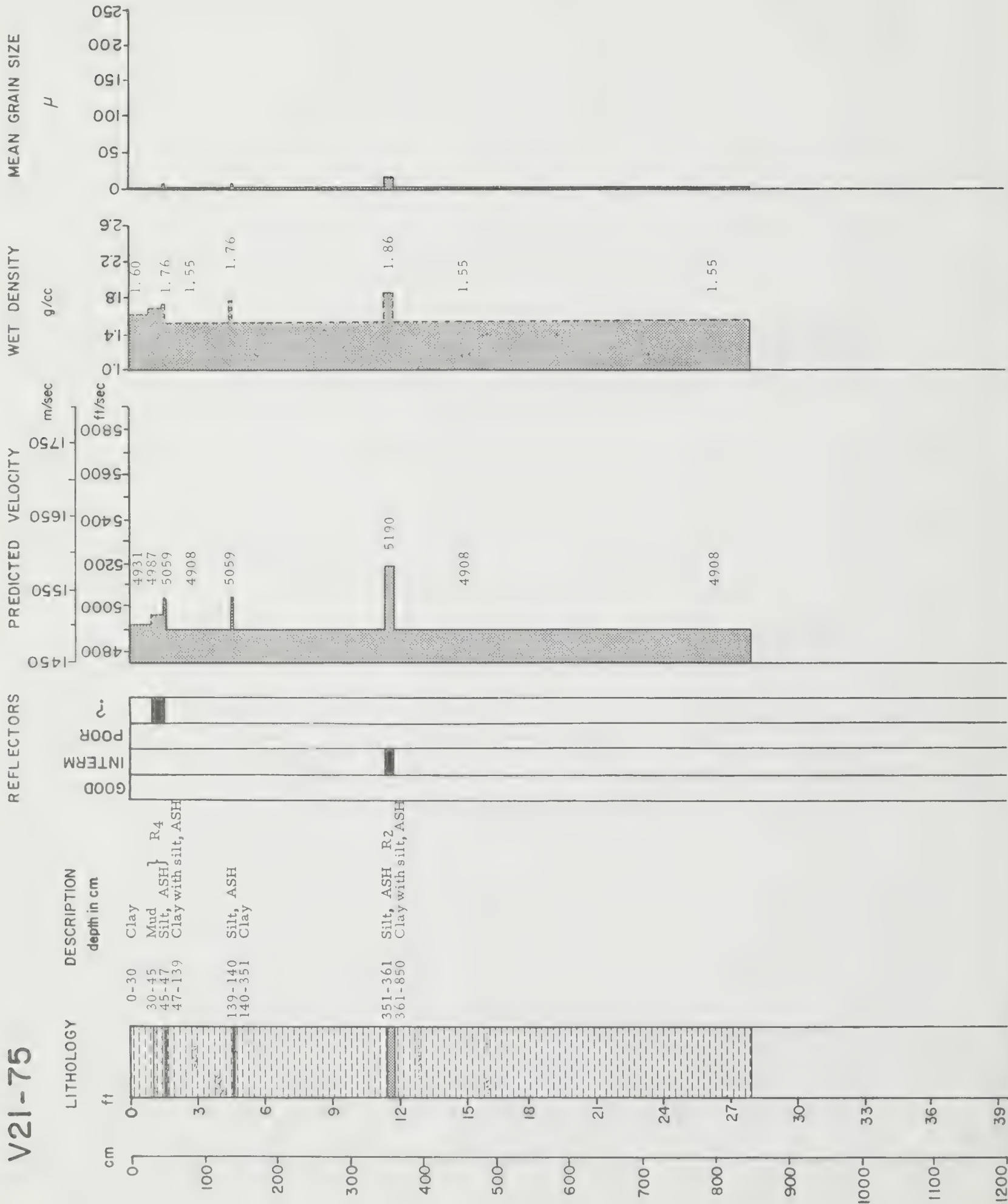




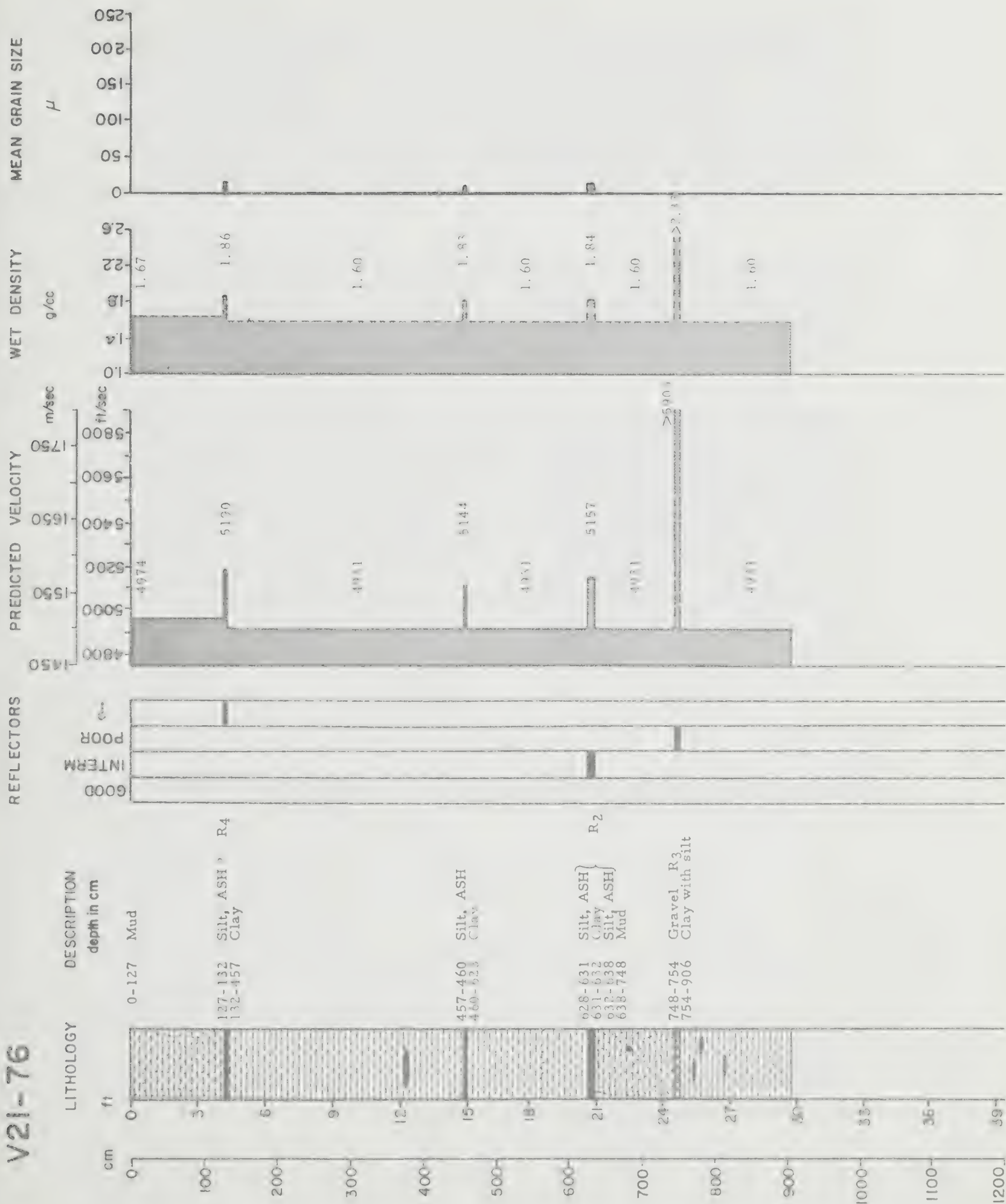
V21-74



V21-75



V21-76



V21-77

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

DESCRIPTION

depth in cm

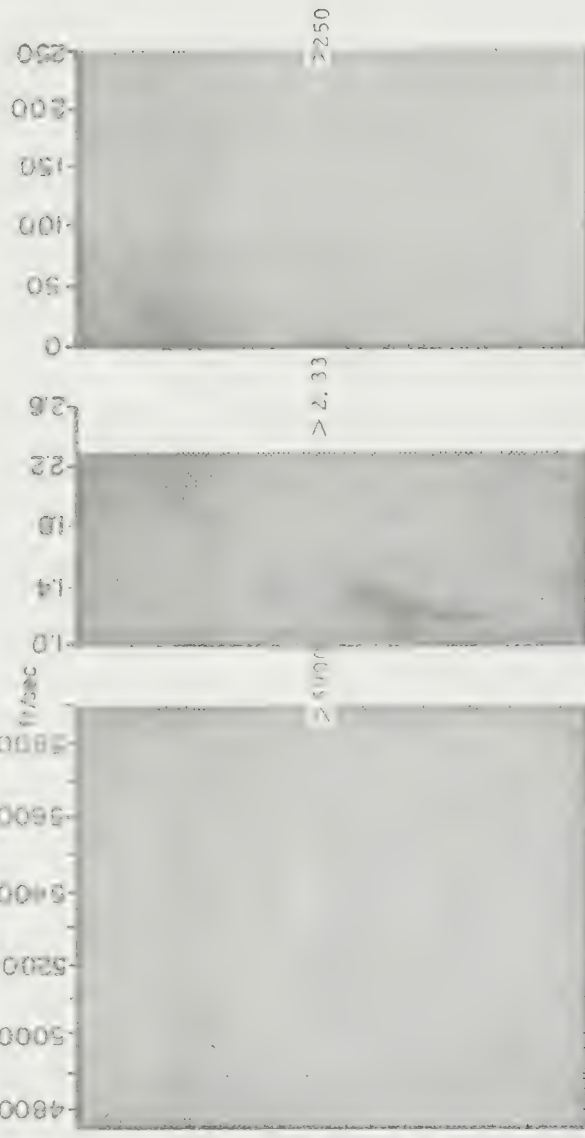
LITHOLOGY

cm

ft

0-30 Sand  
30-420 Gravel, sandy  
R1

GOOD  
INTERM  
POOR



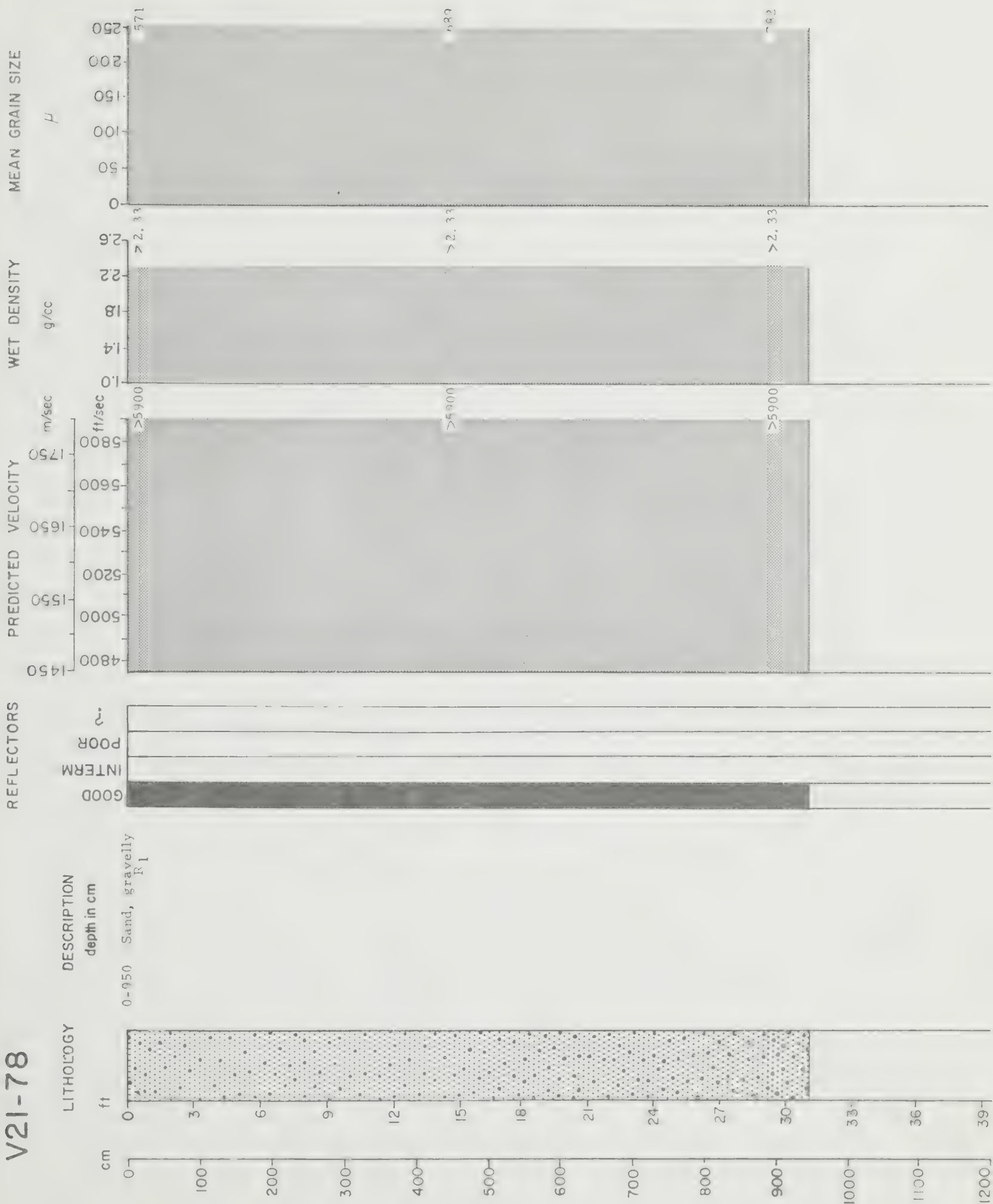
cm

ft

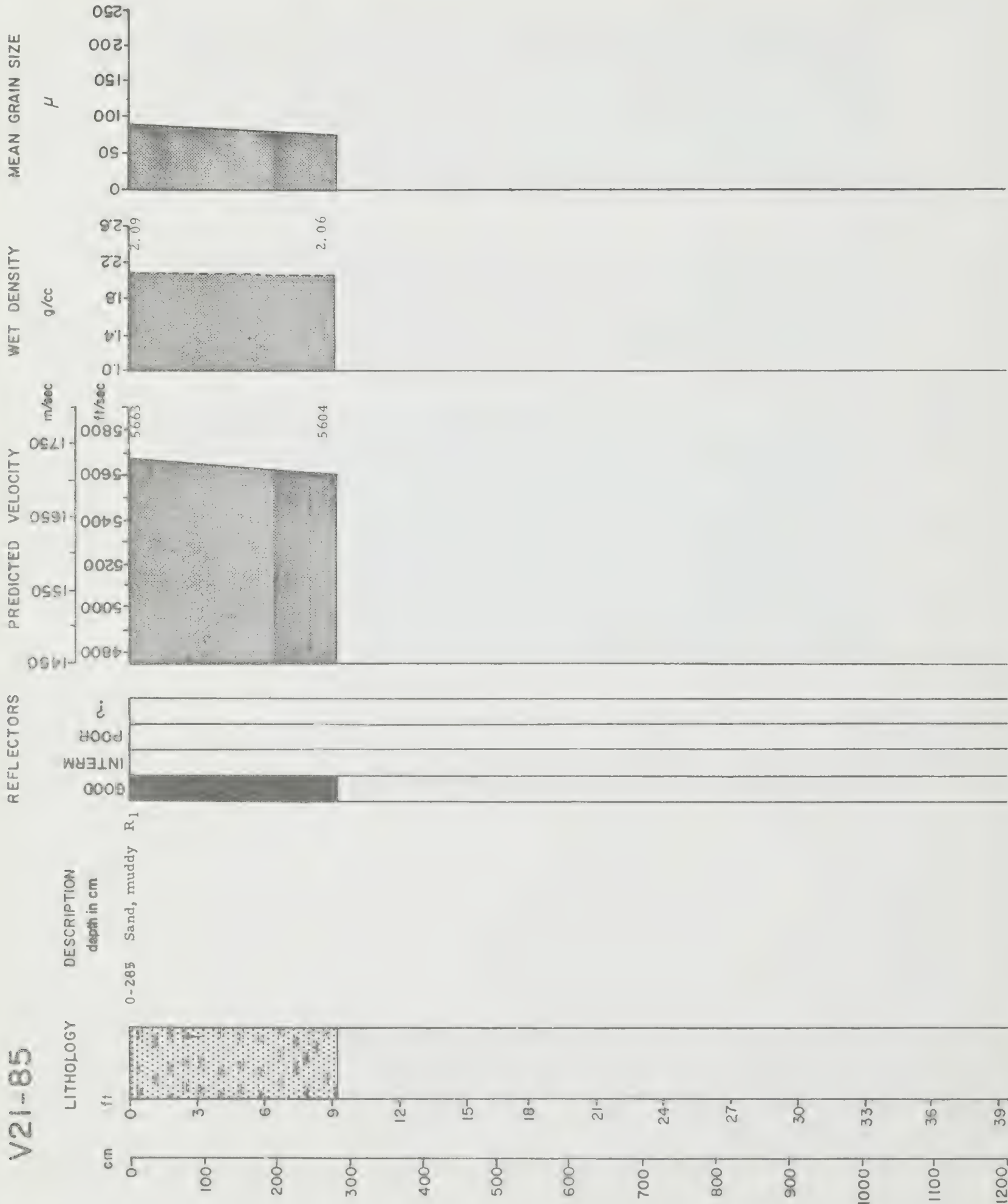
0-30 Sand  
30-420 Gravel, sandy  
R1

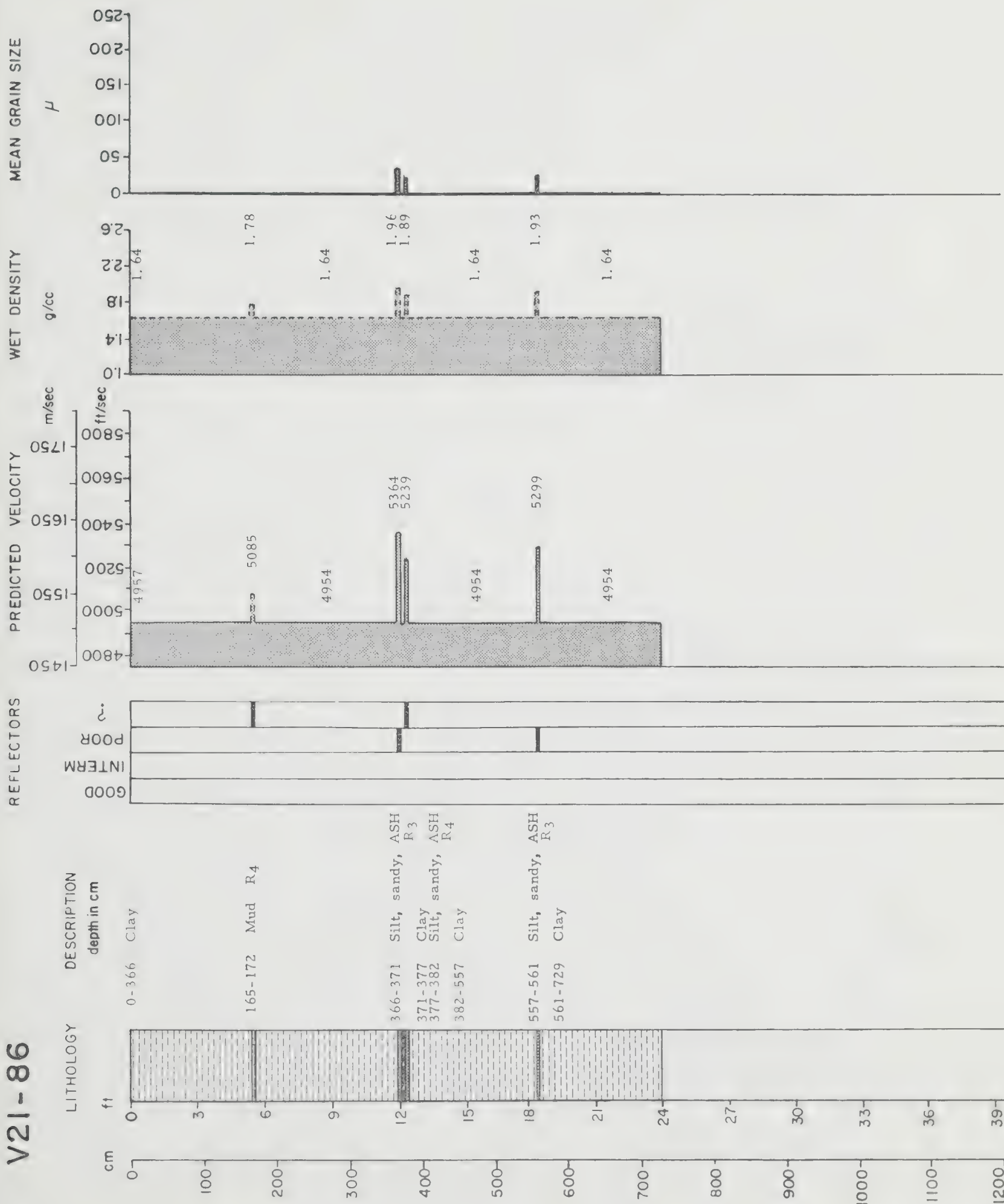
GOOD  
INTERM  
POOR



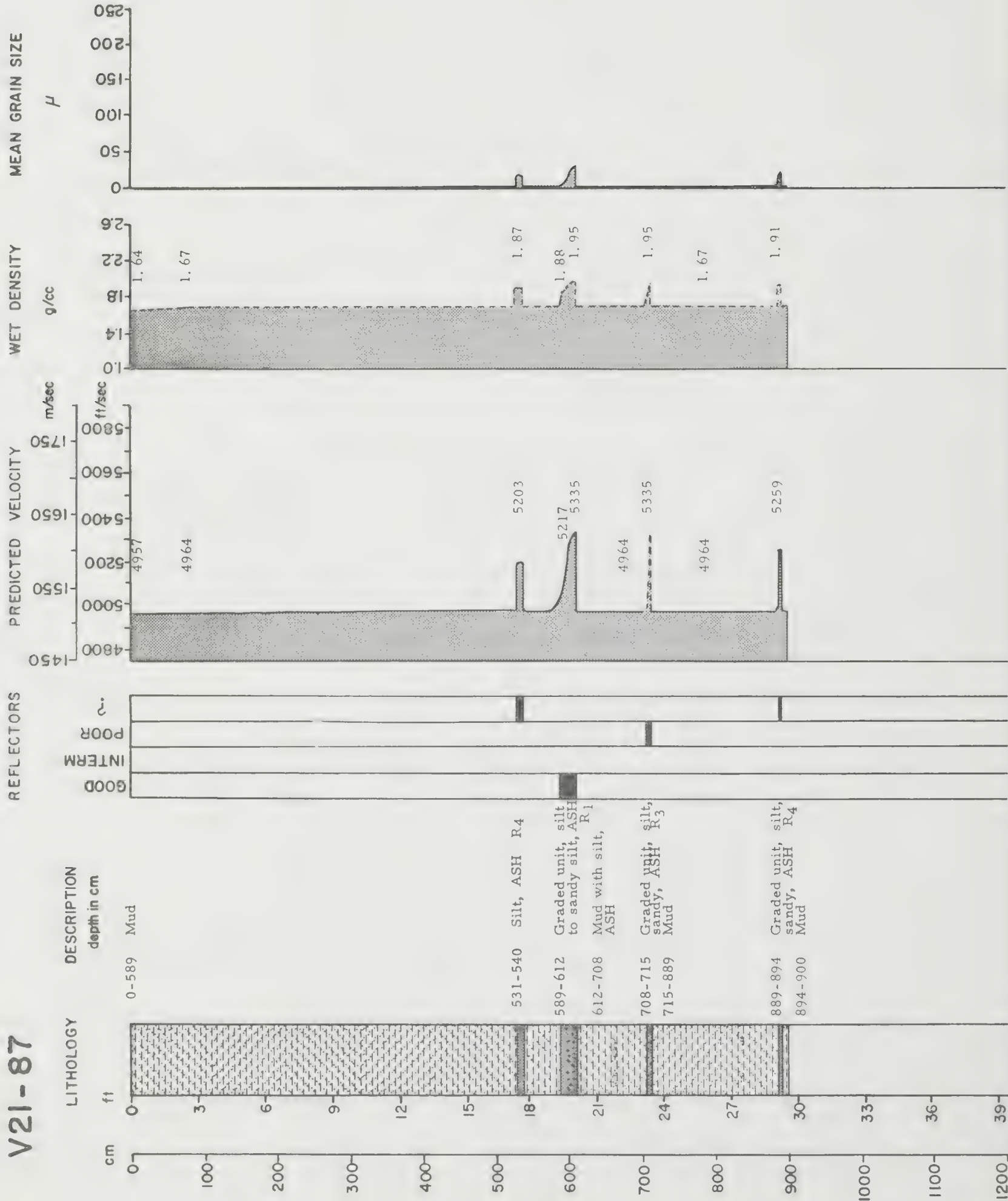


V21-85



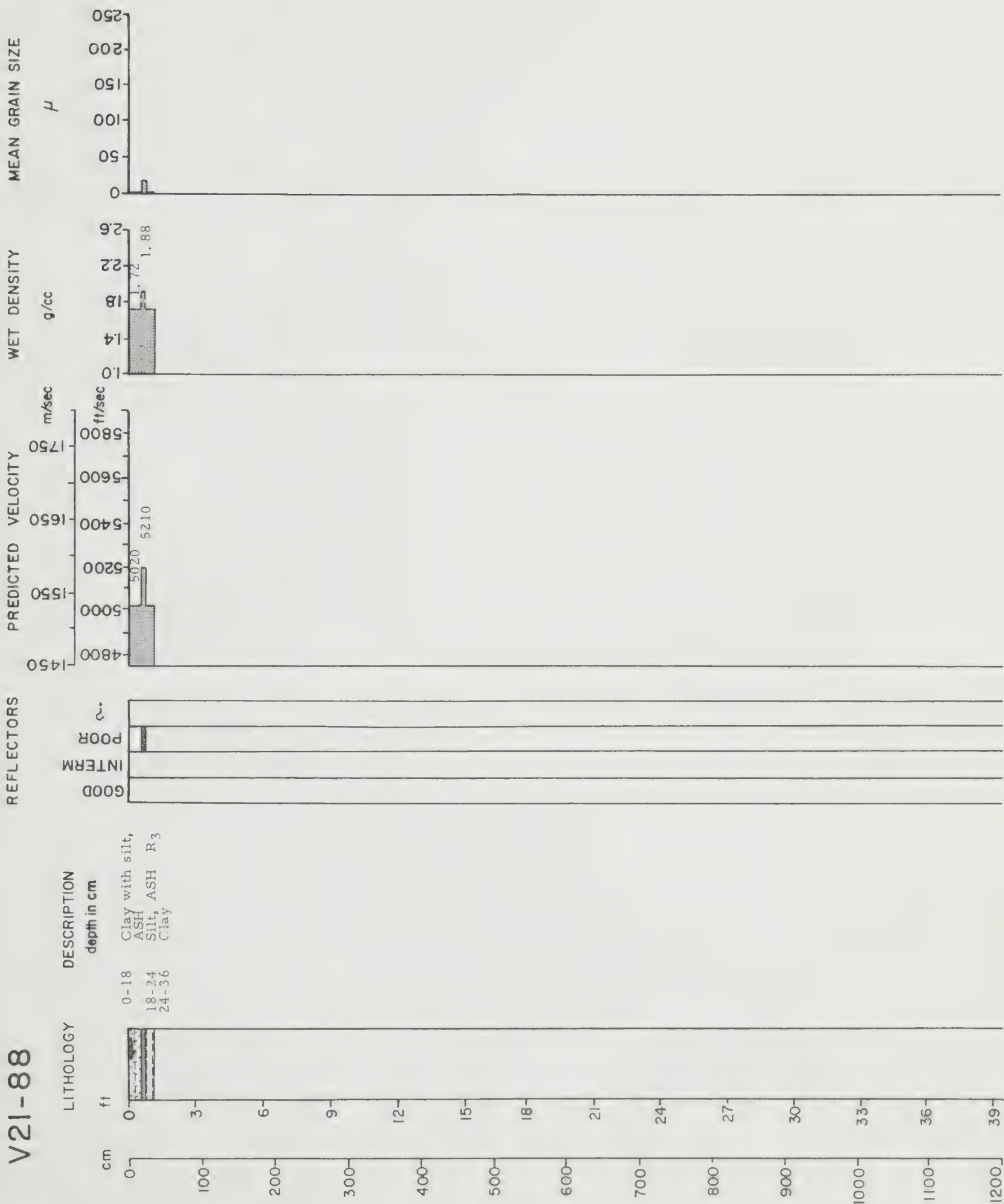


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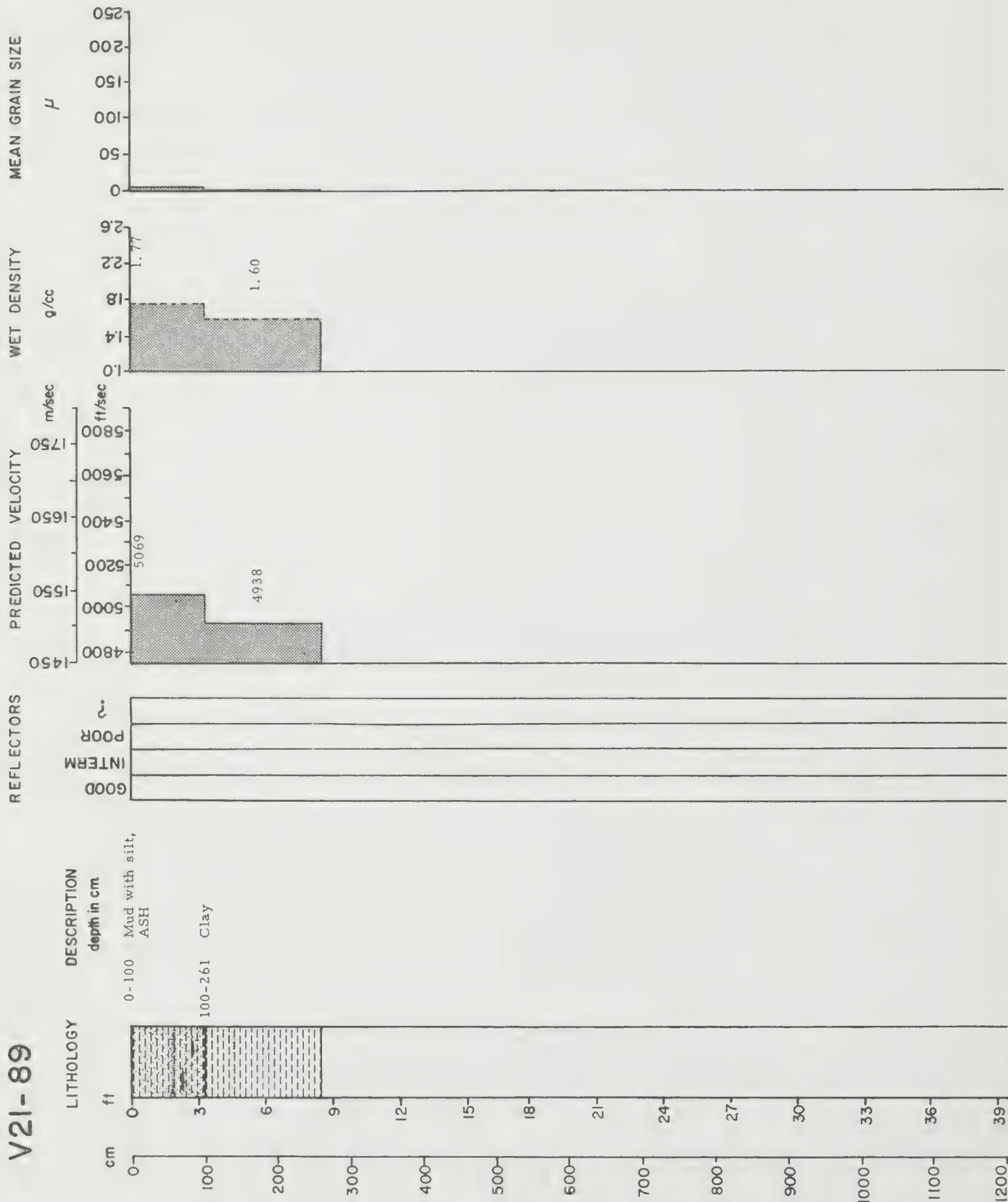




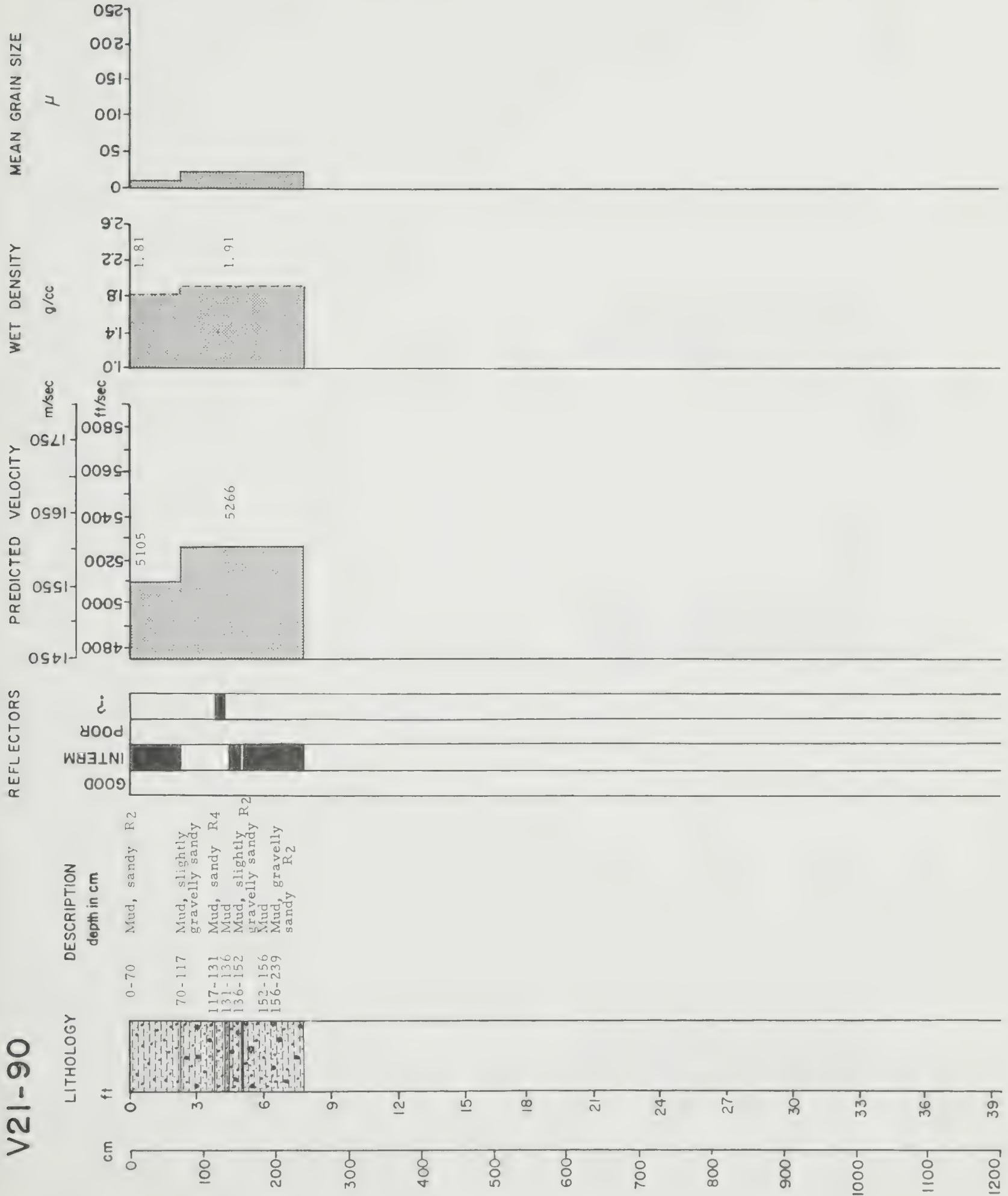
V21-88



V21-89



V21-90



# V21-91

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

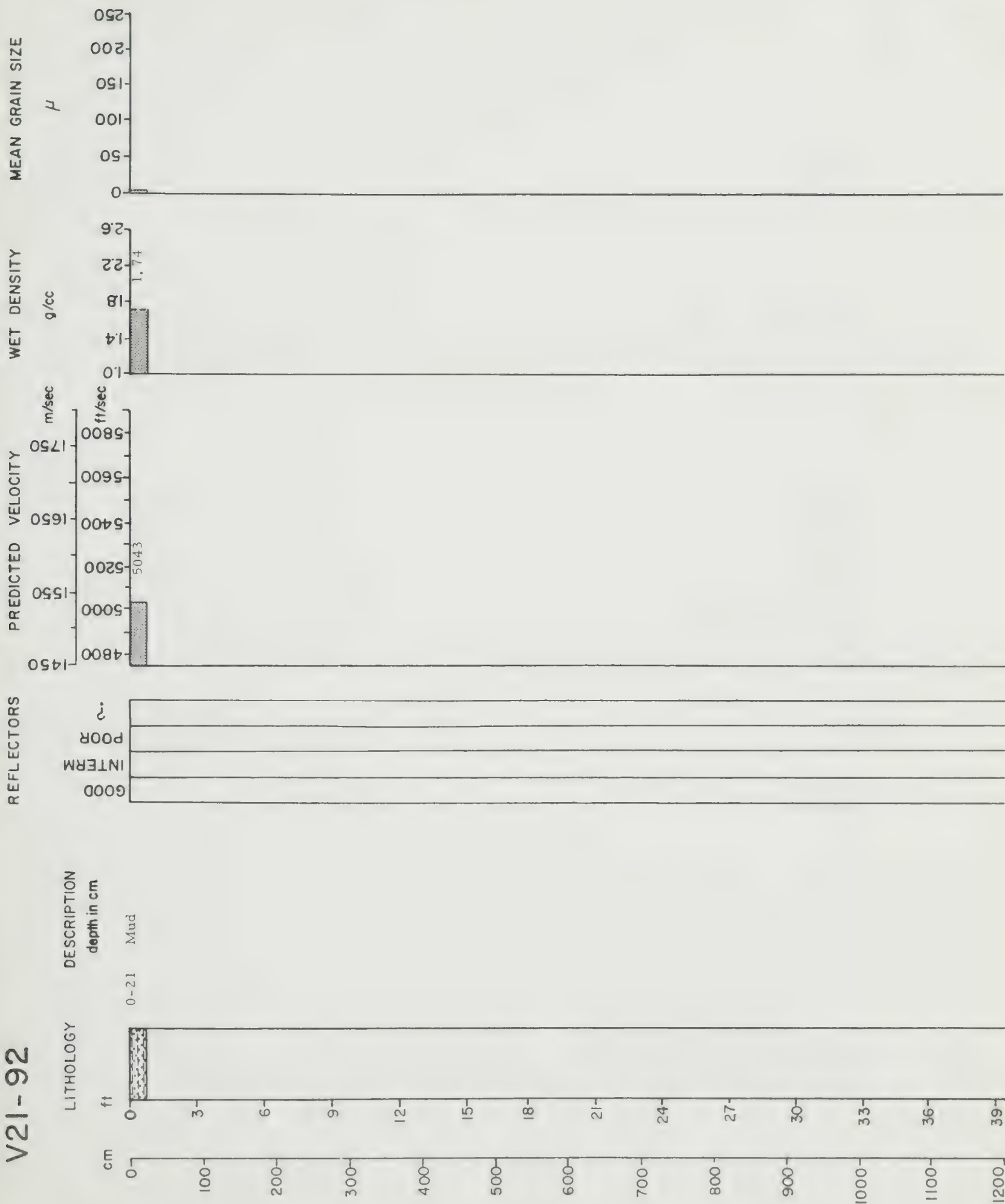
MEAN GRAIN SIZE

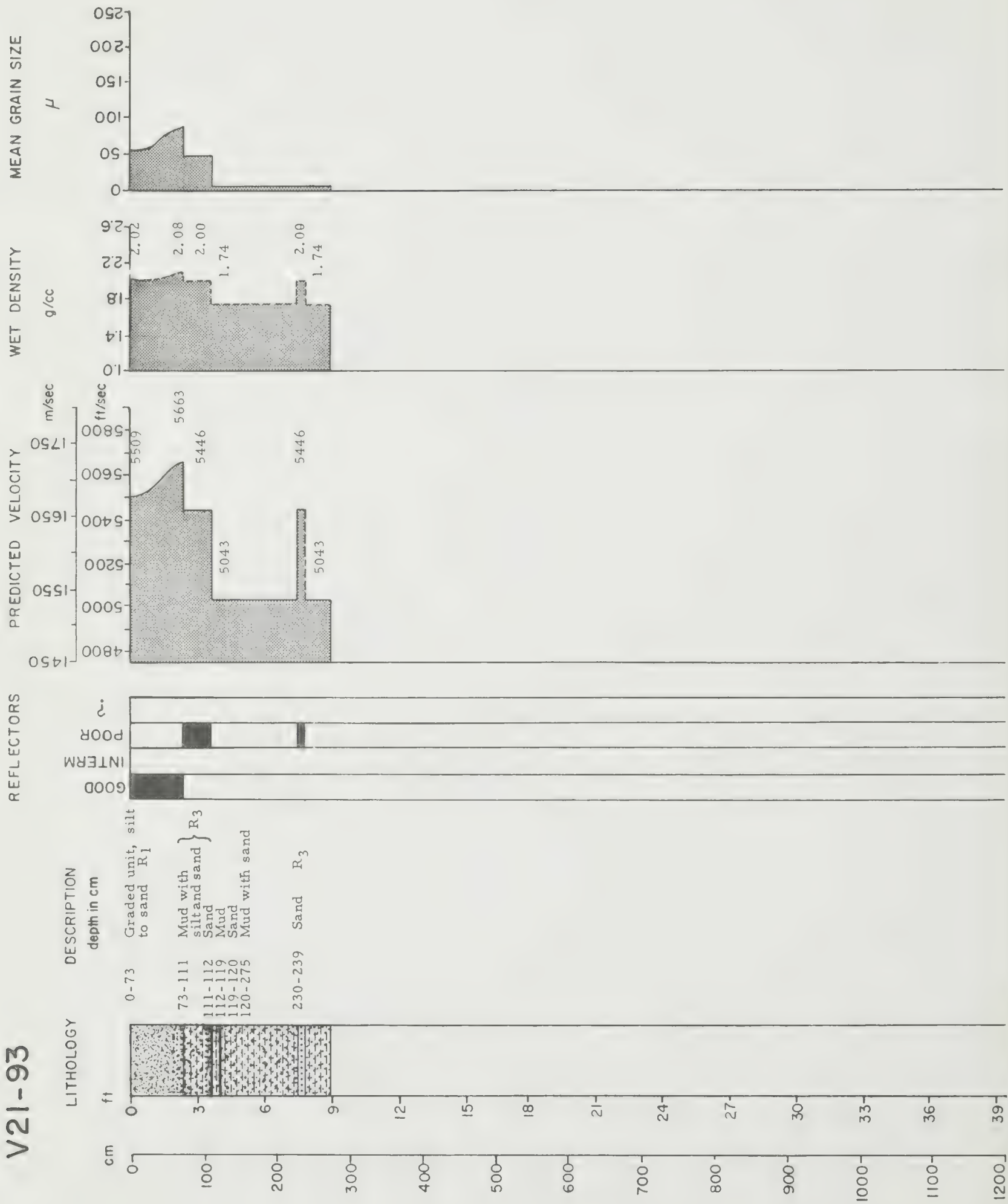
LITHOLOGY	DESCRIPTION	depth in cm
0-8	Silt	
8-23	Graded unit, mud to silt	
9-23	Silt R3	
23-59	Mud	
59-178	Mud with silt	
178-184	Silt, ASH R3	
184-213	Mud	
213-228	Silt, ASH R2	
228-306	Mud	
306-308	Sand, ASH ?	
308-379	Mud	

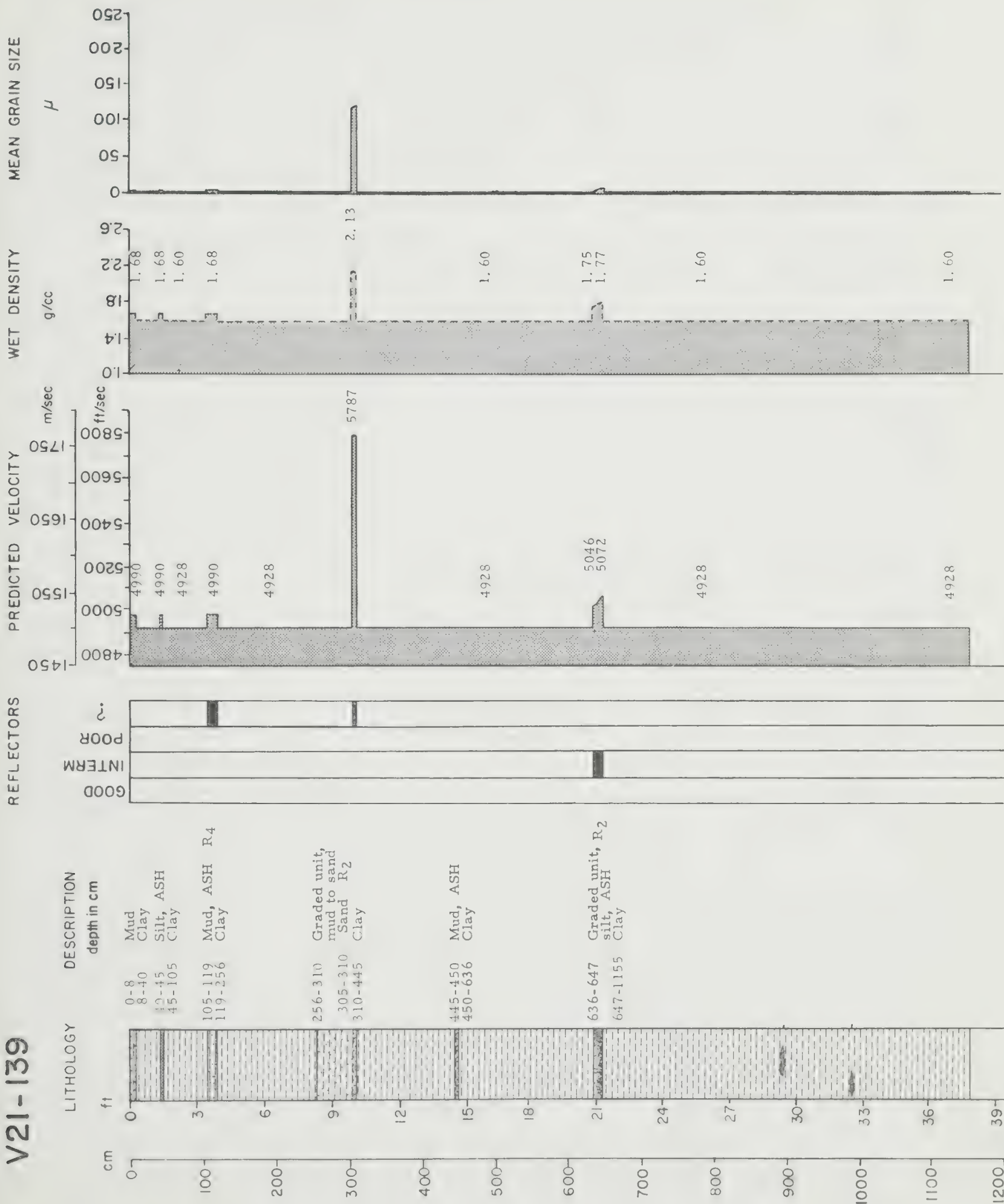




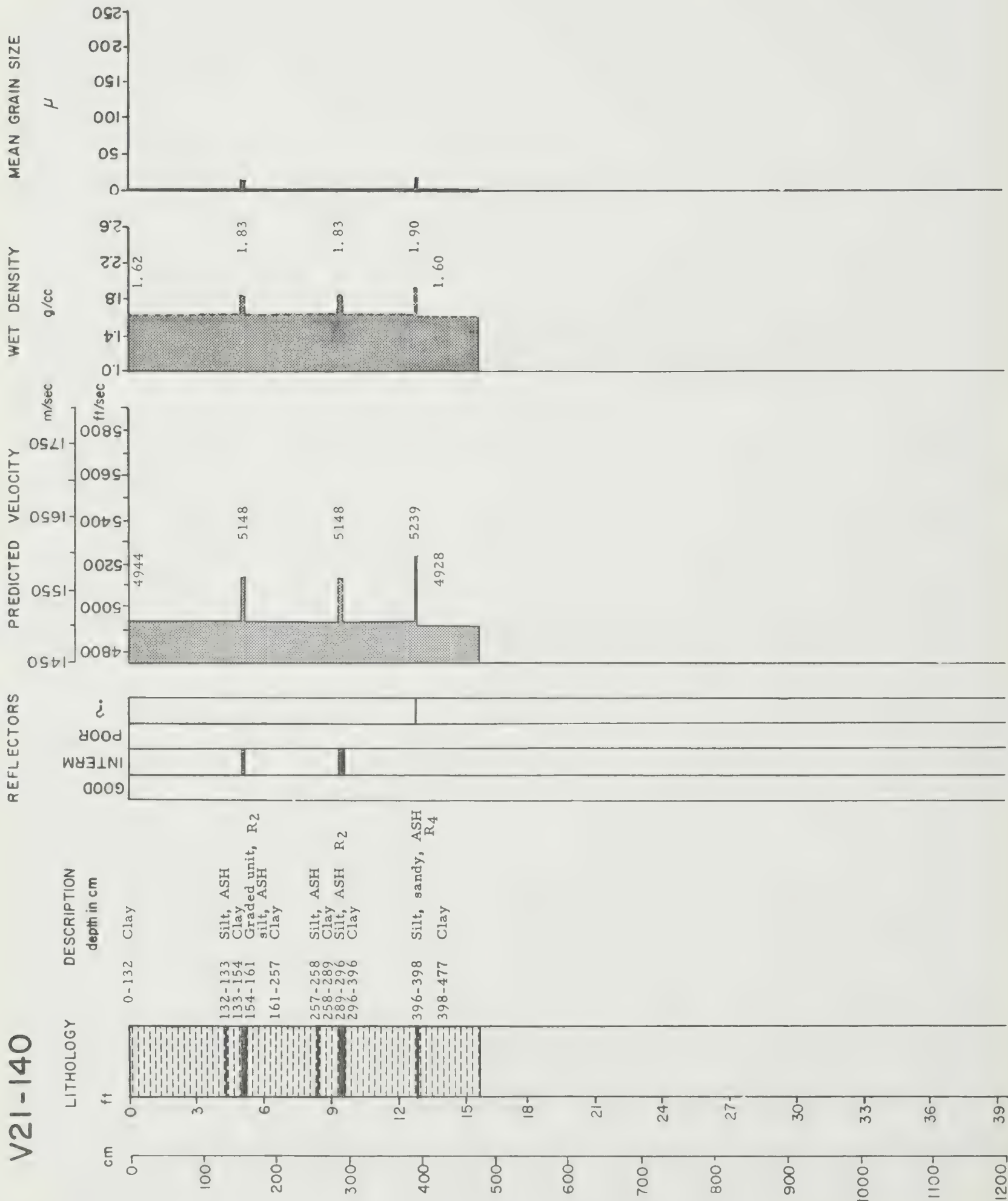
V21-92



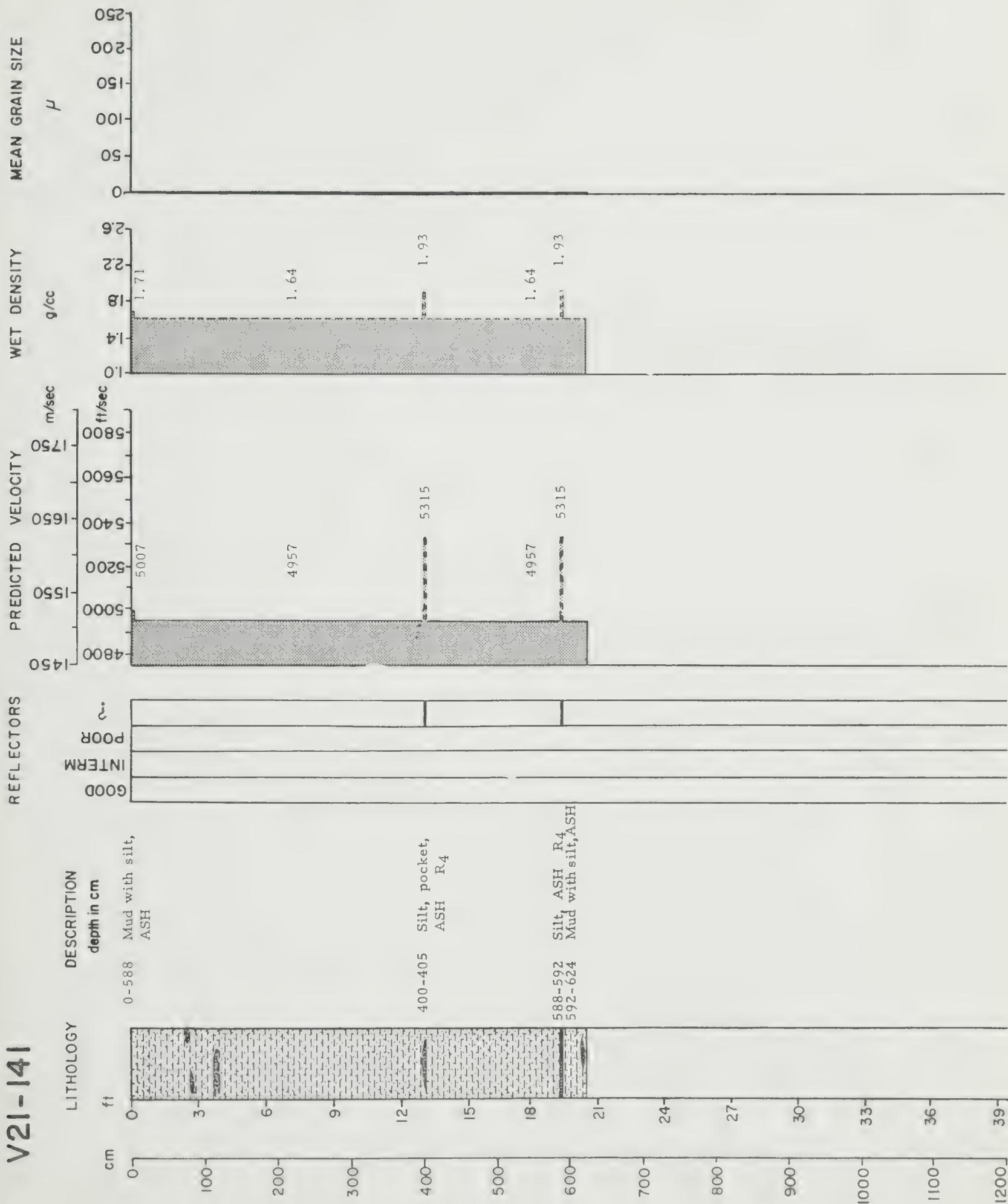




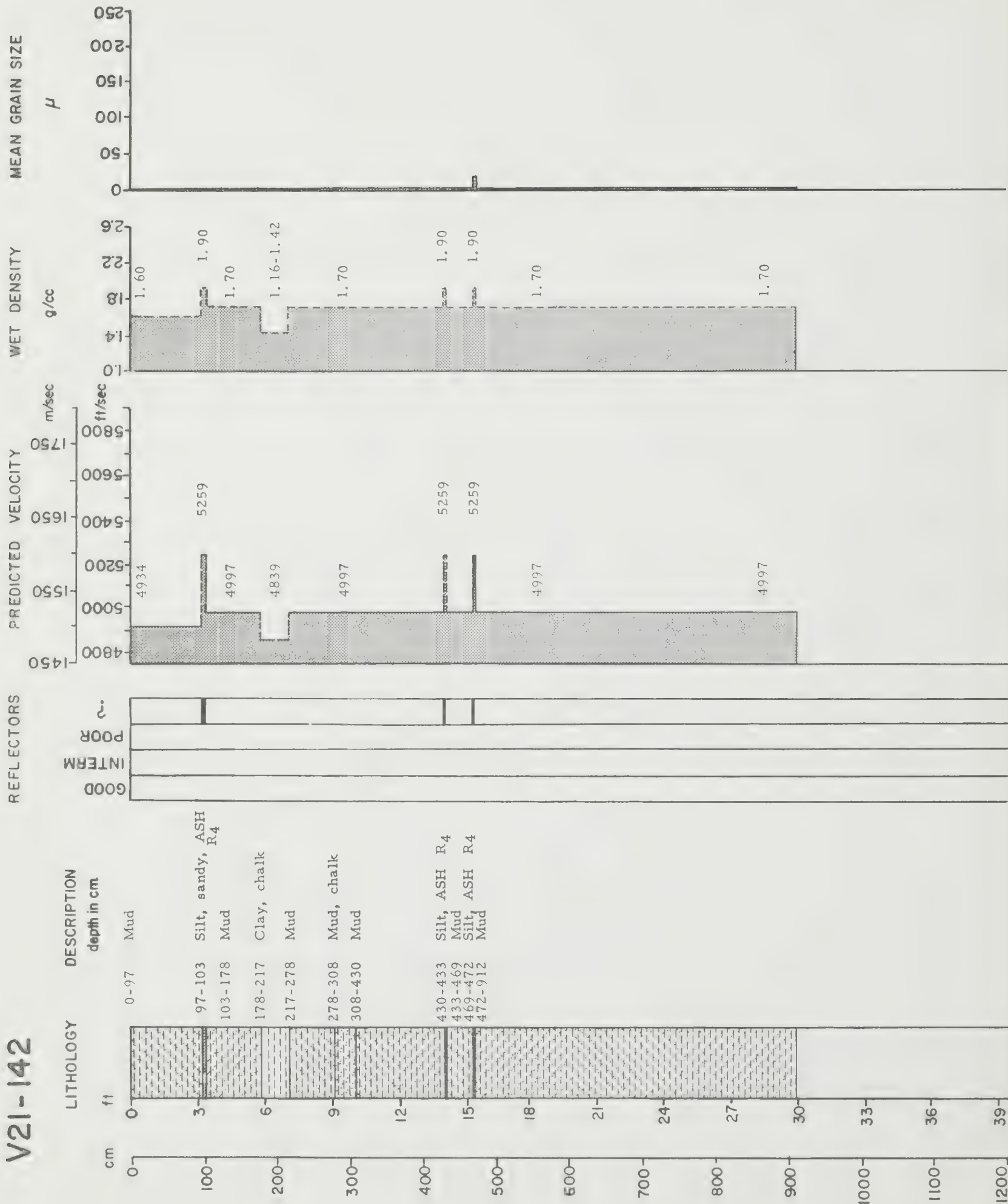
# V21-140

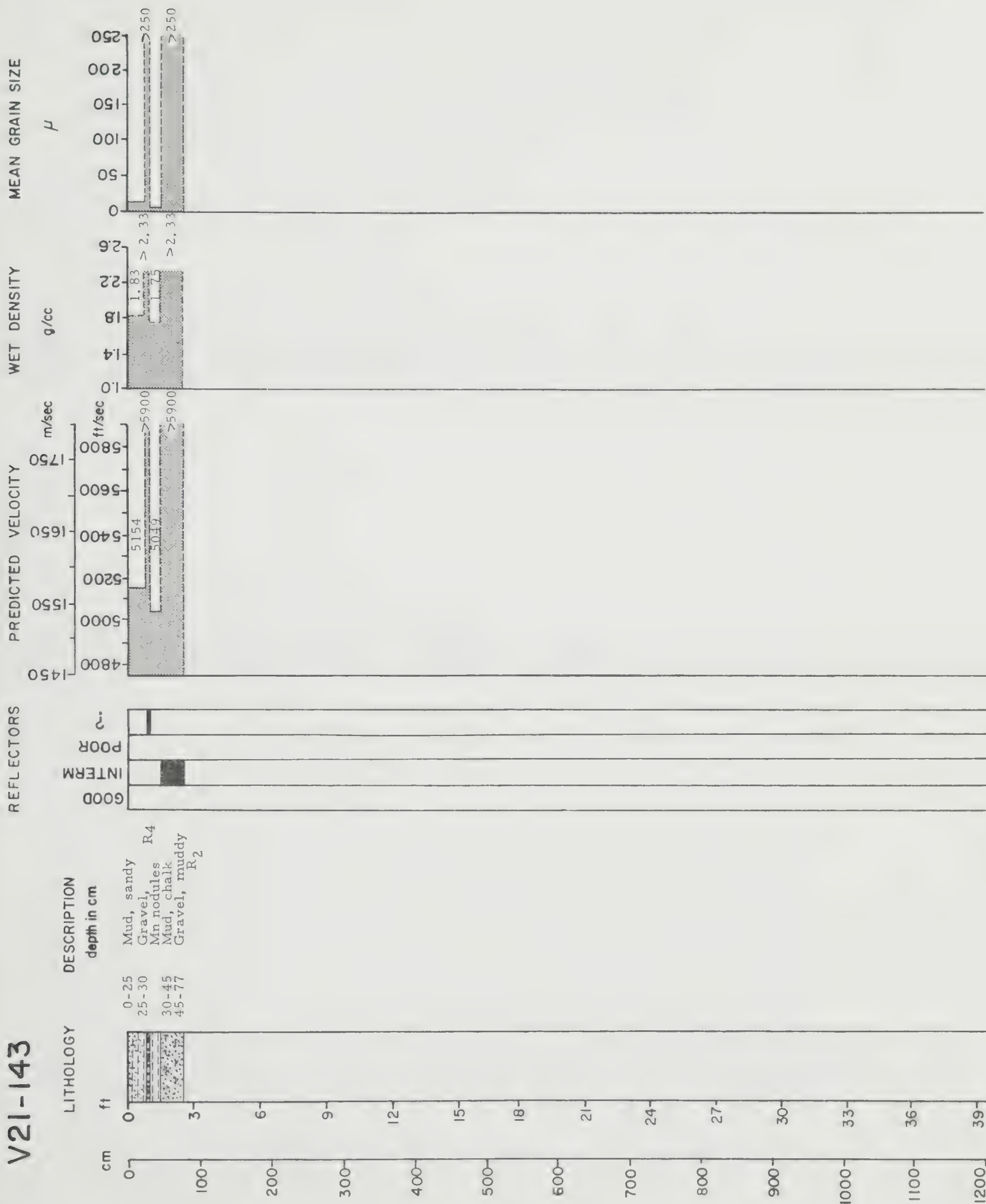


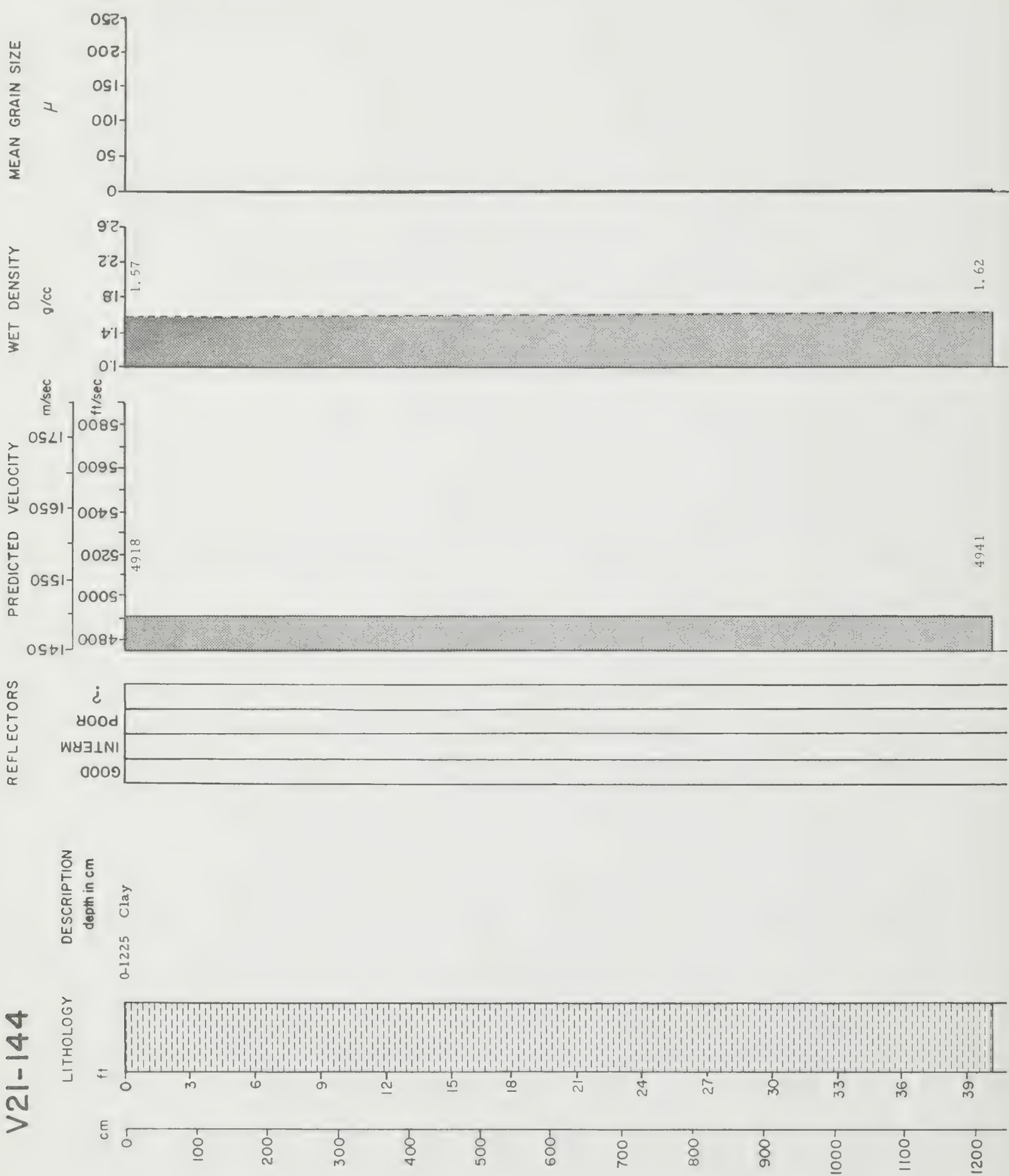




V21-142

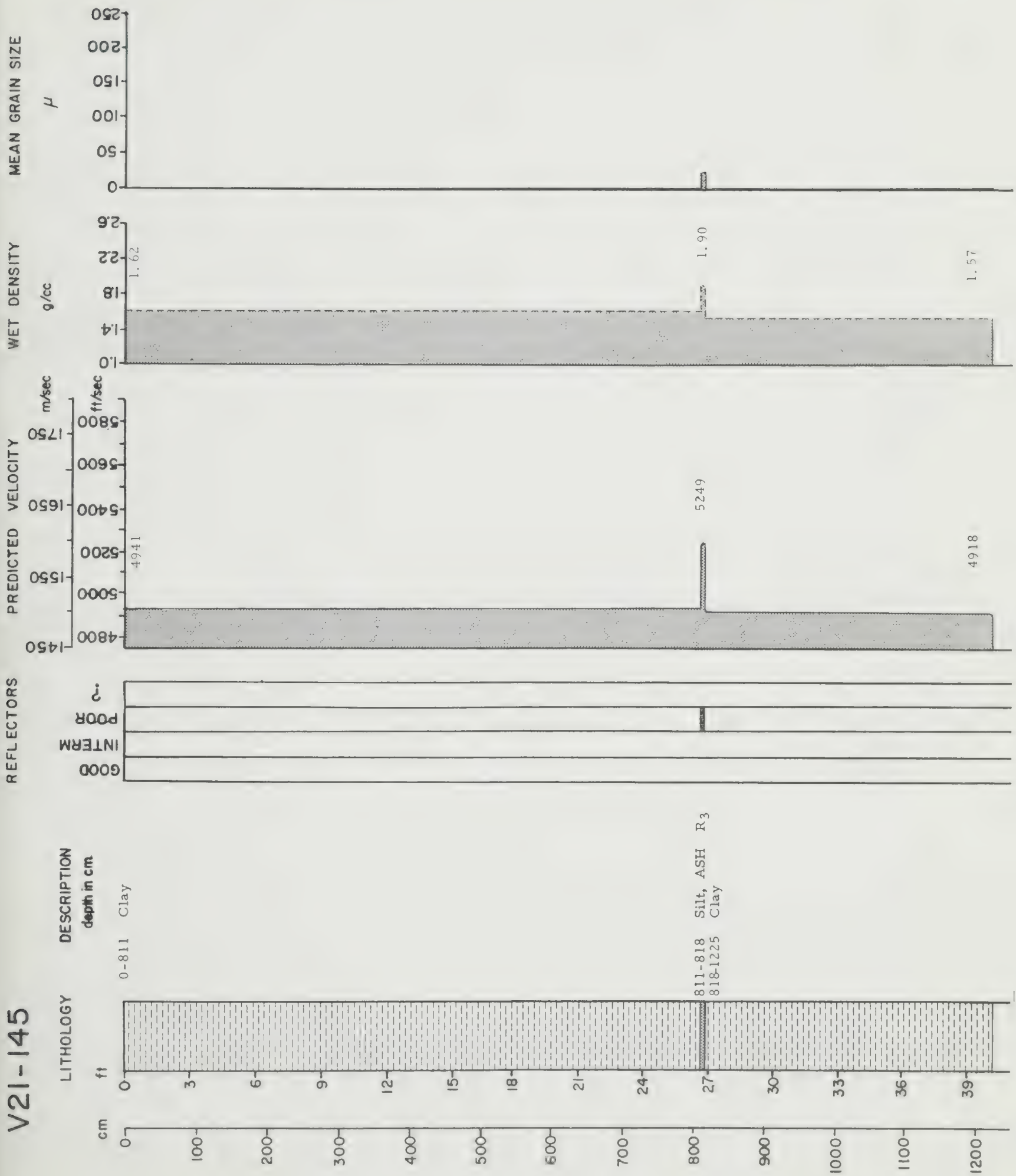




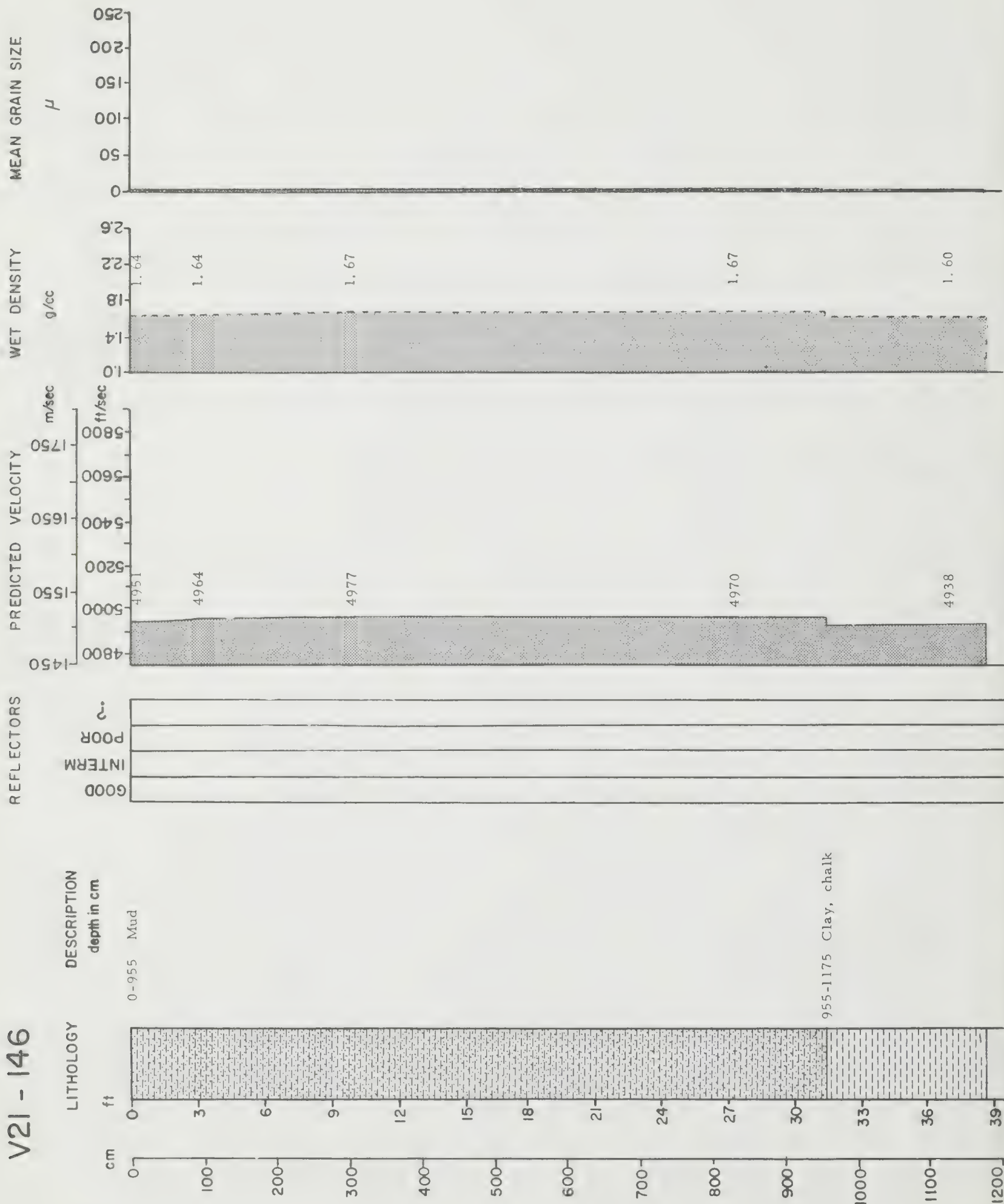




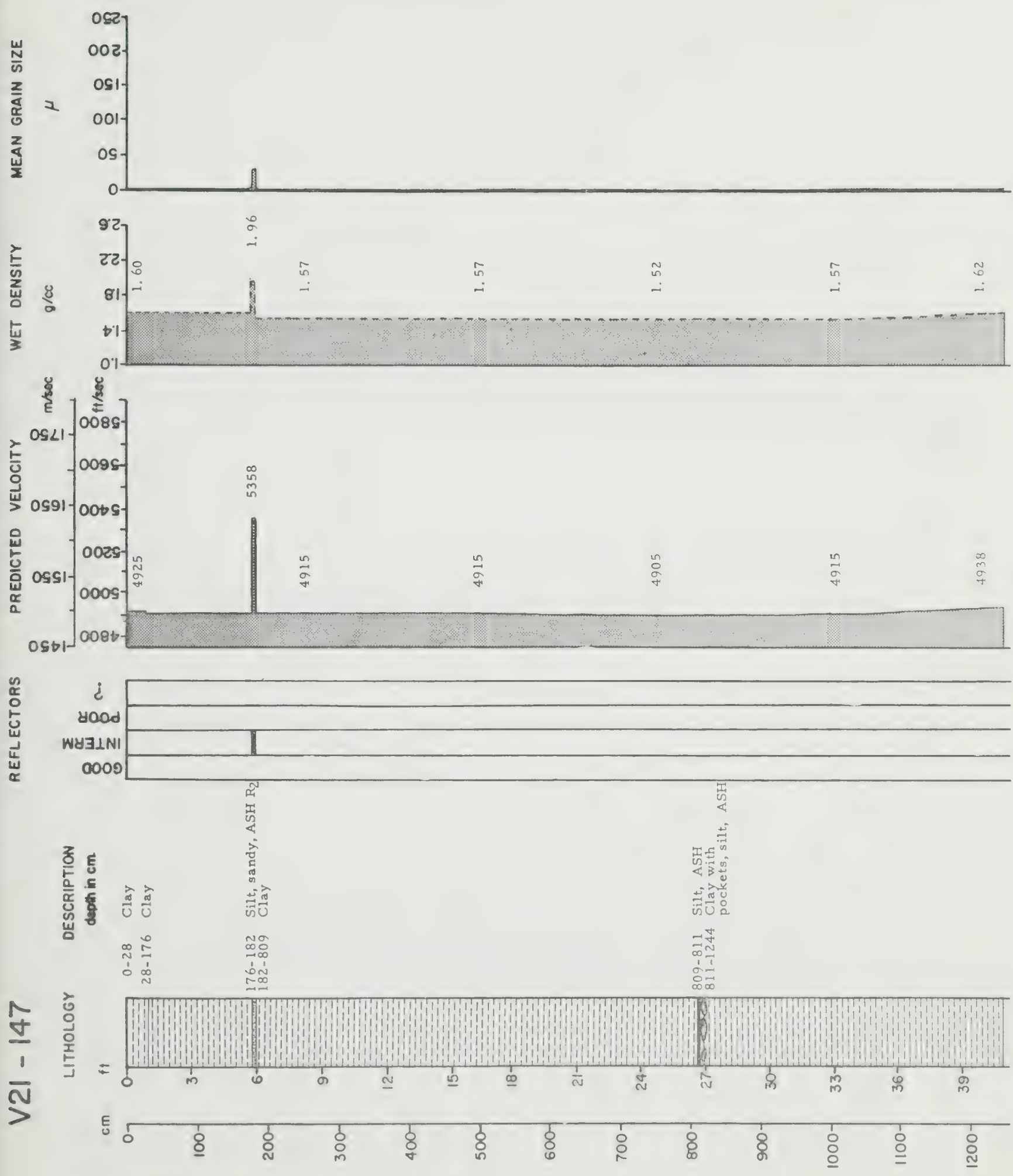
V21-145



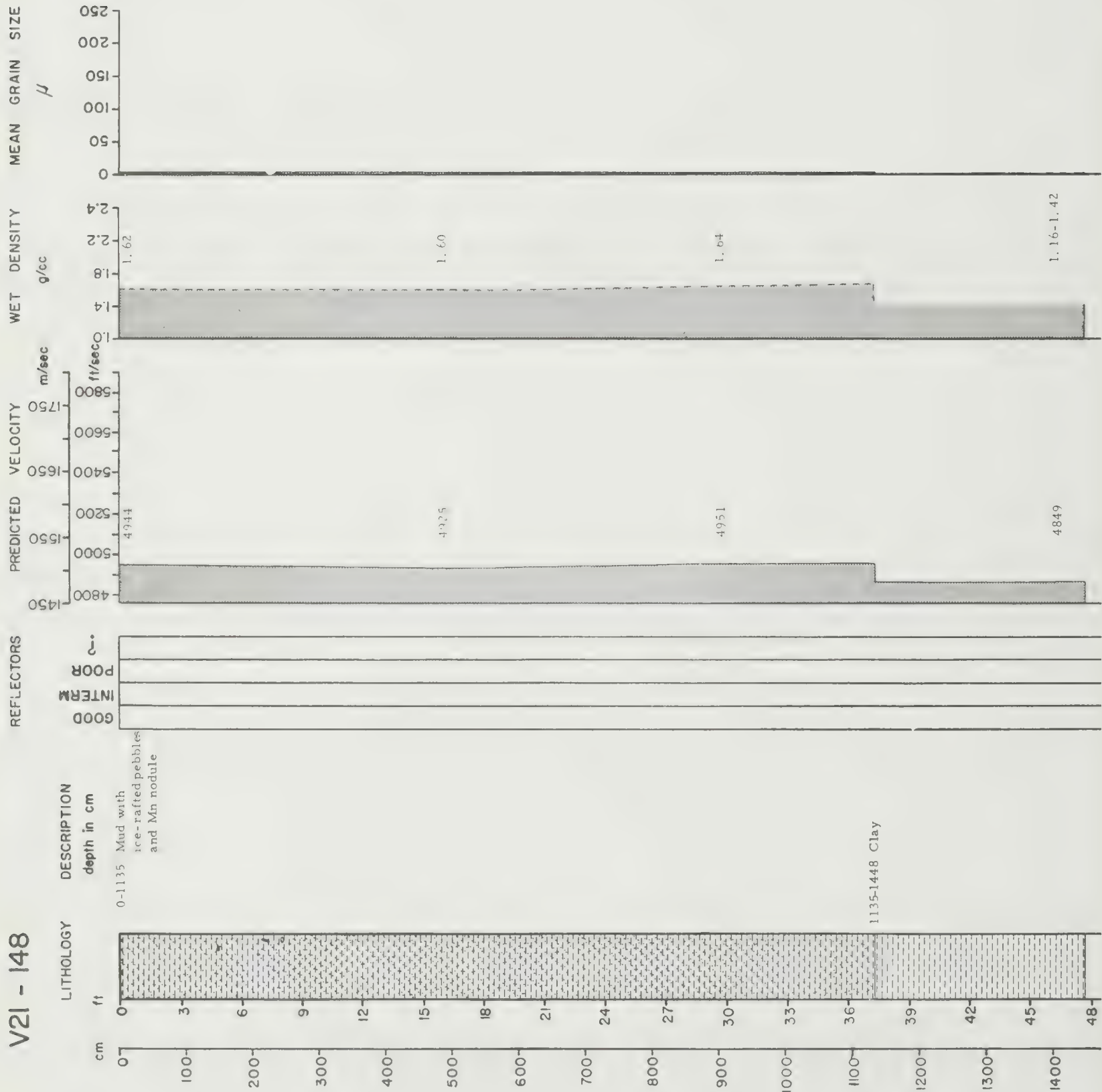
V21 - 146



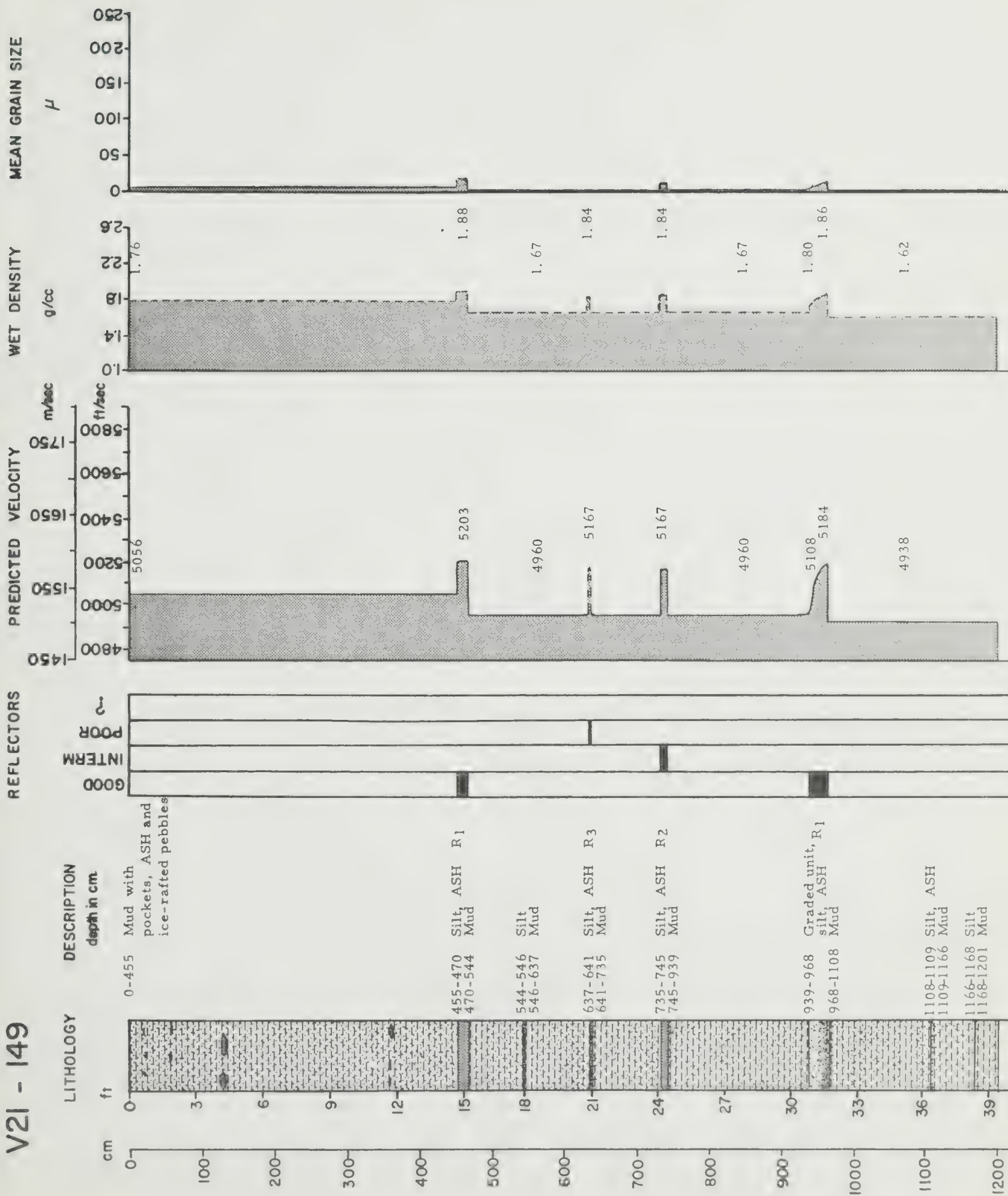
V21 - 147



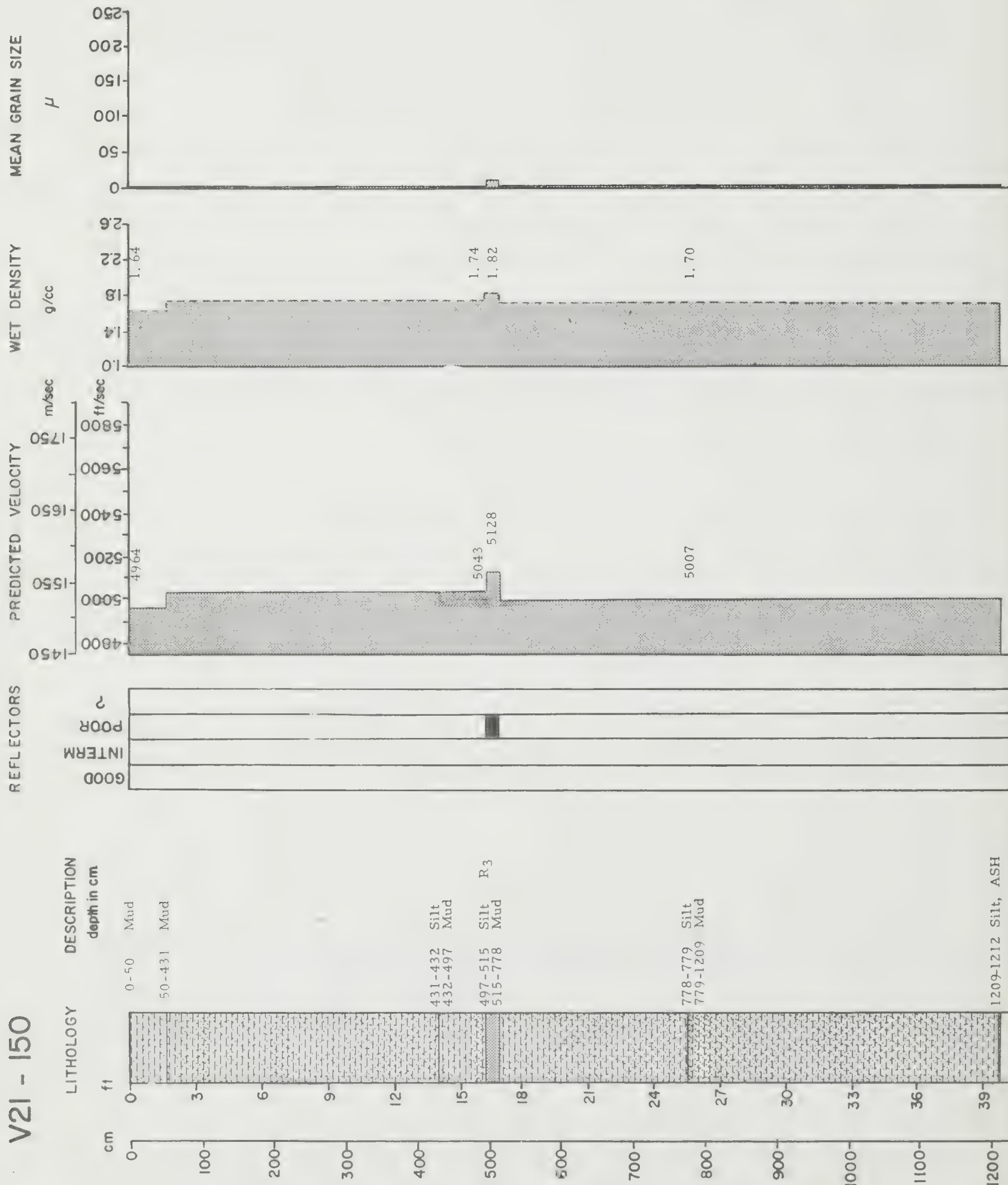
V21 - 148

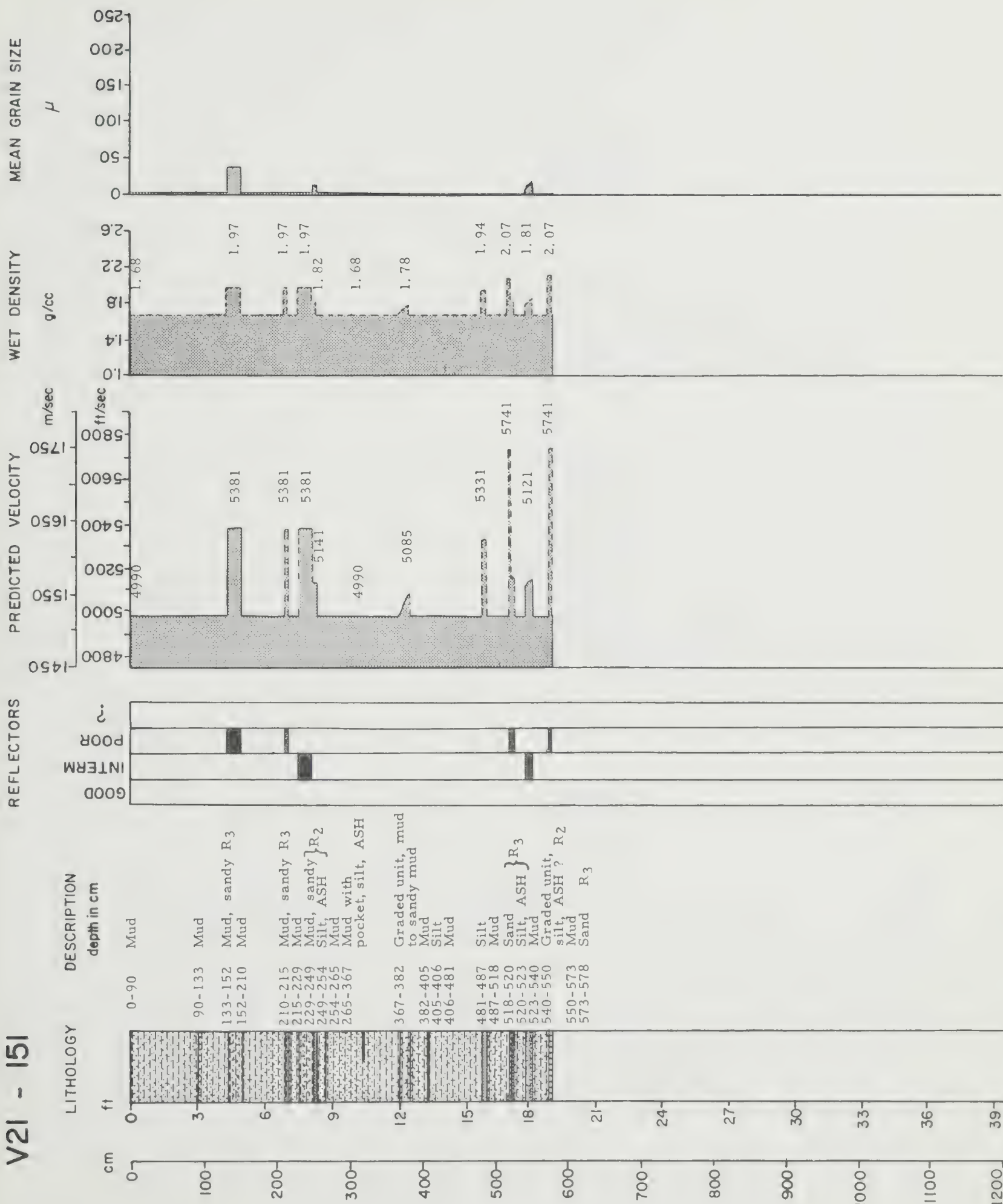






V21 - 150







V21 - 166

REFLECTORS

PREDICTED VELOCITY

WET DENSITY

MEAN GRAIN SIZE

LITHOLOGY

DESCRIPTION

depth in cm

cm

ft

$\mu$

g/cc

m/sec

ft/sec

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

ft

0-325 Mud with silt  
128-208 Clay  
208-225 Silt R2  
325-464 Sand, fine-grained R1  
464-475 Graded unit, mud to silt  
475-480 Graded unit, mud  
480-490 Mud  
490-510 Graded unit, mud to muddy sand  
503-510 Sand R3  
510-536 Mud with silt

GOOD  
INTERM  
POOR

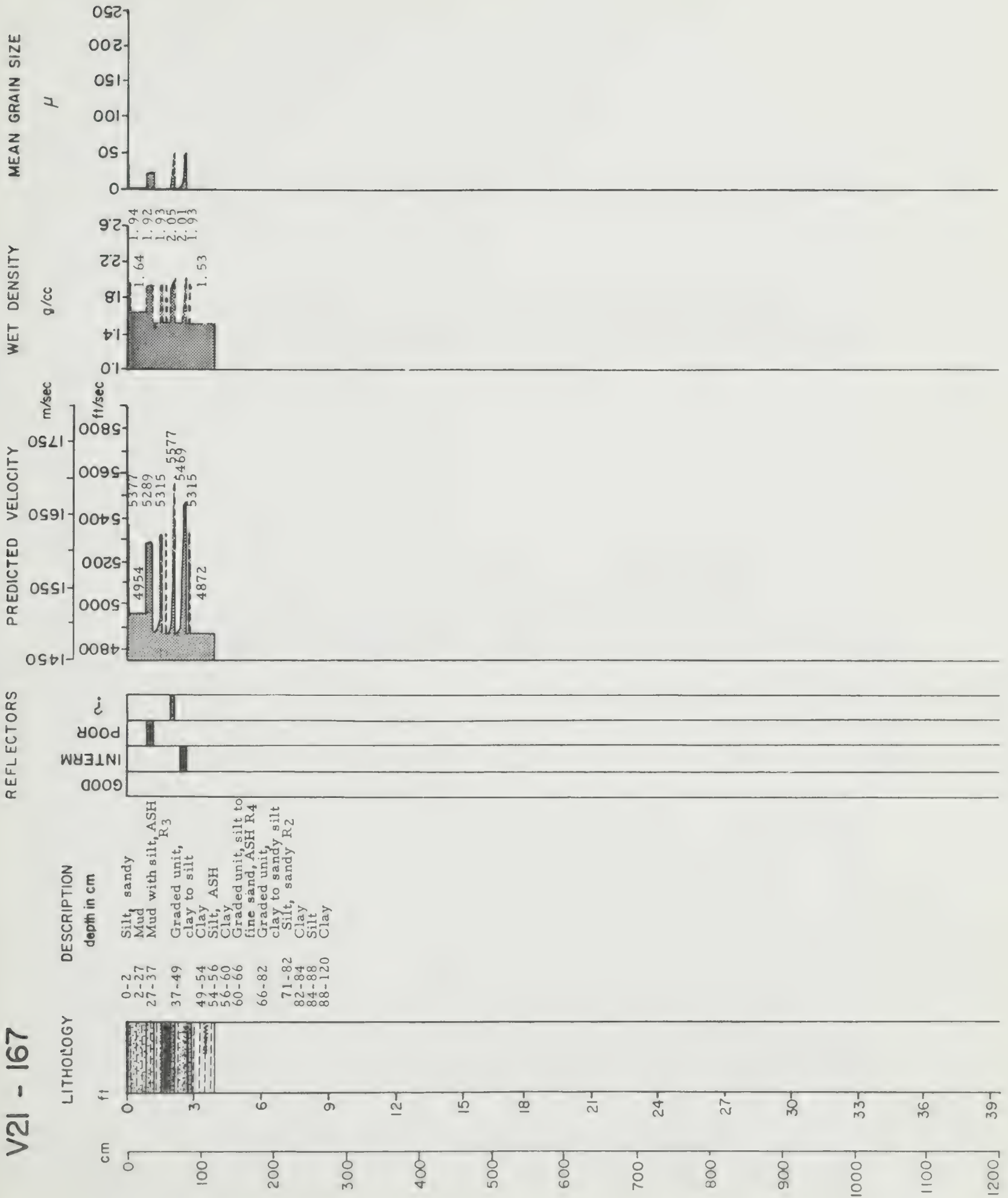
4800  
4900  
4941  
5000  
5150  
5200  
5200  
5154  
5154  
5315  
5804  
5755

1.61  
1.57  
1.83  
1.61  
2.11  
2.13  
1.83  
1.93  
1.61

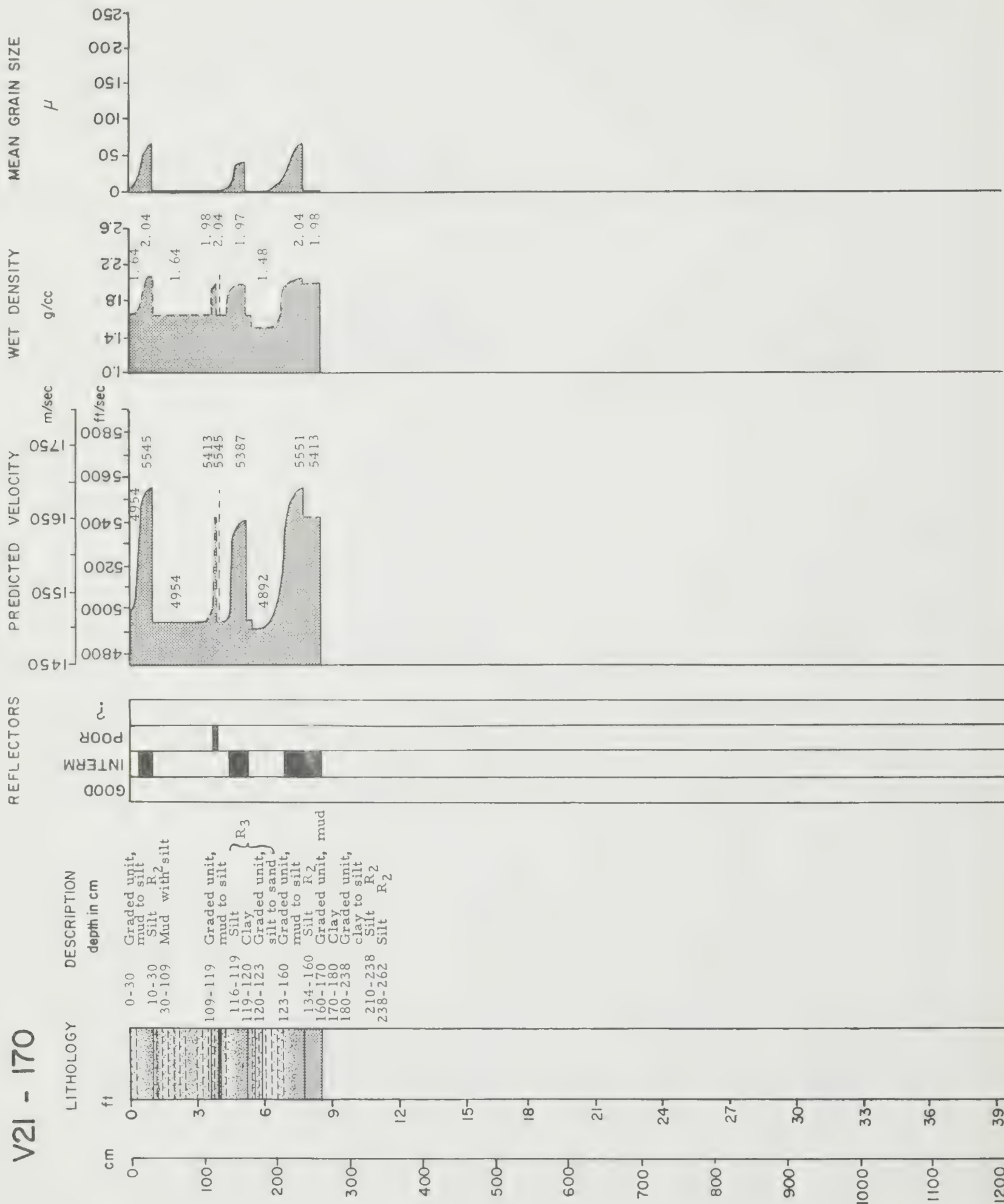
0  
50  
100  
150  
200  
250



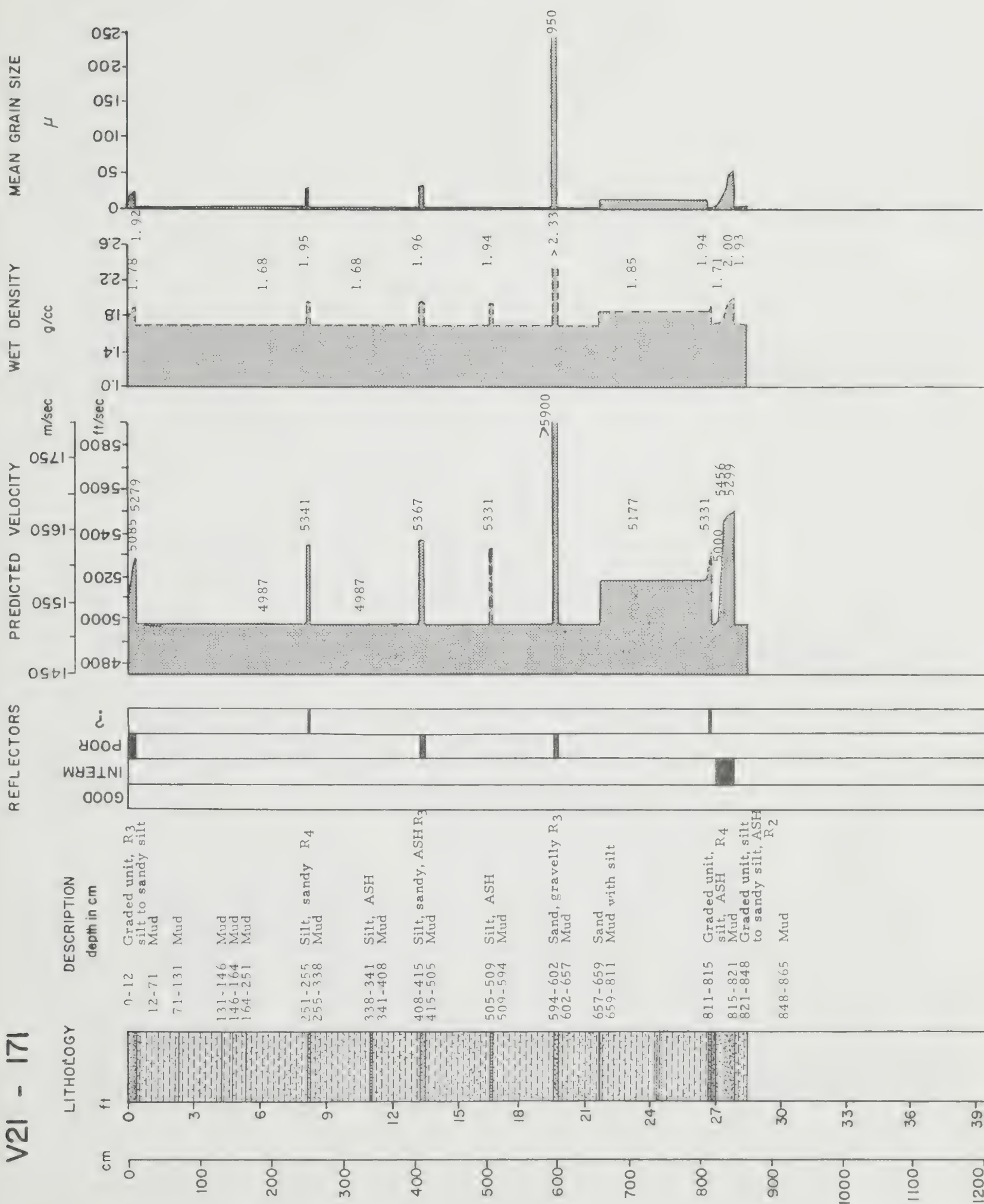
V2I - 167



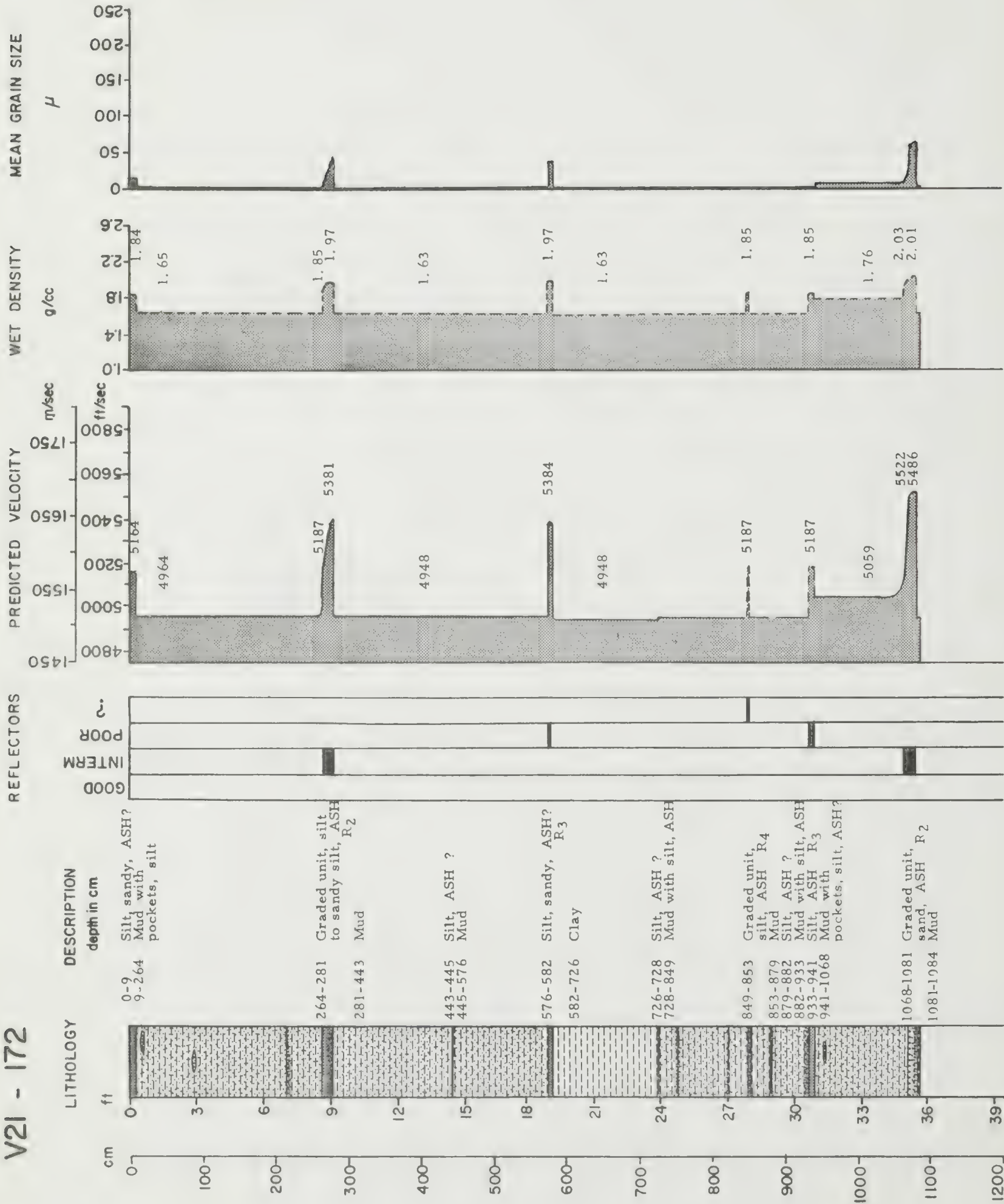
# V2I - 170



V2I - 171

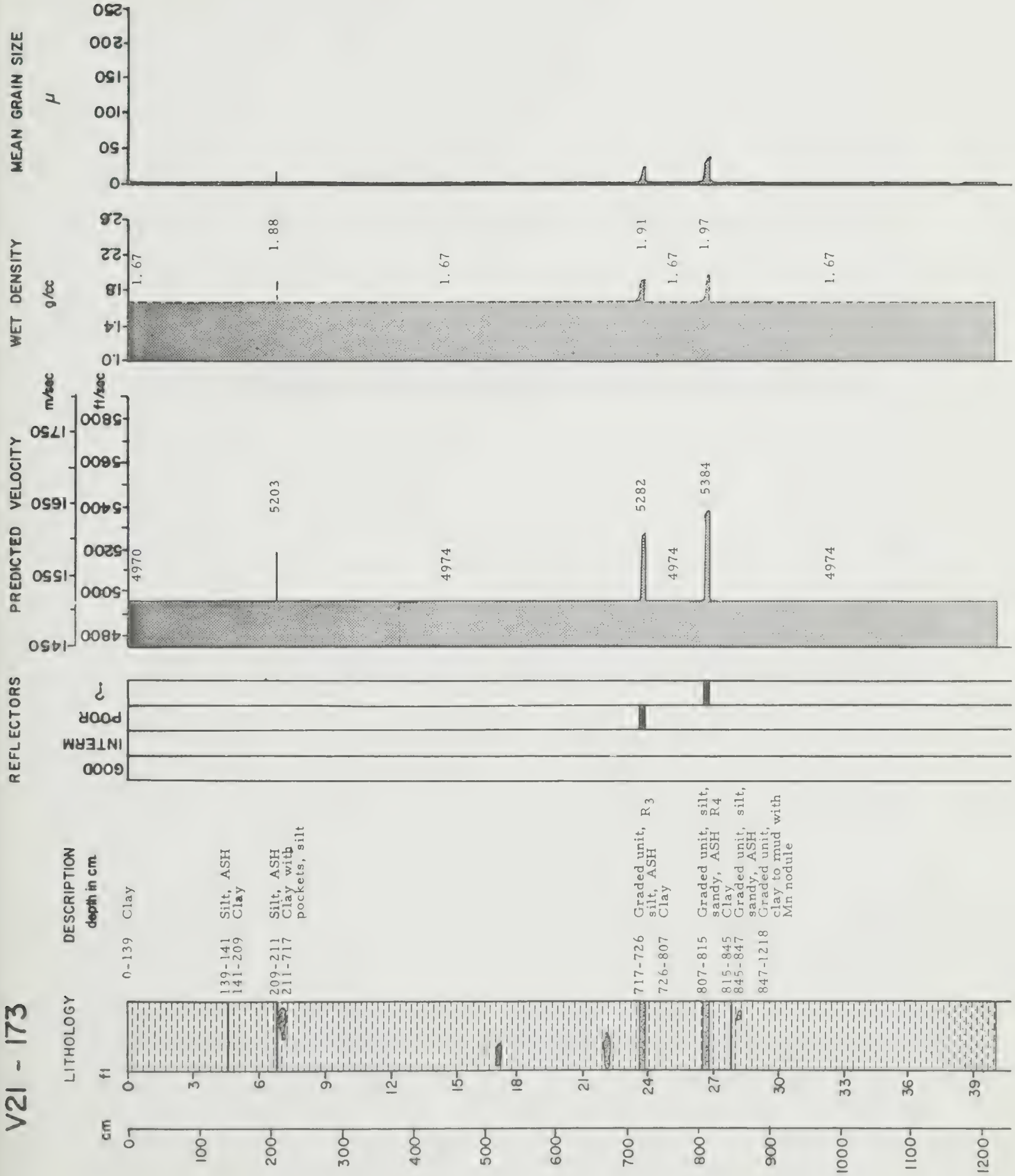


V21 - 172

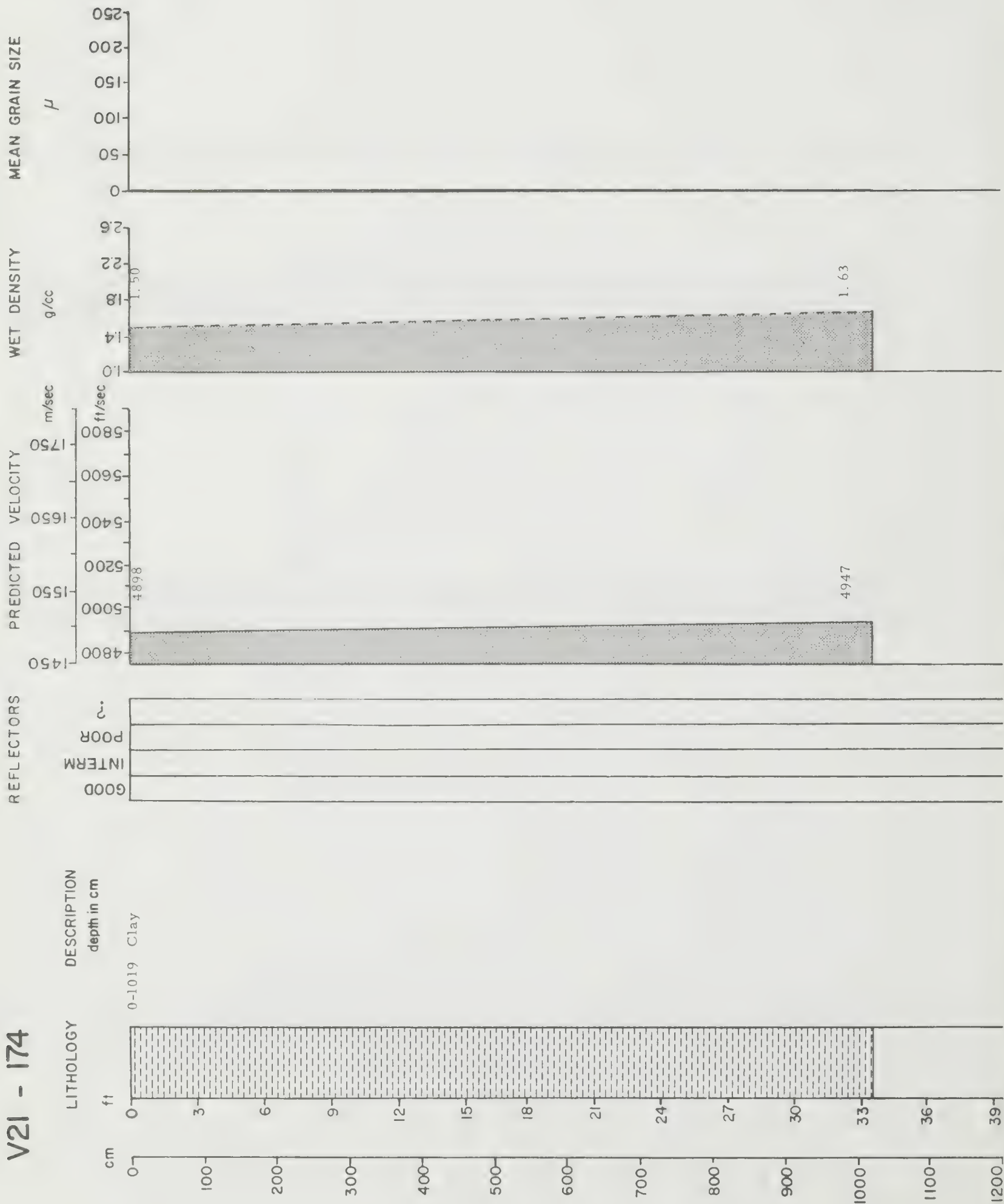




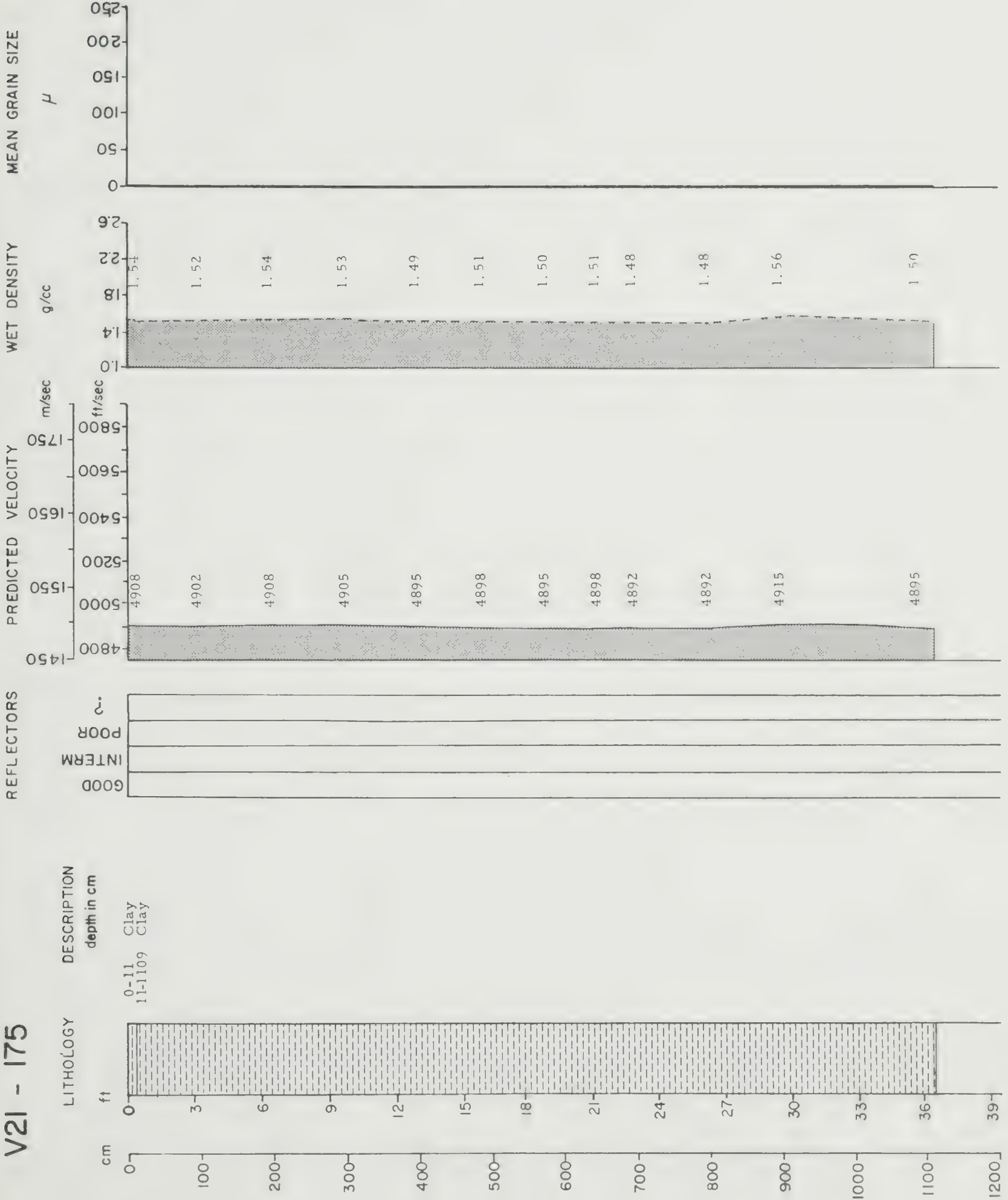
V21 - 173



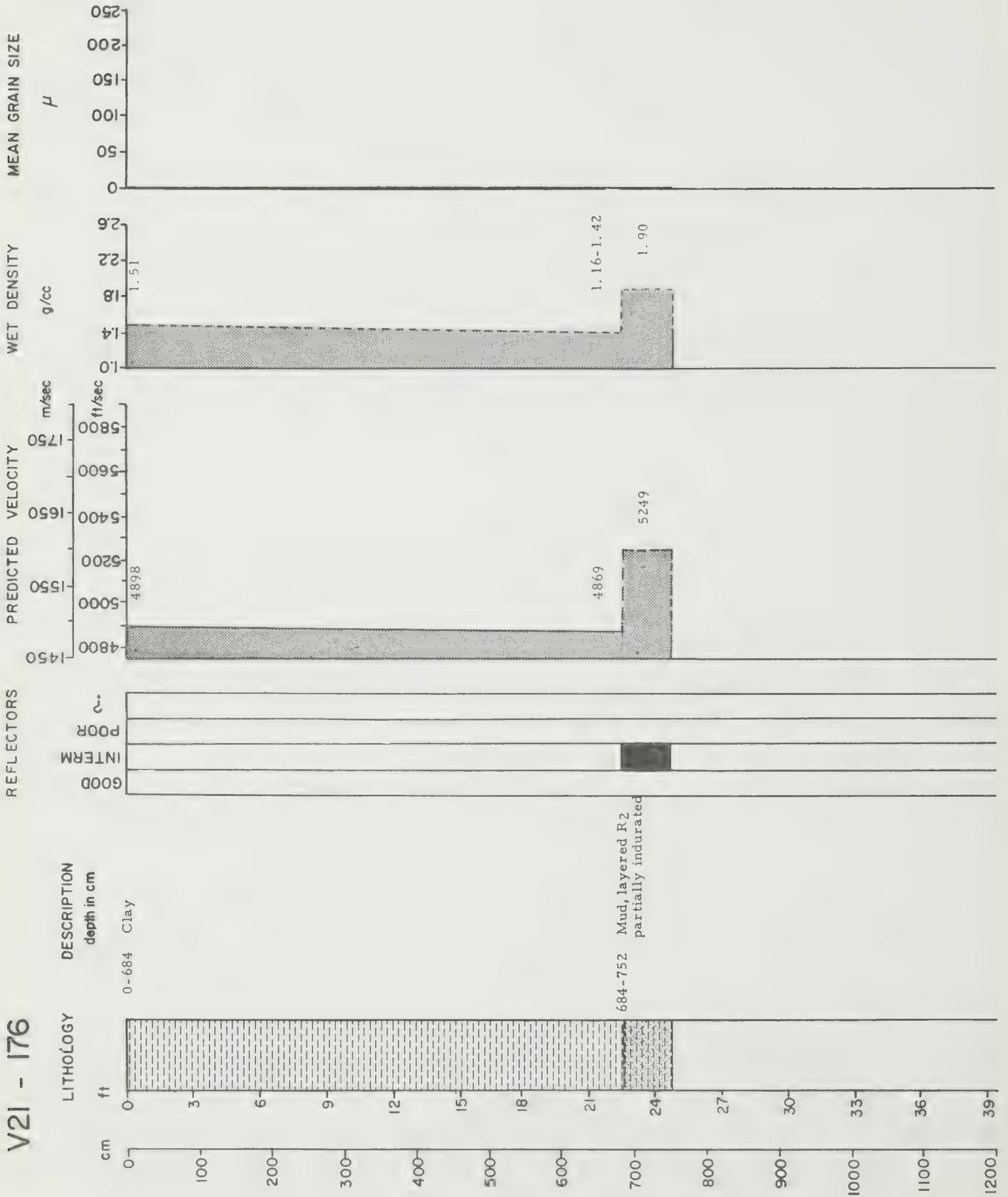
V21 - 174



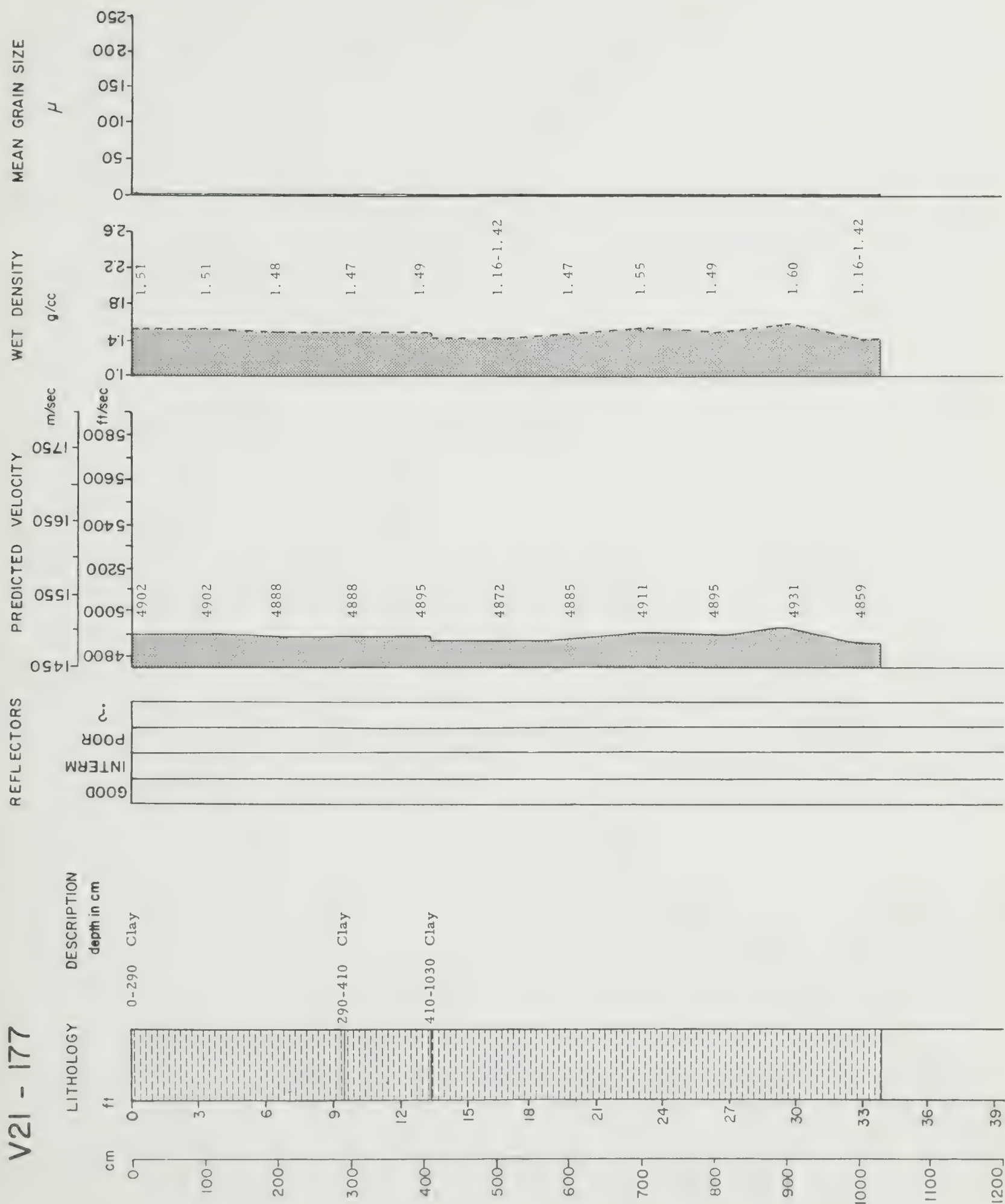
V21 - 175

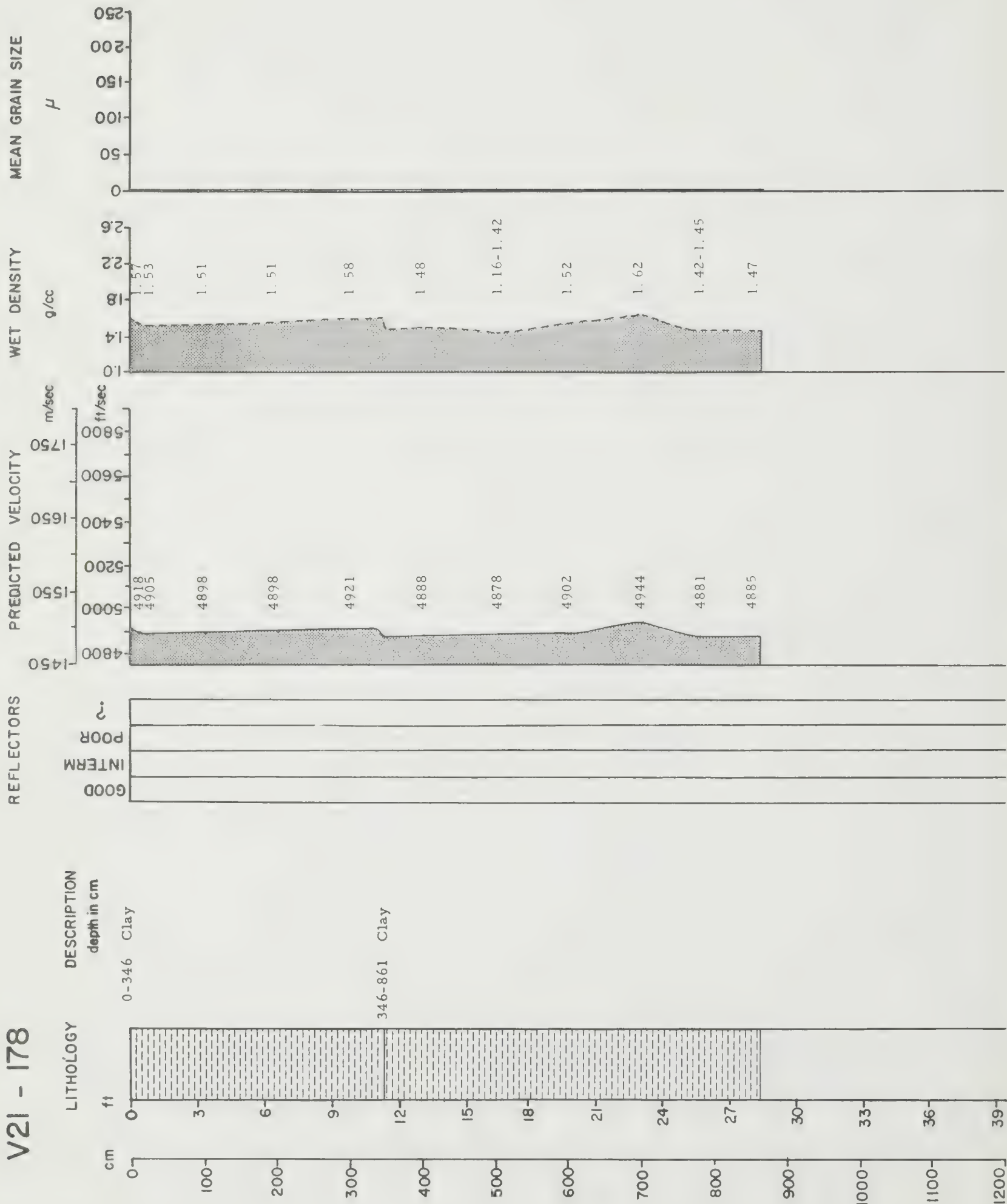


V21 - 176

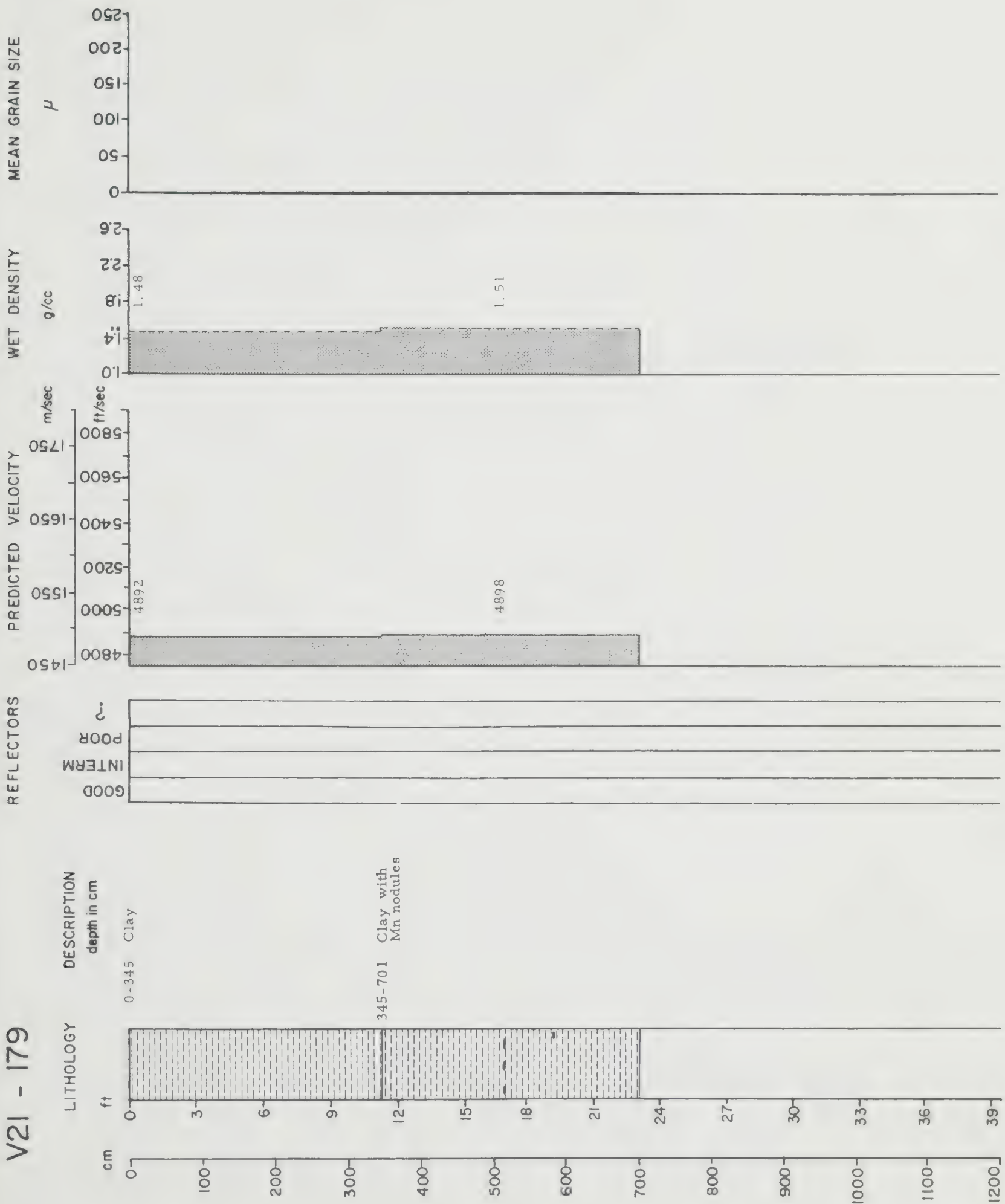




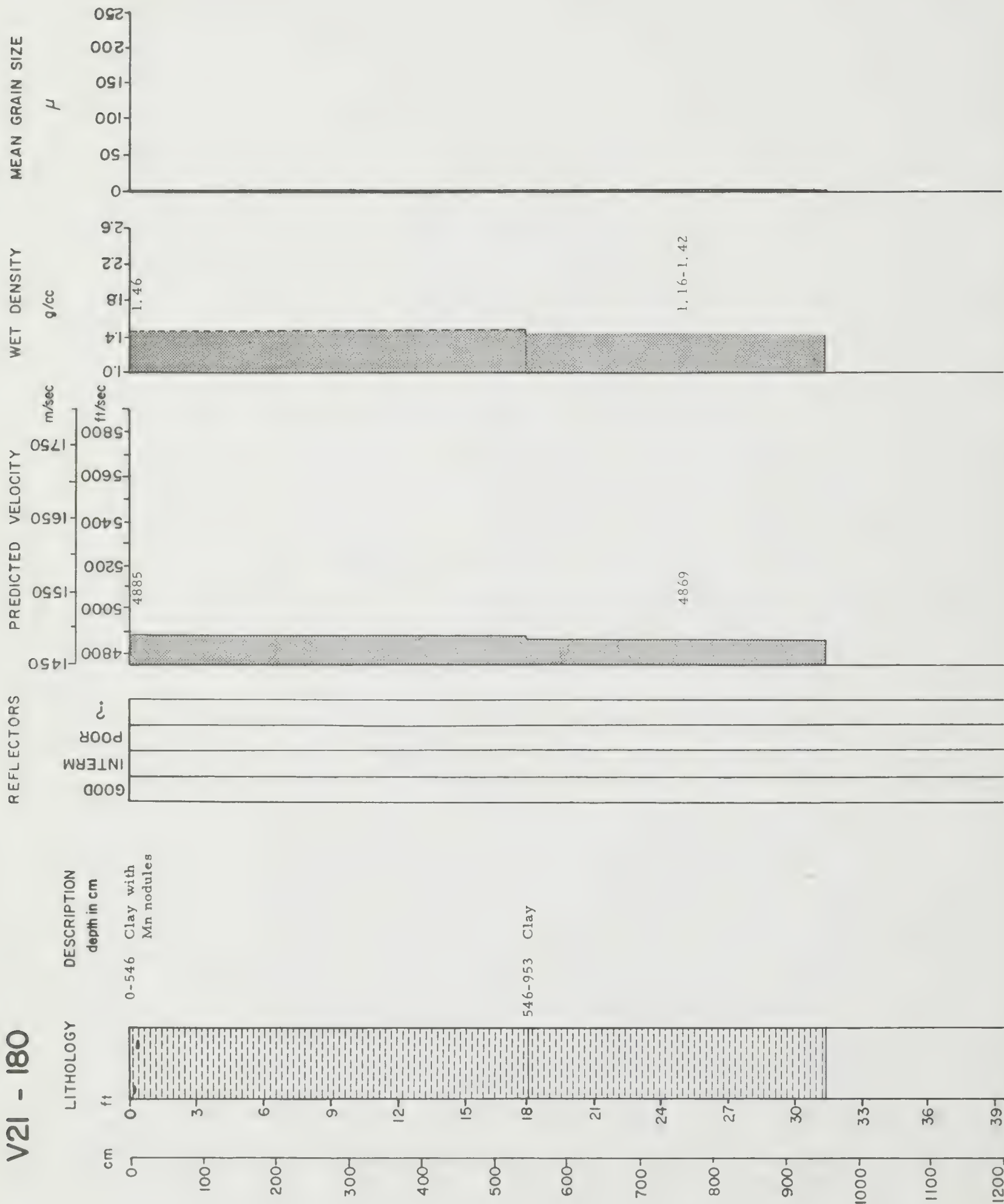




V21 - 179

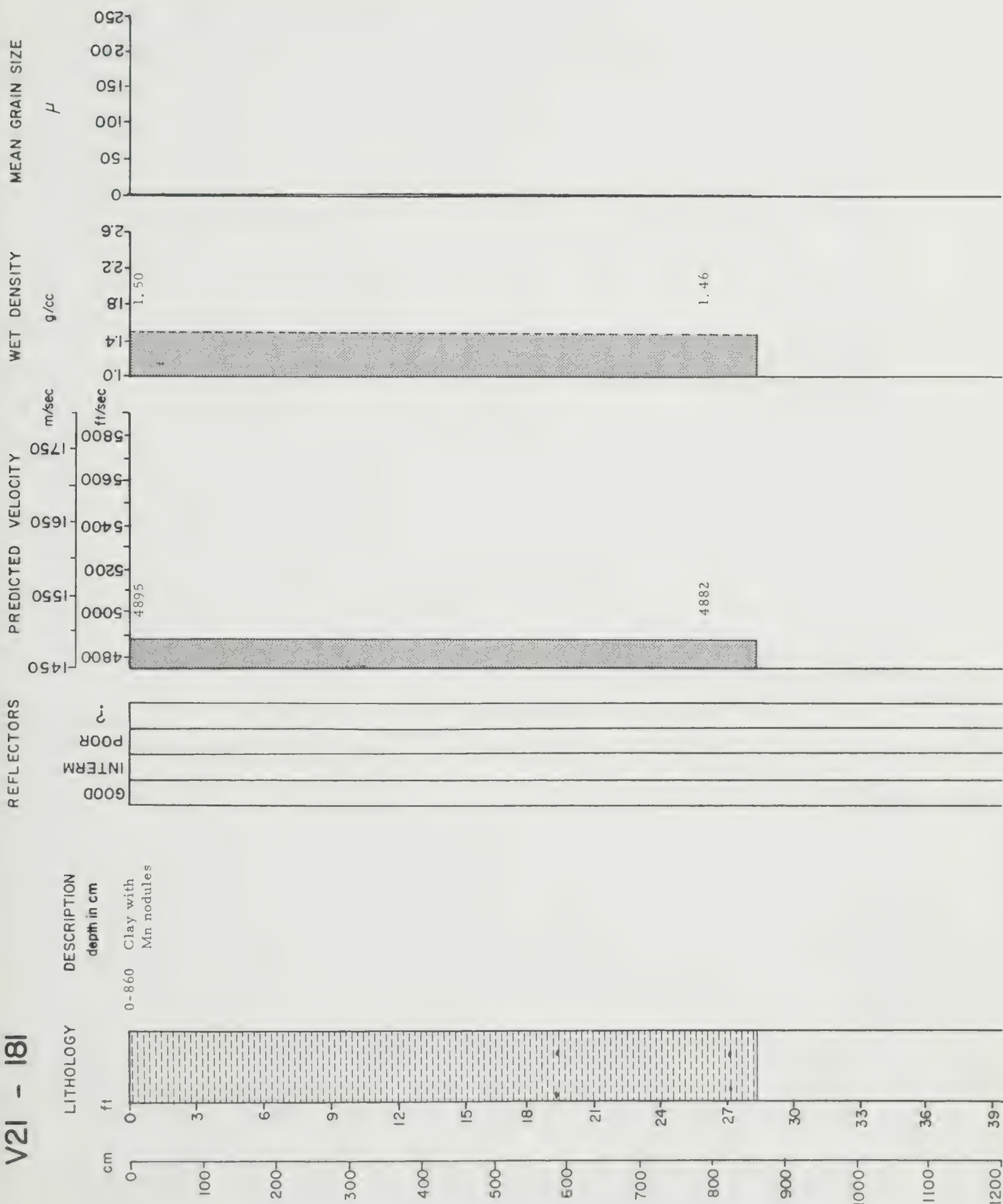


V21 - 180

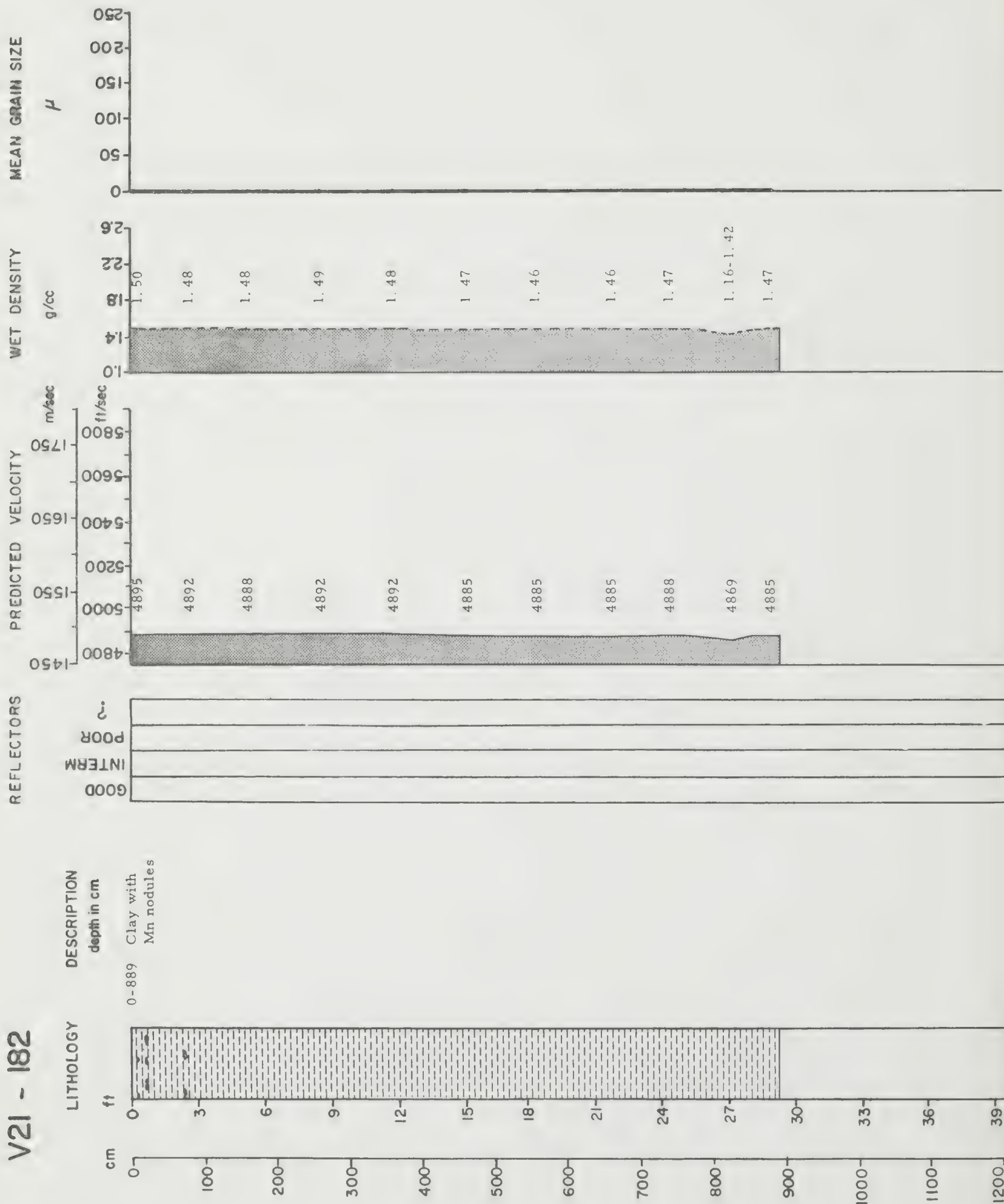


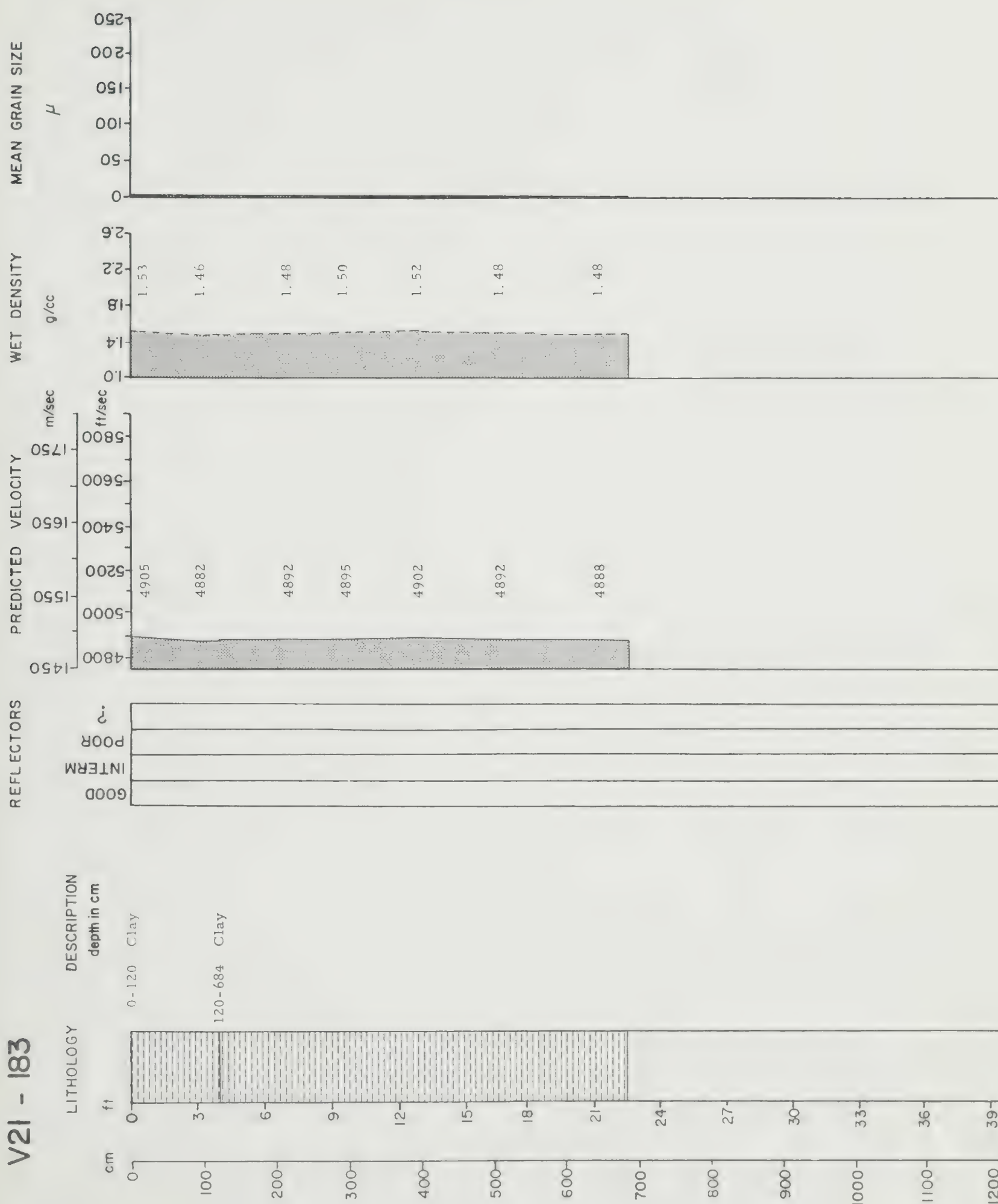


V21 - 181

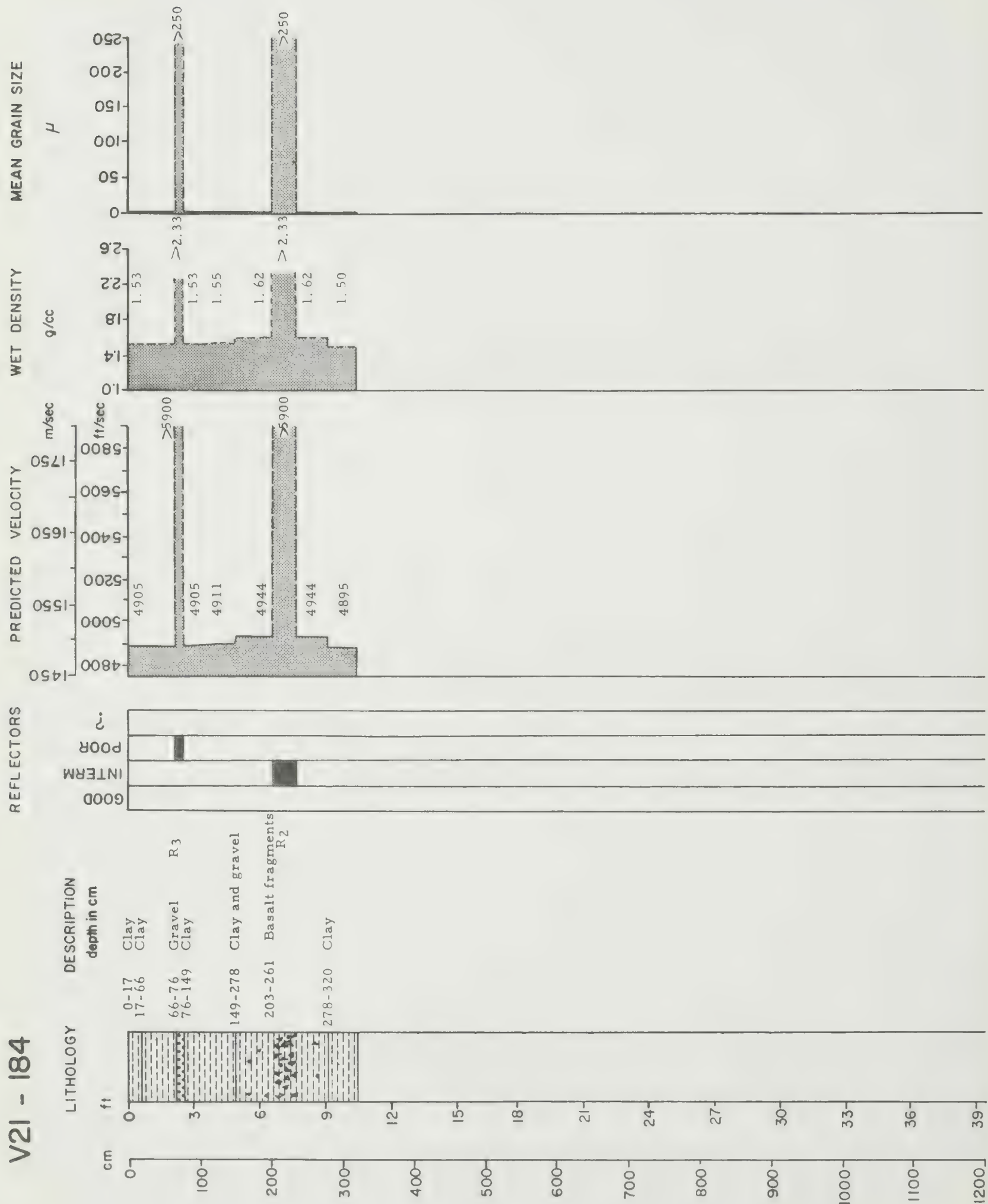


# V21 - 182



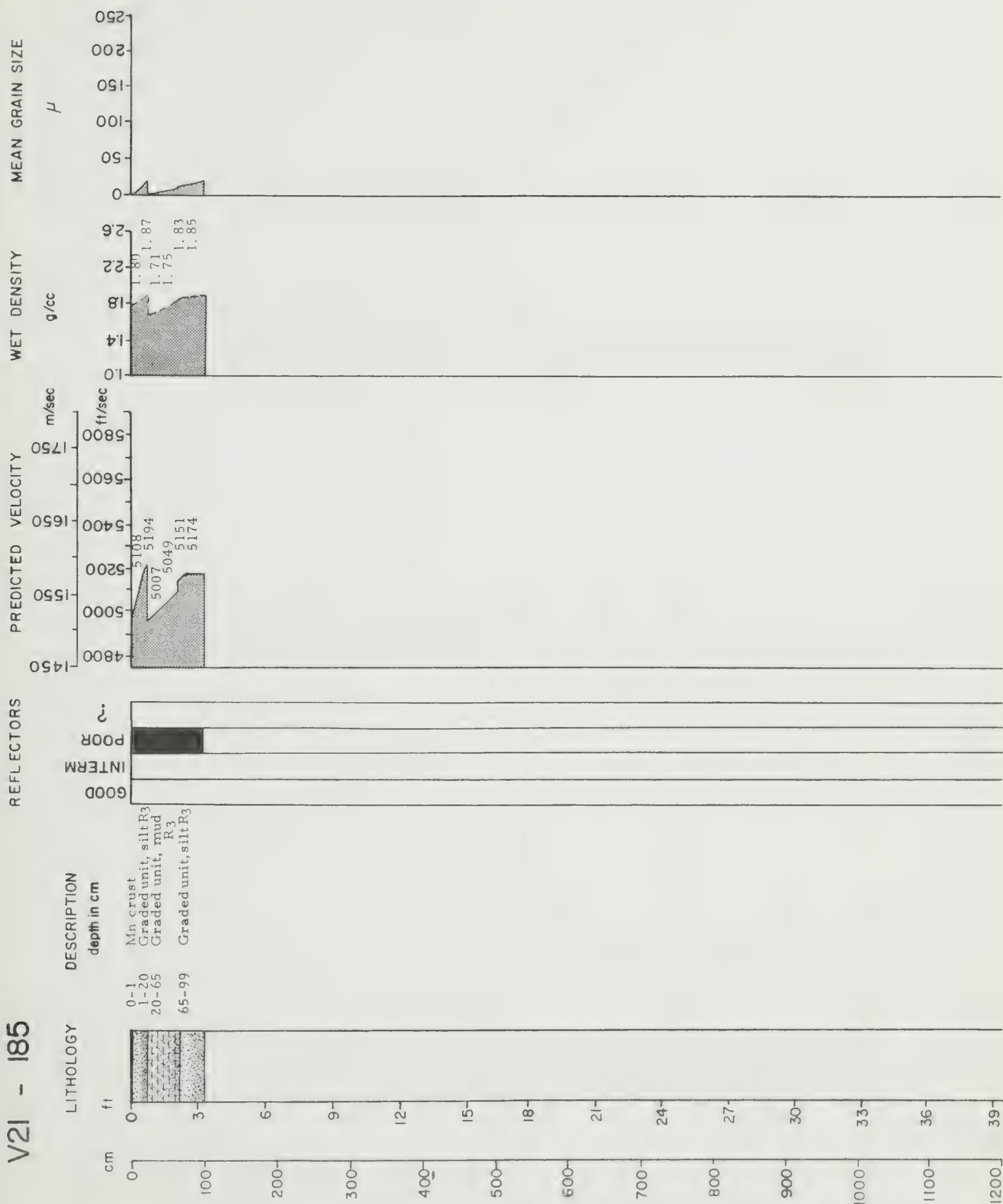


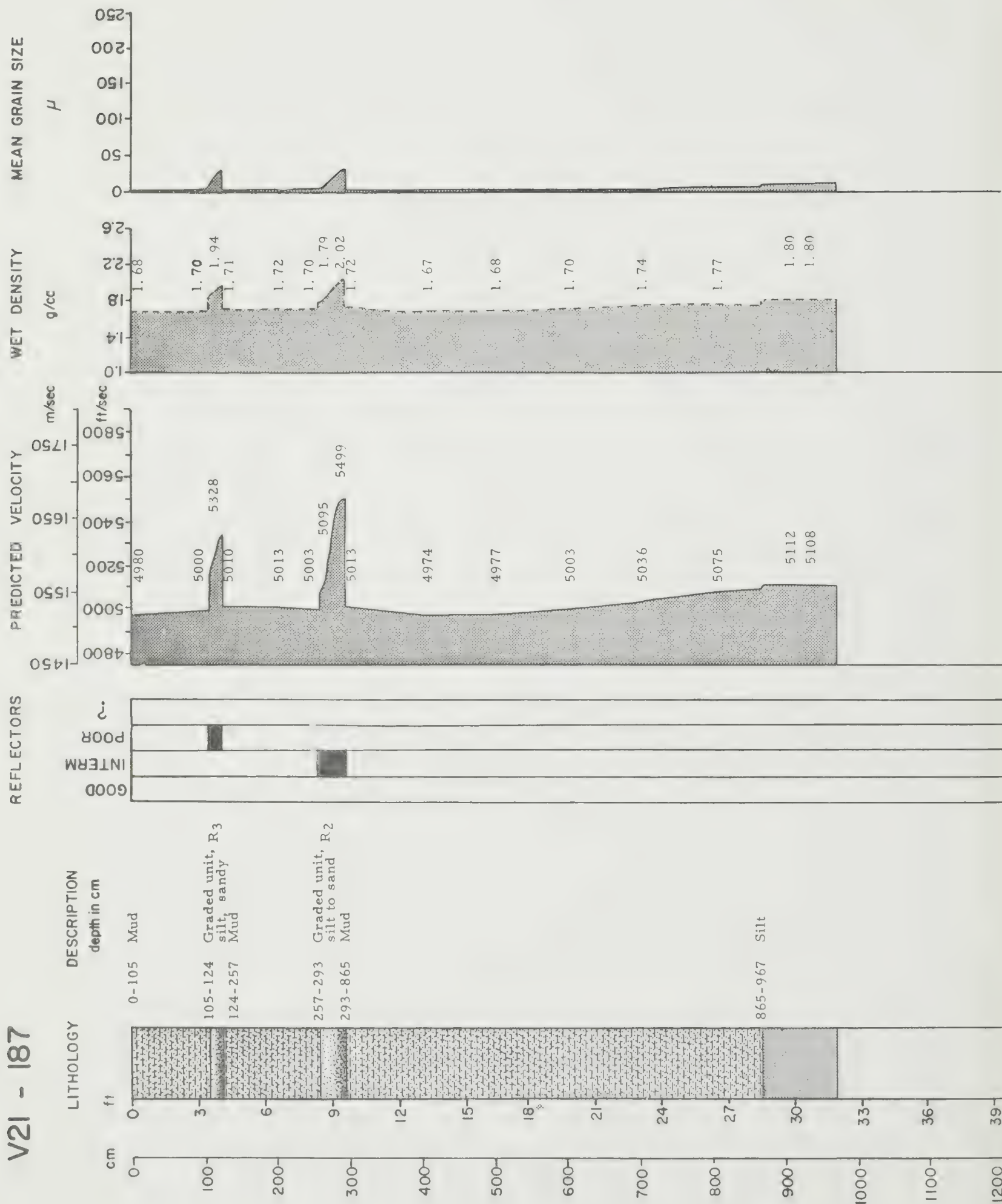
V21 - 184

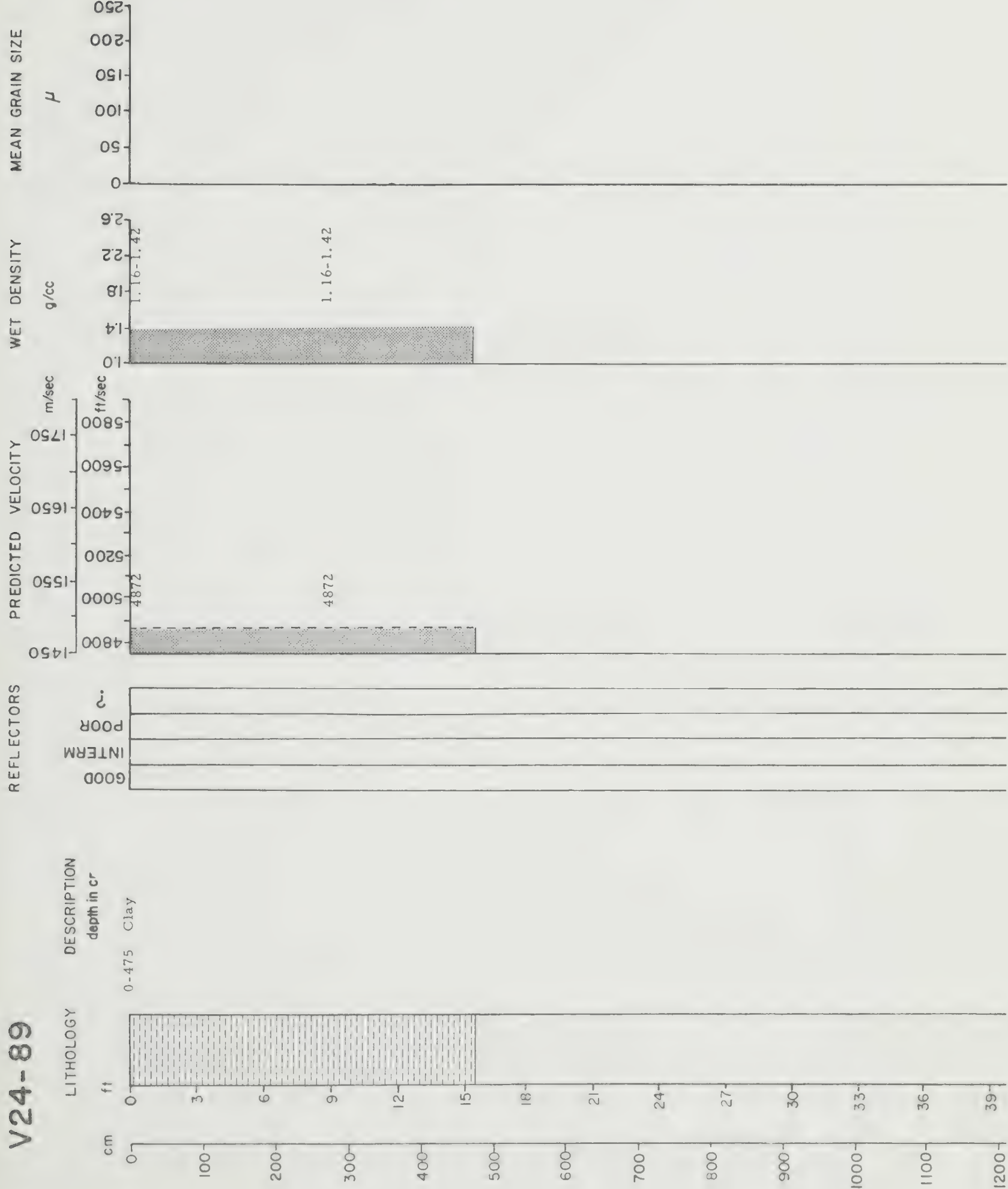




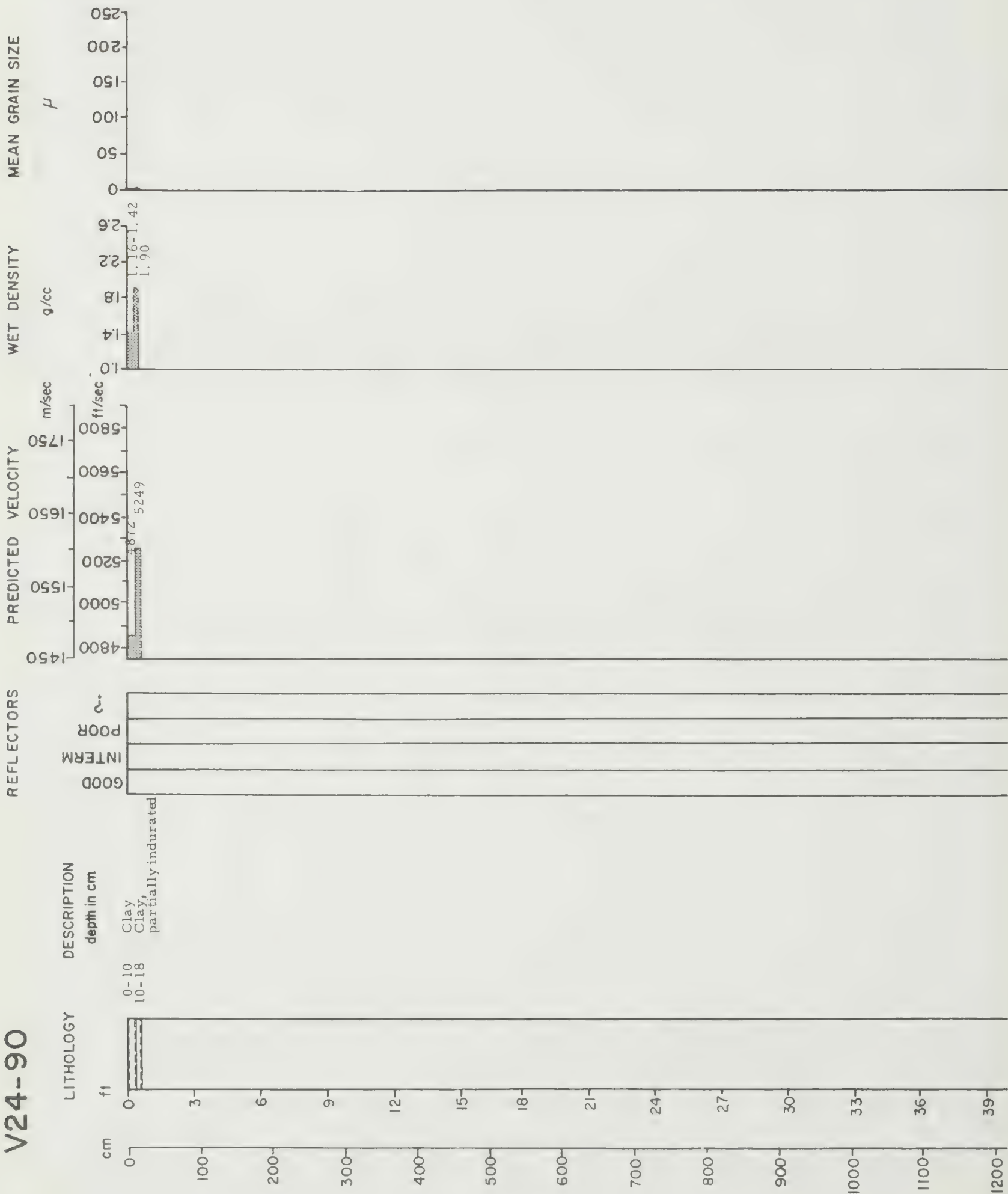
V21 - 185





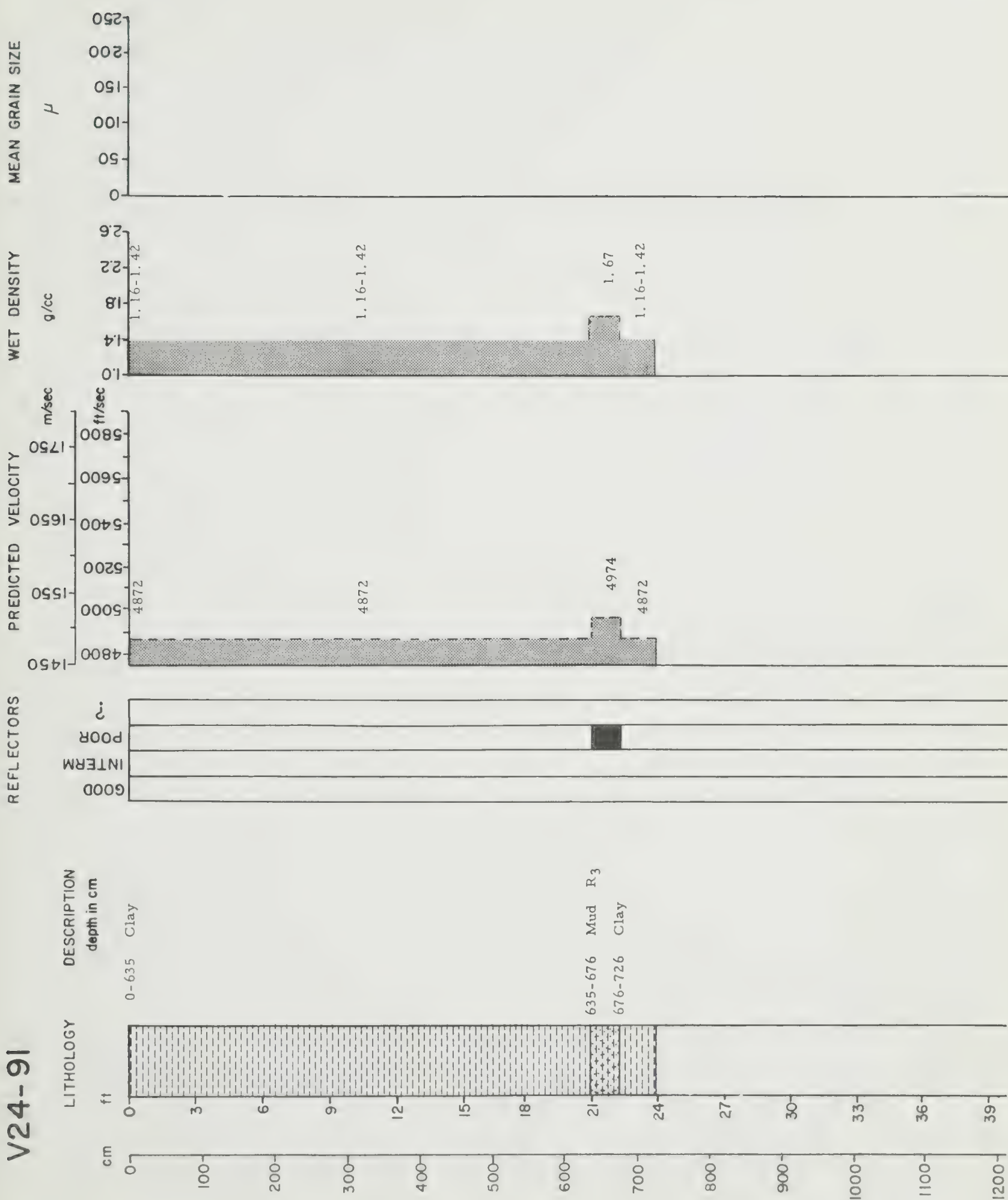


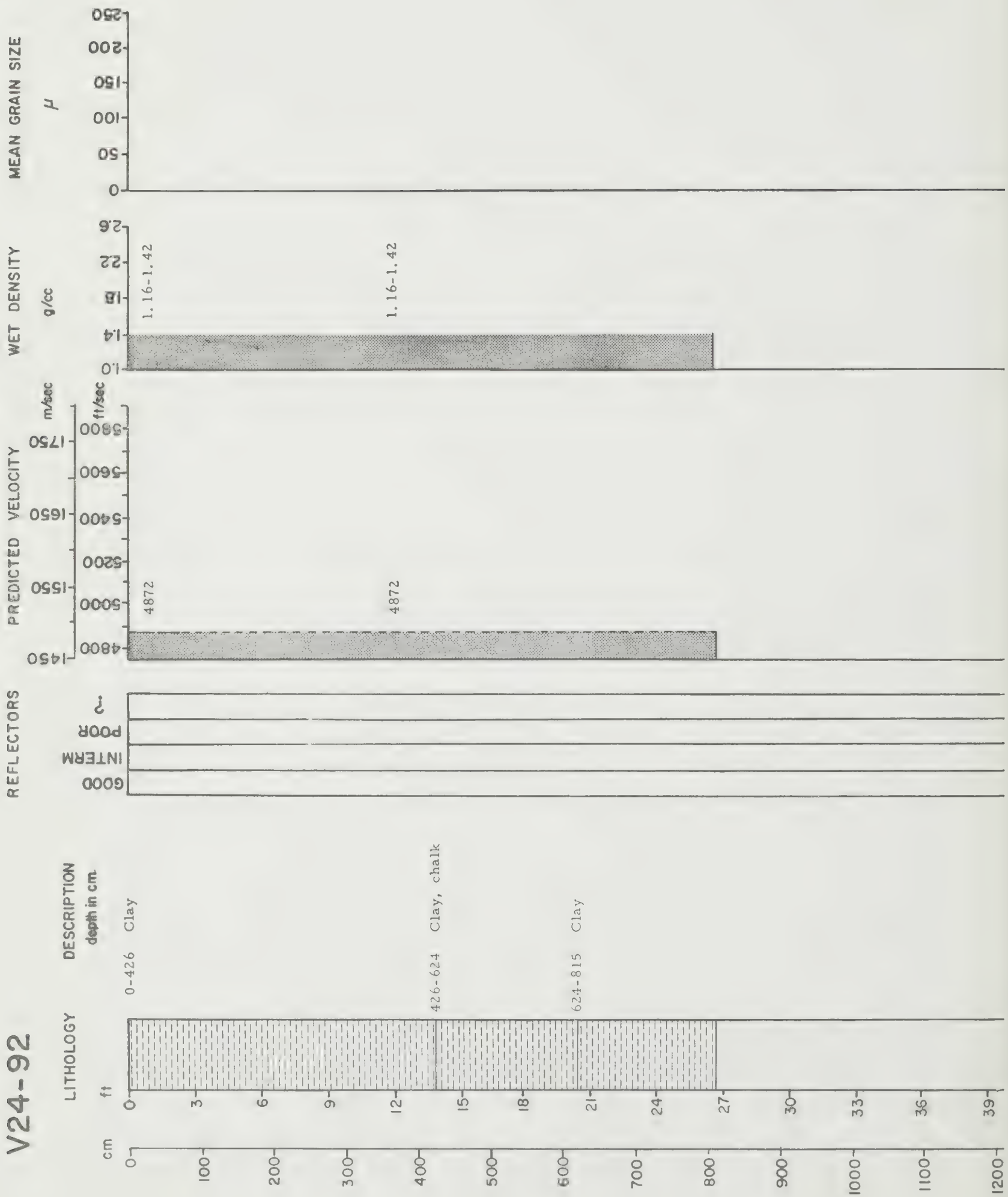
V24-90



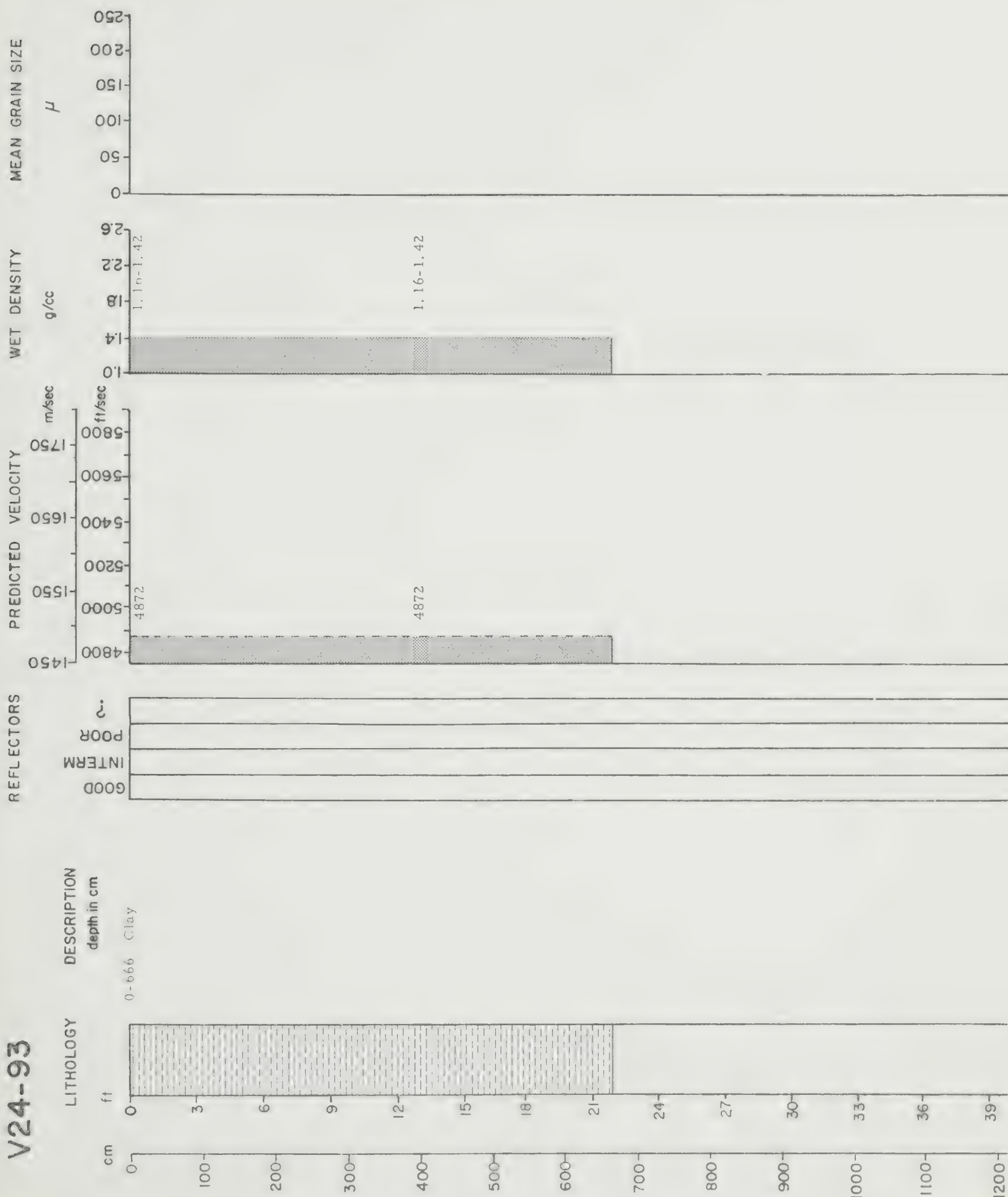


V24-91

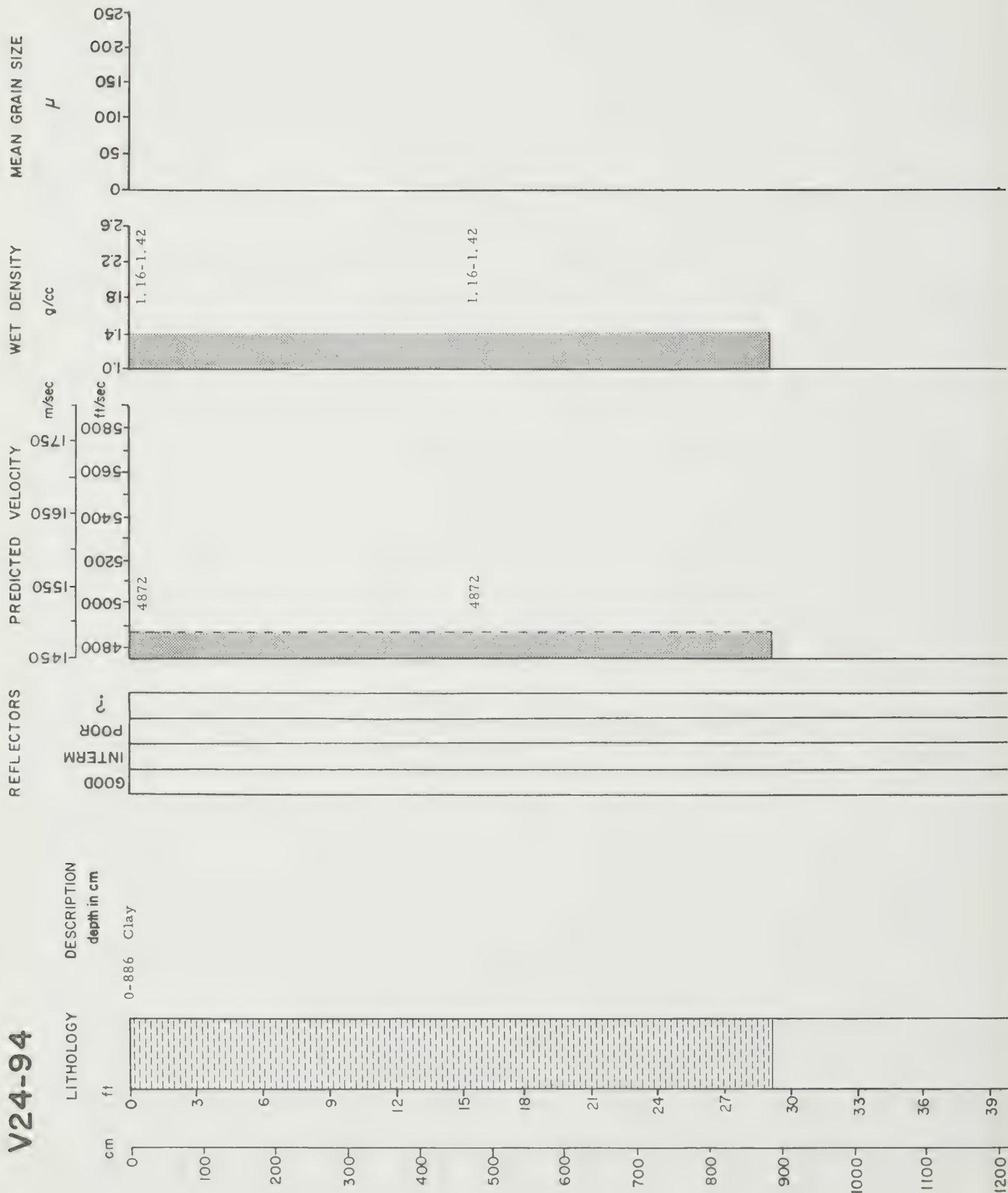




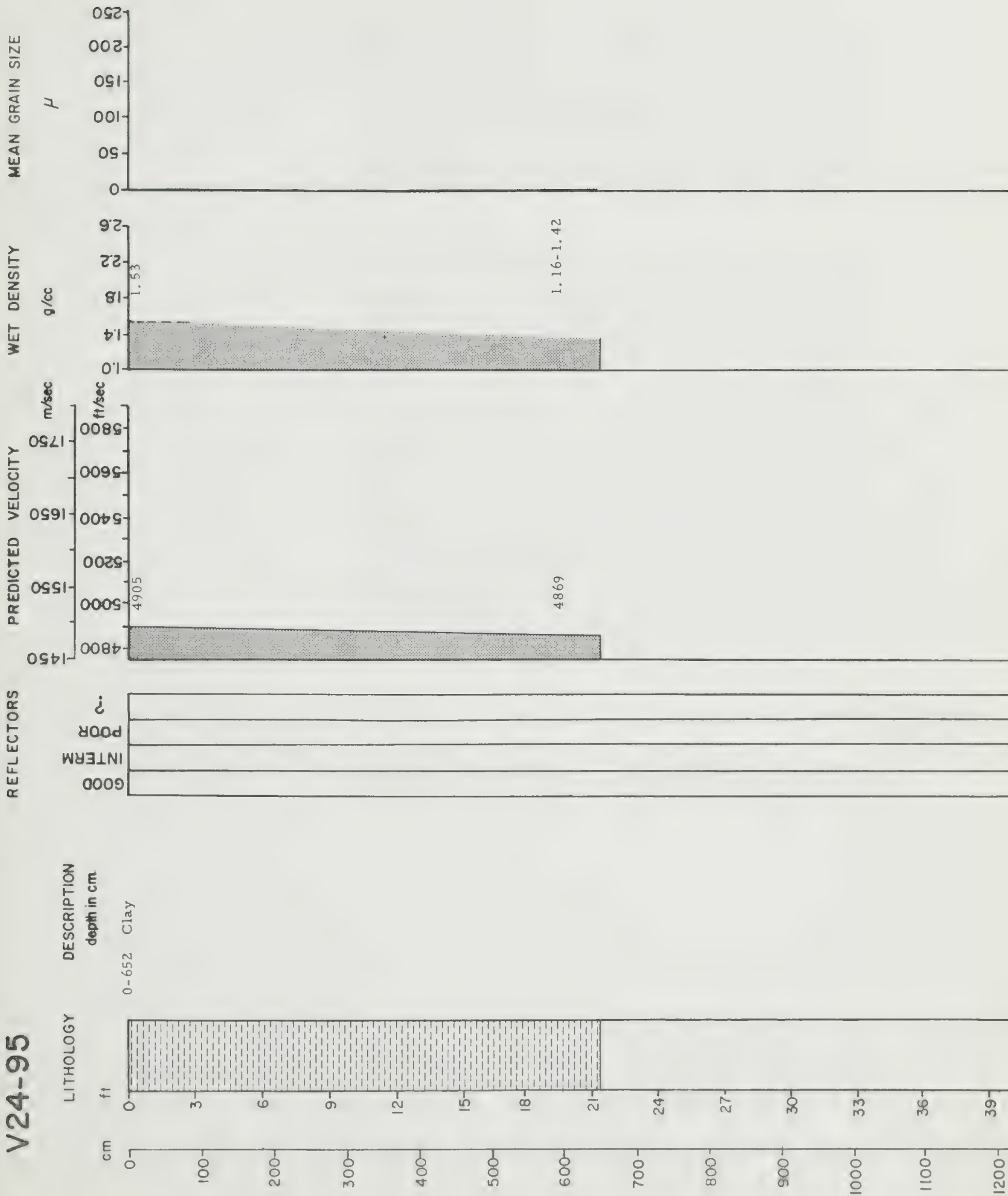
V24-93



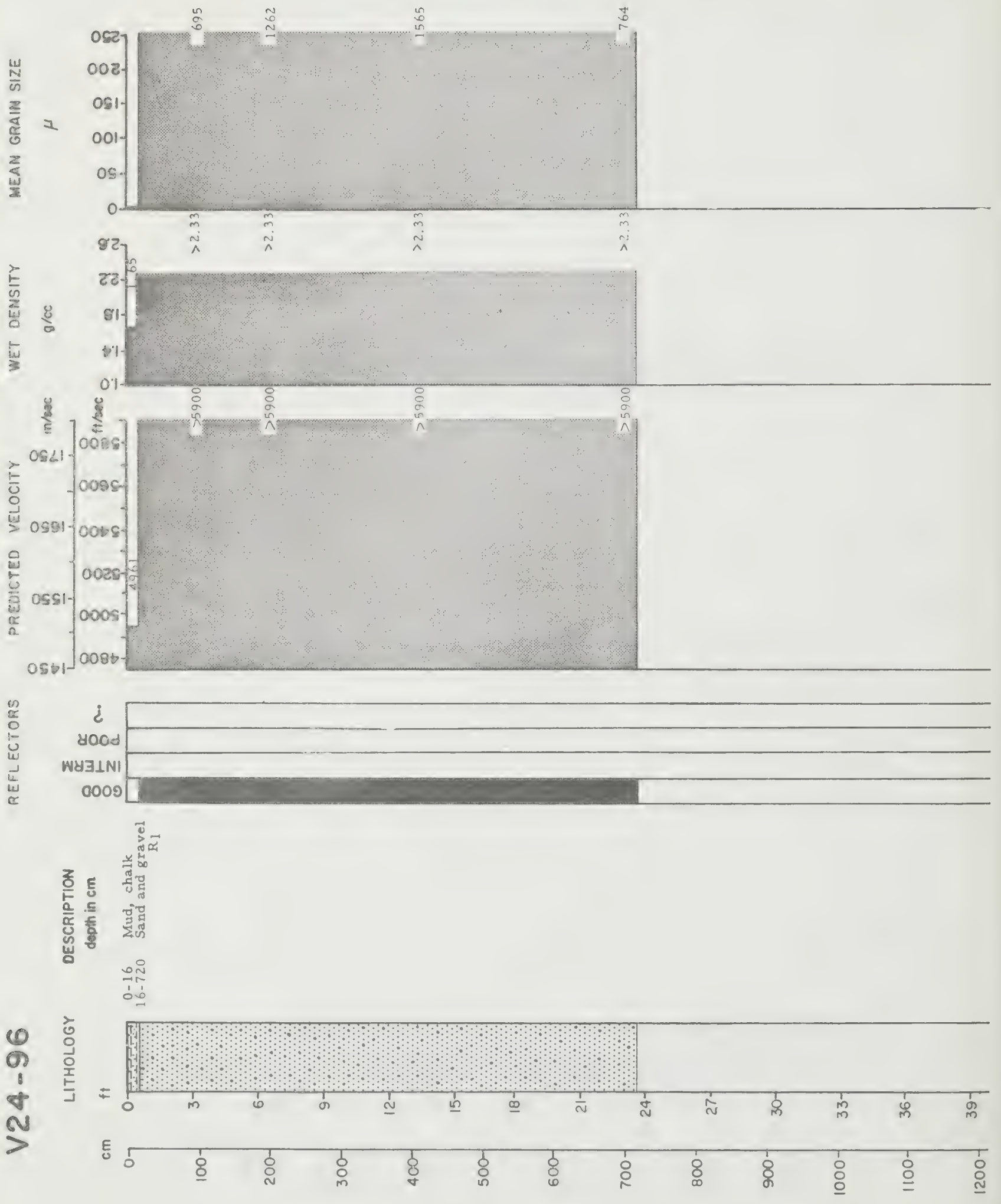
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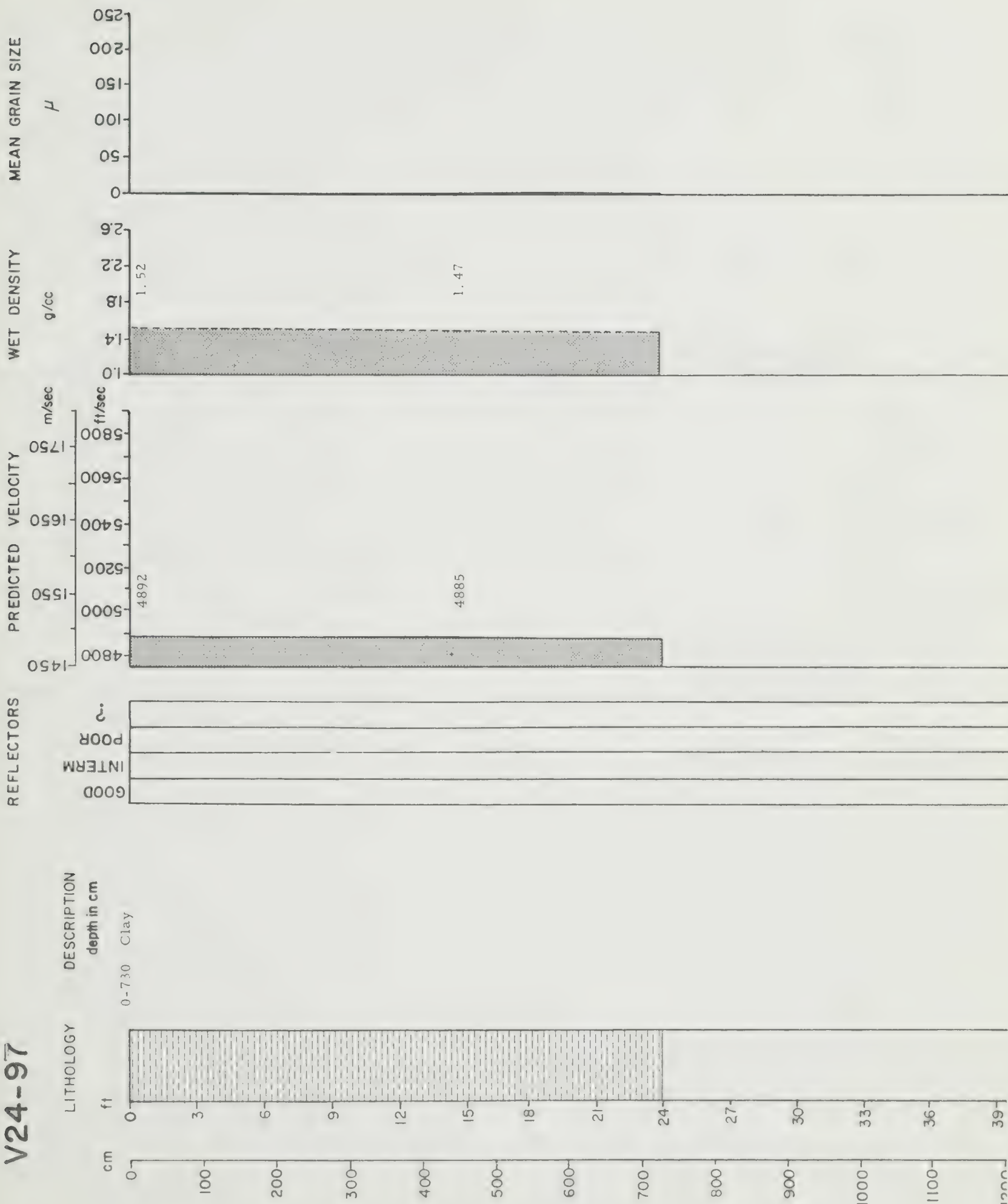




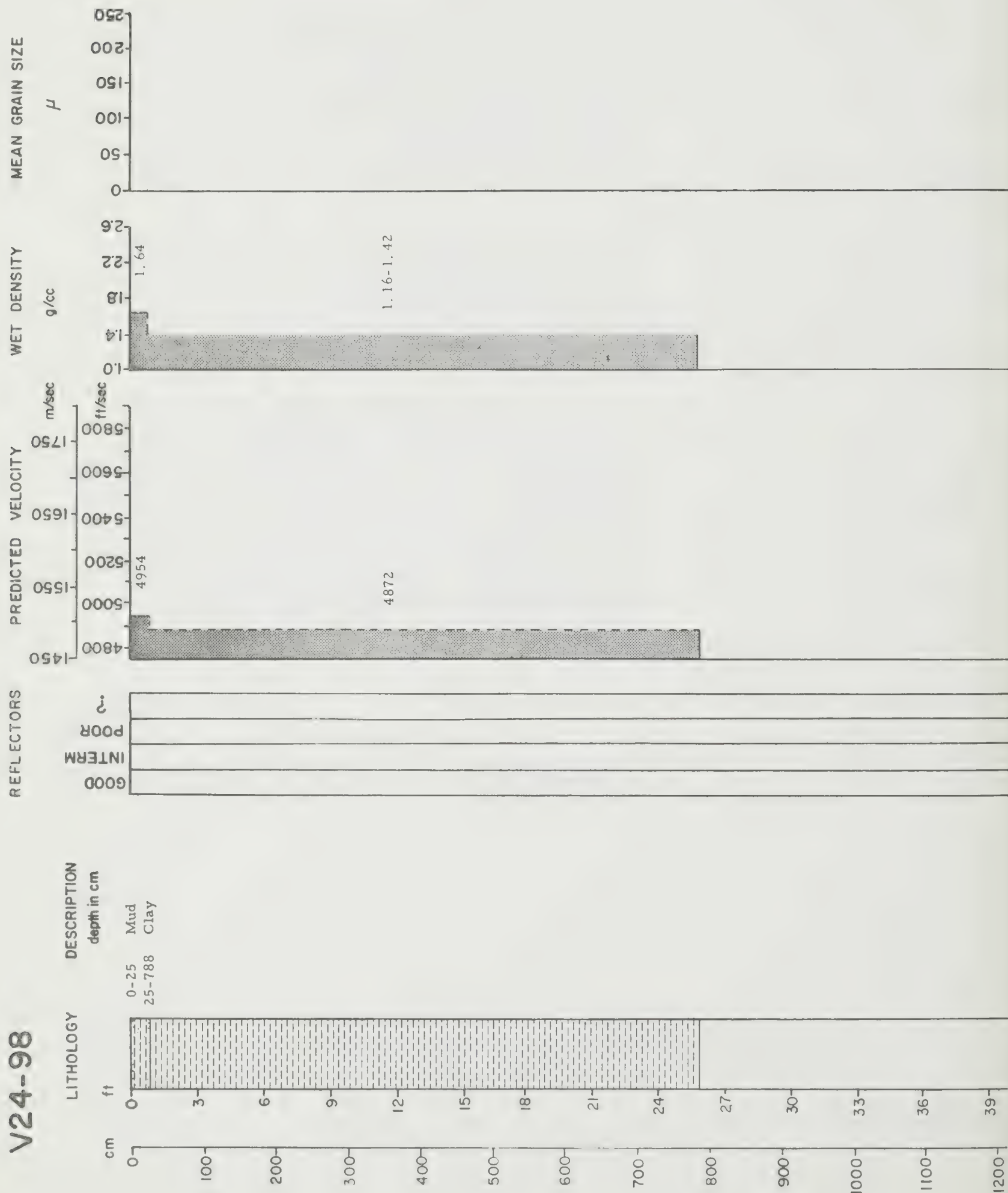
V24-96



V24-97



V24-98





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